

2509 Cedar Creek Road, Ayr, ON Township of North Dumfries Functional Servicing and Stormwater Management Report

May 3, 2024

Prepared for:

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Project No.: 161414214

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Introduction

1.0 INTRODUCTION

1.1 SITE LOCATION

The subject property is located at 2509 Cedar Creek Road in the Township of North Dumfries, Regional Municipality of Waterloo, Ontario as shown on Figure 1. The proposed Draft Plan includes the creation of a new private condo street, seven industrial zoned lots and stormwater management facility. The study area for the project comprises approximately 18.03 hectares, and is a mix of agricultural field, manicured lawns, scrubland, laneways, and buildings. The above described are illustrated in the proposed Draft Plan included in Appendix A.

1.2 BACKGROUND / OVERVIEW

The subject property is located within the Highway 401/97 Employment Area and currently zoned as zone Z.11 (industrial) with a north and south pocket zoned as zone Z.12 (open space). The subject property is bounded by industrial zoned lands to the west, Regional Road 97 (Cedar Creek Road) to the north, agriculturally zoned lands to the south and east. The closest noise sensitive land use (residence) is located approximately 235m east of the proposed Site. The proposed development meets the Class I (light industry). However, it is within the area of influence for Class II and recommended minimum separation distance of 300m from the closest existing residential land use for Class II (heavy industry). The industries in the proposed Site are expected to have MECP approval through the Environmental Compliance Approval (ECA).

1.3 PURPOSE OF THE REPORT

The purpose of this Functional Servicing and Stormwater Management Report (FSR) is to outline how the proposed subdivision can be supplied with adequate services, including sanitary, domestic water, storm drainage, stormwater management (SWM), and utilities to the requirements of the various approval agencies. The servicing strategies presented in this Report are conceptual. Detailed engineering drawings (for construction) and a Final SWM Report will be submitted as part of the final engineering design process once the proposed subdivision has received Draft Plan approval.

Stantec has conducted several onsite investigations to review the existing site conditions (see Existing Conditions Drawings, C-050 in Appendix B). Supplementary reports that should be read in conjunction with this report include:

- Documentation and Commemoration Report—2509 Cedar Creek Road, Township of North Dumfries prepared by Stantec Consulting dated February 2024.
- Geotechnical Investigation Preliminary Geotechnical Investigation for proposed industrial development, 2509 Cedar Creek Road, Ayr, ON prepared by Stantec Consulting dated January 2024.



Introduction

- Hydrogeological Assessment, 2509 Cedar Creek Road, Township of North Dumfries, ON prepared by Stantec Consulting dated May 2024.
- Land Use Noise Compatibility Study for the proposed industrial development at 2509 Cedar Creek Road, Township of North Dumfries Ontario, prepared by Stantec Consulting dated January 2024.
- Planning Justification Report, 2509 Cedar Creek Road, Ayr, Township of North Dumfries, ON prepared by Stantec Consulting dated May 2024.
- 2509 Cedar Creek Road, Ayr, ON Township of North Dumfries Scoped Environmental Impact Study prepared by Stantec Consulting dated May 2024.
- 2509 Cedar Creek Road Industrial Development, Chloride Impact Assessment- prepared by Stantec Consulting dated May 2024.
- 2509 Cedar Creek Road Traffic Impact Study, prepared by Stantec Consulting dated February 2024.

1.4 ENVIRONMENTAL ASSESSMENT REQUIREMENTS

The subject lands are located within the Regional Municipality of Waterloo (Region), Township of North Dumfries and within the administrative jurisdiction of the GRCA. The GRCA Regulation Limit associated with the Roseville Swamp Cedar Creek Provincially Significant Wetland Complex is on private property to the east and will be encroached upon by the SWM outlet channel. The subject lands lie within the Cedar Creek Sub Watershed of the Grand River Watershed.

Plans and policies relating to natural heritage that will be considered are detailed in the Scoped Environmental Impact Study.

All of the works required for the Cedar Creek lands are described in the subsequent sections of this Report. The plans, included in this Report, show the location of the proposed septic field, wells and SWM Facility, as well as grading, and utilities. The intent of this Report and, the supplementary Reports, is to ensure that the commenting agencies and the public are made aware of the servicing strategies for the proposed development.





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CEDAR CREEK ROAD HOLDINGS INC.

2509 CEDAR CREEK ROAD, AYR TOWNSHIP OF NORTH DUMFRIES, ON

Project No. 161414214 SITE LOCATION PLAN

Revision

Reference Sheet Figure No.

Date

Overall Grading

2.0 OVERALL GRADING

2.1 EXISTING LAND USE AND SITE TOPOGRAPHY

Most of the subject lands is currently vacant and used for agricultural purposes with remnants of a residential dwelling, associated driveways and ancillary structures along the northwest portion of the Site. Generally, the site slopes down in a southerly direction with an overall grade change of approximately +/-13m.

The topography of the subject lands slopes from west to east with a number of localized high and low points throughout the Site, elevations ranging from approximately 316 m along the northeast property line along Cedar Creek Road to approximately 301.0 m at the southern edge of the Site. There are localized hills and valleys within the Site with slopes ranging from 0.8% to 5%. There are two major existing drainage patterns within the Site; the first and largest catchment conveying external drainage from lands north of Cedar Creek Road via an existing culvert towards the Site and external lands directly west of the Site via the south Cedar Creek roadside ditch. These external areas enter the Site along the north edge of the property, crossing the lands and drains to a low area along the eastern property line to the neighboring lands (2407 Cedar Creek Road). The second includes external drainage from the Existing Municipal Infiltration based SWM Facility directly west of the subject lands that spill during large rain events to the remaining lands, south of the above noted catchment, that drain via sheet flow uncontrolled offsite through the southern property line of the Site to Con 10 PT Lots 28 & 29 Alps Road.

The shallow soil conditions at the Site typically comprised 0.8m to 1.4m of surficial silty sand topsoil overlying predominantly sand as well as sand and gravel/ gravel deposits. Localized, silt and/ or clay deposits were observed. Cobbles and boulders were noted withing the sand and gravelly deposits.

2.2 SITE AND ROAD PROFILE DESIGN CONSTRAINTS

Constraints in designing the road profiles and lot grading are as follows:

- Match existing grades, where possible, to minimize grading and cut/fill quantities and minimize changes to the surface hydrology and hydrogeology of the area.
- Match existing road elevations, with consideration given to forecasted road redevelopments (i.e., Cedar Creek Road).
- Satisfy the Town of North Dumfries's requirements for minimum and maximum road grades.
- Where possible, provide a major overland flow route.



Overall Grading

- Respect existing environmental feature configurations, elevations that are to be retained, and prescribed wetland buffer limits.
- Provide a spill point and conveyance for the Existing Municipal Infiltration based Stormwater Management Facility west of the subject lands.
- Provide a drainage conveyance for external lands north and west of the subject lands.

2.3 PROPOSED ROAD PROFILES AND OVERAL SITE GRADING

A preliminary road profile has been established for Street A, based on the proposed street alignment, to satisfy the constraints outlined in the previous section 2.2 - Design Constraints and Procedures (see Preliminary Road Profile Drawing C-200 included in Appendix B). The road profile is relatively smooth with grades ranging from a minimum of 0.5% to a maximum of 5.0%. The design strategy for the Street A grades was to match existing elevations at Cedar Creek Road and to maintain an overland flow drainage route to the proposed SWM Facility, while attempting to match the existing topography. The proposed centerline road elevations are illustrated on the enclosed Preliminary Road Profile C-200 referenced above and the Preliminary Servicing and Grading Plan C-400 to C-402 also included in Appendix B.

The proposed Street A road cross section for the private road within the subject development is shown on Figure 2. The cross section has been designed to be superelevated draining to the east and include for roadside ditches that have been sized to accommodate the conveyance for the various storm events. The east road ditch is proposed to collect the drainage from the proposed road and lots fronting onto the road such to convey the drainage to the proposed SWM Facility. The proposed ditch along the west side of the proposed road has been sized to provide conveyance for the major flows expected to spill from the existing Infiltration based SWM Facility west of the development such to drain south, by-pass the proposed SWM Facility and directed to the outlet channel that crosses the neighboring property known as 2407 Cedar Creek Road to the existing wetland located at Con. 10 PT Lot 27 on Cedar Creek Road.

The proposed lot grading within the Site will range between a minimum of 2.5% and a maximum of 6%, including 3:1 transition slope to accommodate the various grade changes within the proposed development (i.e., adjacent to the proposed SWM Facility) and at various perimeter locations surrounding the Site. The lot grading is designed to split drainage such to minimize raising the Site. The lot grading is designed to be split drainage with the front of the lot draining to the east road ditch and the rear draining to a rear lot ditch. Both the east ditch and rear lot ditch convey lot drainage to the proposed SWM Facility for treatment prior to discharging to the outlet channel. Profiles of the east road ditch, rear lot ditch and outlet channel are illustrated in the Preliminary Road Profiles referenced above and the proposed grading is illustrated on the Concept Grading Plans also noted above and included in Appendix B.



Overall Grading

The stormwater management (SWM) Block is proposed at the southern edge of the Site. The SWM outlet is proposed to discharge to an outlet channel that will be established with an easement in favour of the proposed development, that will traverse the southern and eastern portions of the adjacent lands known as 2407 Cedar Creek Road, to the existing wetland located at Con. 10 PT Lot 27 on Cedar Creek Road and eventually discharging to the southern edge of the Roseville Swamp Cedar Creek Provincially Significant Wetland Complex on the west side of the CP rail line.

Preliminary earthwork calculations have been performed based on the preliminary road profiles and lot grades. The calculations indicate that there is an earth fill shortage with a surplus of existing topsoil. Surplus topsoil is to be reused onsite as fill where feasible, to minimize the fill shortage and import requirement. Please refer to Conceptual Cut/Fill Plan and earth quantities on Drawings C-900 also included in Appendix R

At detailed design, profiles and grading will be refined to minimize the required earth fill shortage.



3.0% FOR ROADS < 1.0% GRADE 2.5% FOR ROADS > 1.0% GRADE

Notes

TYPICAL ROAD CROSS—SECTION
"STREET_A"

MINIMUM DEPTH OF COVER (UNLESS OTHERWISE SPECIFIED) GAS MAIN 0.60m HYDRO 0.90m TELEPHONE 0.75m CABLE T.V. 0.75m

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CEDAR CREEK ROAD HOLDINGS INC.

2509 CEDAR CREEK ROAD, AYR TOWNSHIP OF NORTH DUMFRIES, ON

NOTE(1) - THICKER SUBBASE WILL BE REQUIRED

WHERE SUBGRADE CONSISTS OF SILT.

Project No. 161414214

CROSS-SECTION

Revision

Reference Sheet

Figure No. 2.0

Date

Site Servicing

3.0 SITE SERVICING

3.1 SANITARY AND WATER SERVICING

Individual onsite sewage systems utilizing conventional septic system and tertiary treatment with subsurface discharge of treated effluent will provide sanitary servicing for each lot in the development. The individual onsite sewage systems will be located entirely within each property boundary. It is intended that these services would be privately owned and operated.

The conventional septic system consists of a two-compartment septic system, followed by a septic bed, fed either by gravity (where site topography allows it) or with an effluent pump. The gravity system, being the most economical where soils in place consist of sand, being the case at most of the proposed lots, will require the largest septic field footprint. The tertiary system is an advanced treatment system with a modified septic tank, used as a digester, followed by a biofilter tank, a recirculation pump, and an effluent pump feeding a modified septic field. As the treatment process normally occurring within the septic field, with a tertiary system, this treatment would be completed within these aforementioned tanks and respective septic field footprint could be reduced by one third compared to the conventional system.

This would allow an increase in the number of employees at a given lot, for the same septic field footprint.

Additional details regarding the water and sewage system feasibility is outlined in a Study included in Appendix C.

The Provincial Policy Statement (2005) section 1.6.4.4 does allow for individual onsite services as follows: Individual onsite sewage services and individual onsite water services shall be used for a new development of five or less lots or private residences where municipal sewage services and municipal water services or private communal sewage services and private communal water services are not provided and where site conditions are suitable for the long-term provision of such services. Despite this, individual onsite sewage services and individual onsite water services may be used to service more than five lots or private residences in rural areas provided these services are solely for those uses permitted by policy 1.1.4.1(a) and site conditions are suitable for the long-term provision of such services. In rural areas located in municipalities: a) permitted uses and activities shall relate to the management or use of resources, resource-based recreational activities, limited residential development and other rural land uses. Based on the above, the proposed development complies with the Provincial Policy Statement.



Site Servicing

3.2 STORM SERVICING

No traditional storm sewers are proposed for the subject development as the majority of the proposed Lots and road will drain to the proposed roadside ditches or rear yard ditch that conveys site drainage to the proposed SWM Facility. This drainage pattern is further described in Section 4.0 below. A by-pass storm sewer is proposed such to convey external drainage from the north and west of the Site to the adjacent lands mimicking the existing drainage conditions. Further details regarding this by-pass storm sewer described below in section 4.0 and demonstrated on the engineering plans included in Appendix B.



Preliminary Stormwater Management

4.0 PRELIMINARY STORMWATER MANAGEMENT

The Preliminary Stormwater Management (PSWM) design has been completed in support of the Draft Plan for the proposed 2509 Cedar Creek Rd Industrial Development, North Dumfries, Ontario. This section discusses the PSWM strategy for the Site that has been developed in order to mitigate potential impacts of the proposed development on adjacent water features.

4.1 STUDY APPROACH

A SWM strategy for the Site has been developed in order to mitigate against potential offsite water quality and quantity impacts associated with the development of the subject lands.

The SWM design involved the following study components:

- Complete a hydrologic study to determine the existing site conditions (pre-development conditions) with respect to topography, soils information, and existing land uses.
- Prepare an existing (pre-development) and proposed (post-development) condition hydrologic model using SWMHYMO to determine runoff volumes and peak flow rates to downstream areas.
- Complete the preliminary design of the SWM Facility to provide sufficient water quality and water quantity control to achieve target rates to downstream receivers.
- Summarize the Study through preliminary design and recommendations.

4.2 BACKGROUND

The following reports and primary guidance documents were referenced in the completion of the proposed SWM design:

- Preliminary Geotechnical Investigation for Proposed Industrial Development, 2509 Cedar Creek Road, Ayr, Ontario, Stantec Consulting Ltd., January 16th, 2024.
- Erosion and Sediment Control Guide for Urban Construction, Toronto and Region Conservation Authority, 2019.
- City of Kitchener Development Manual, City of Kitchener, 2021.
- Stormwater Management Planning and Design (SWMPD) Manual, Ministry of the Environment, Conservation and Parks (MECP), March 2003.
- Low Impact Development Stormwater Management Planning and Design Guide (LID Manual), Credit Valley Conservation Authority and Toronto and Region Conservation Authority, 2010.



Preliminary Stormwater Management

4.3 STORMWATER MANAGEMENT DESIGN CRITERIA

The SWM criteria for the subject lands were established through the above-mentioned documentation and pre-consultation with the Grand River Conservation Authority (GRCA), the Township of North Dumfries, and the Region of Waterloo. The SWM criteria are as follows:

- Water Quality Provide sufficient permanent pool and extended detention volume to meet the MECP Enhanced (80% Total Suspended Solids [TSS] Removal) criteria and promote the at-source removal of potential contaminants.
- Water Quantity Provide sufficient water quantity control to maintain proposed peak flow rates
 to existing levels for all storms up to and including the 100-year storm event.
- **Infiltration and Water Balance** Promote infiltration measures where possible and provide best efforts to match existing infiltration rates.
- **Erosion Control** Provide sufficient extended detention for the 25 mm storm event with a minimum 24-hour drawdown period.
- **Erosion and Sediment Control** Provide appropriate erosion and sediment control during construction/area grading to protect adjacent properties from potential siltation.

4.4 EXISTING CONDITIONS

4.4.1 Topography and Surface Drainage

As noted in the *Preliminary Geotechnical Investigation Report* (Stantec, 2024), the Site generally slopes down toward the south with an overall grade change of approximately 13 m. Based on topographic information, the ground surface is highest in the north of the subject site near elevation 314 m above mean sea level (AMSL) and slopes down toward the south border of the property near elevation 301 m AMSL. There is a high point in the northeast of the Site, with an elevation of approximately 316 m AMSL.

The Site is generally split by a drainage divide running east to west near the centre of the property. The drainage divide creates two predominant drainage zones (flows to the east and flows to the south), with flows from both directions draining overland to neighboring properties, and ultimately discharging to Cedar Creek. Additionally, several external catchment areas drain onto and are conveyed through the Site. These include a small agricultural area to the east of the site draining overland onto the site and a large mostly industrial area to the north that is conveyed to the Site through an existing culvert under Cedar Creek Road. These external areas are conveyed through the Site, eventually discharging east to the neighboring property. Additional industrial catchment areas to the west of the Site, including the outflow from an existing SWM feature, enter the Site from the west and discharge east or south.

Existing conditions drainage information is presented on Figure 3 and Figure 3.1, which present the Pre-Development Drainage Plans.



Preliminary Stormwater Management

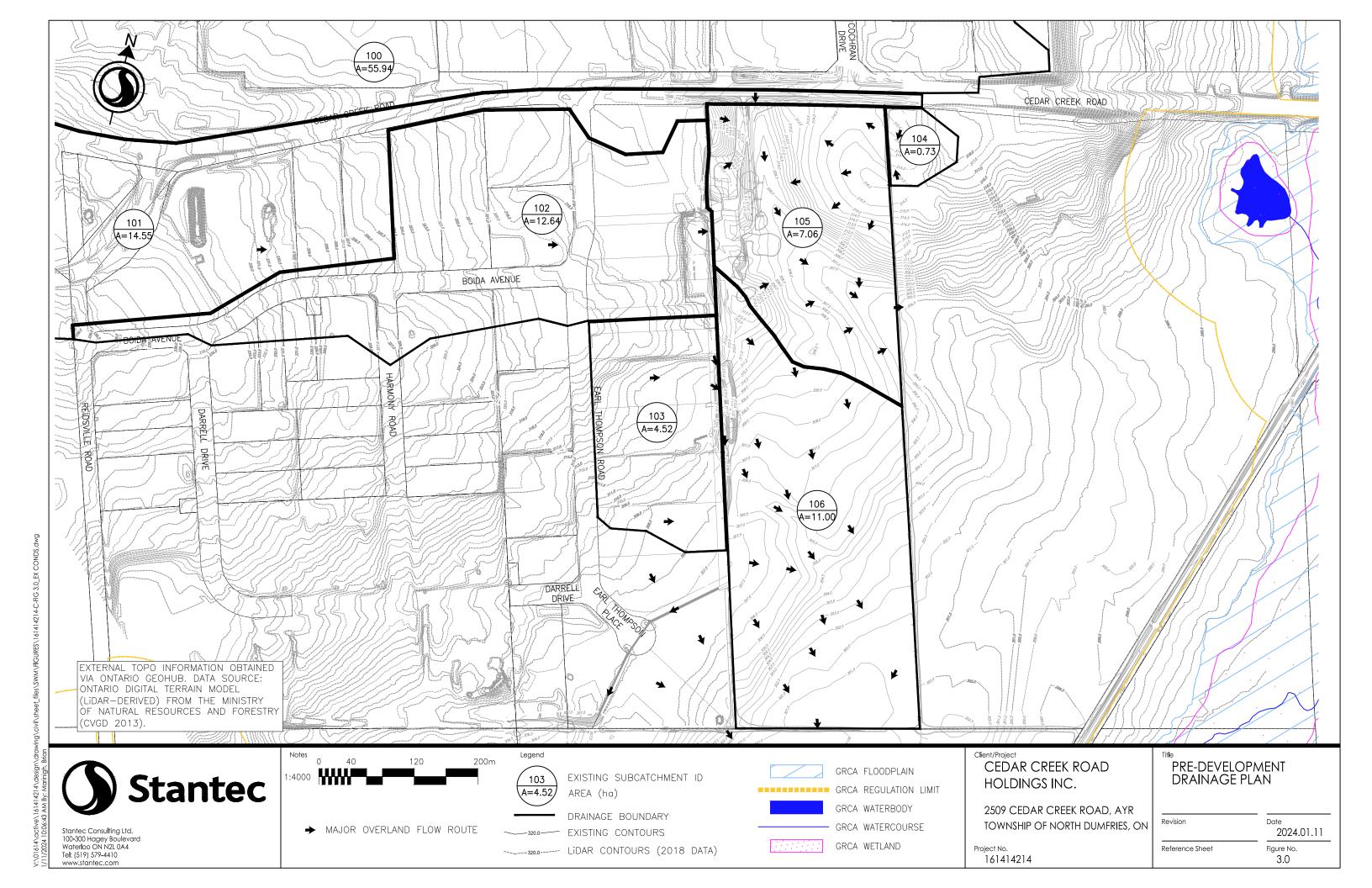
4.4.2 Geotechnical Information

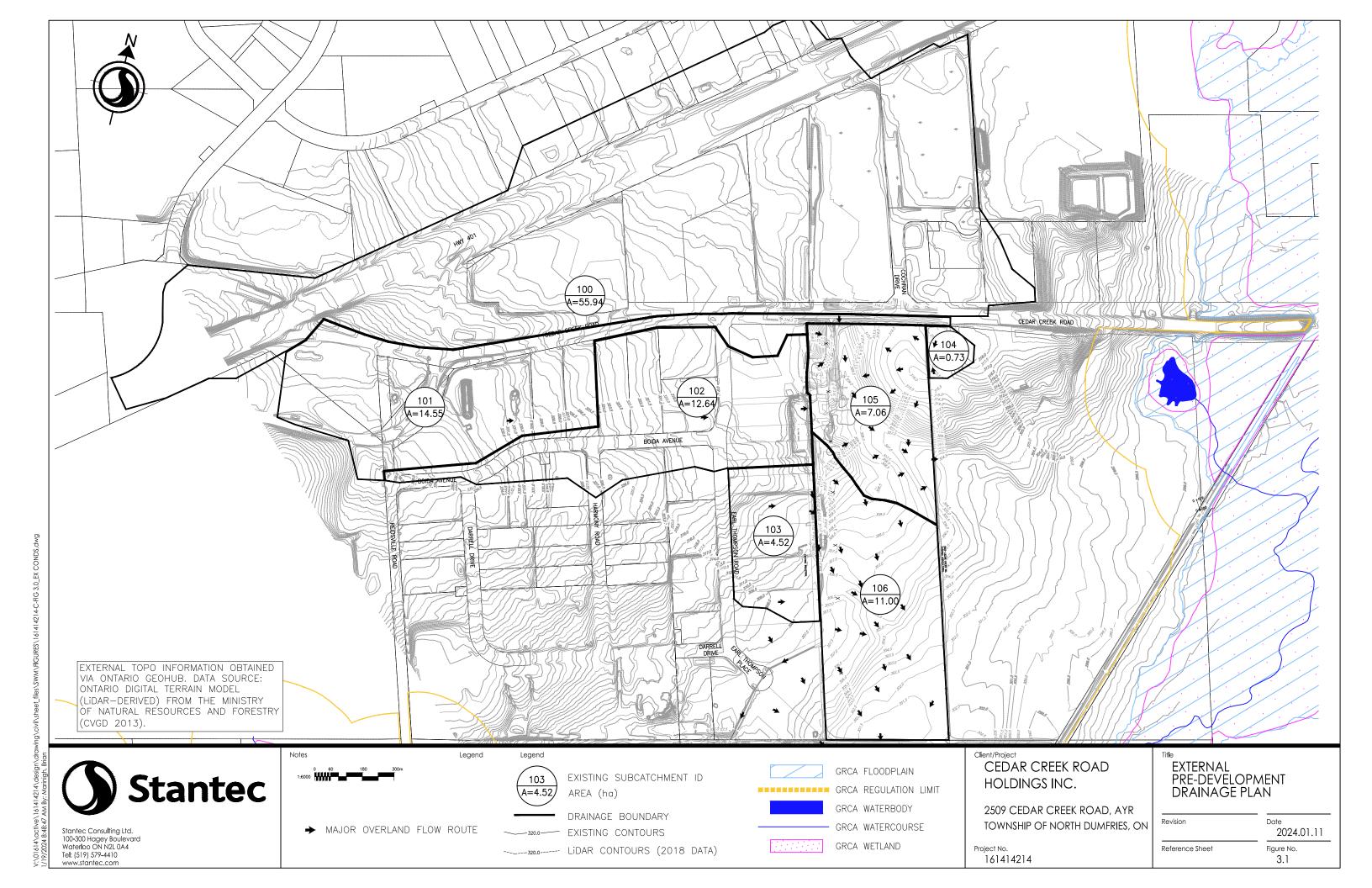
As identified in the *Preliminary Geotechnical Investigation Report* (Stantec, 2024), the subsurface soils for the Site are predominantly sand overlain by a silty sand topsoil. Some sand and gravel/gravel deposits and occasional silt and/or clay deposits were also found in some locations. Cobbles and bounders were also noted within the sand and gravel deposits. Bedrock was not encountered at the boreholes advanced for this Site.

Based on results from the *Preliminary Geotechnical Investigation*, groundwater levels in the north third of the Site ranged between 2.8 m below ground surface (BGS) to 10.3 m BGS (elevations ranging from 304.6 m to 305.3 m AMSL) in spring 2022 and were approximately 0.5 - 1 m lower in fall 2022 (Stantec, 2024). The monitoring wells in the south two-thirds of the Site were dry during testing, so the depth of the water table in this region is unknown. However, well depths in this area ranged from 5.02 m BGS to 6.03 m BGS (296.77 m AMSL to 305.89 m AMSL), suggesting that the water table is located further BGS than this in these areas. There is a potential for localized perched groundwater at shallower depths following heavy rain or snow melt in the spring (Stantec, 2024).

Thus, the predominant soil conditions (sand with trace silt and gravel) will generally be suitable for at-source infiltration of precipitation. In areas with higher silt content, lower infiltration rates should be expected.







5.0 STORMWATER MANAGEMENT DESIGN

5.1 HYDROLOGIC MODELING

A hydrologic model was prepared using SWMHYMO to simulate drainage conditions for the subject development under existing and proposed development conditions. The model was employed to predict flows and design SWM systems to ensure the criteria are achieved.

In the absence of IDF parameters for Township of North Dumfries, City of Kitchener's IDF parameters were used. Model results were obtained for the existing and proposed conditions for the following events:

- The 25 mm, 4-hour Chicago Storm derived using the parameters as provided in Table 1
- The 2-, 5-, 10-, 25-, 50-, and 100-year, 3-hour Chicago distributions derived using the parameters provided in Table 1
- The 48-hour Regional Rainfall Event (i.e., Hurricane Hazel)

Table 1: Rainfall Events - City of Kitchener IDF Parameters

	IDF Parameters							
Return Period	A	В	С	Depth (mm)				
25 mm, 4-hr	509	6	0.7989	25.0				
2-year, 3-hr	743	6	0.7989	34.3				
5-year, 3-hr	1593	11	0.8789	47.3				
10-year, 3-hr	2221	12	0.9080	56.3				
25-year, 3-hr	3158	15	0.9355	68.3				
50-year, 3-hr	3886	16	0.9495	77.2				
100-year, 3-hr	4688	17	0.9624	87.1				
Hurricane Hazel	-	-	-	285				

5.2 EXISTING CONDITIONS HYDROLOGIC MODEL

An existing conditions hydrologic model was prepared to simulate existing conditions for the Site. Input and output files for the SWMHYMO model are provided in Appendix D. Soil Conservation Service (SCS) Curve Numbers (CN) and catchment parameters were calculated for each existing catchment based on land use and soil type and are provided in Appendix D. Delineation of existing drainage catchments is provided on Figure 3 and Figure 3.1 which present the Pre-Development Drainage Area Plans, and are summarized below:

- Catchment 100: 55.94 ha of industrial property northwest of the Site and part of Highway 401, draining south through a culvert under Cedar Creek Road into the Site and flowing south/east through the Site.
- Catchment 101: 14.55 ha of external catchment containing a portion of Cedar Creek Road, a portion of industrial property, and a grassed area near Highway 401 off-ramp, entering the Site in the north and draining overland to the south/east.
- Catchment 102: 12.64 ha of external industrial area west of the Site, draining to private external SWM feature overflowing into the subject Site, ultimately flowing east through the Site.
- Catchment 103: 4.52 ha of external industrial area west of the Site, draining east into the Site and ultimately flowing south.
- Catchment 104: 0.73 ha of external agricultural area northeast of the Site, draining west into the Site and ultimately flowing south/east through the Site.
- Catchment 105: 7.06 ha of agricultural area in the north portion of the Site including a small house and driveway, draining to agricultural land to the east and eventually to Cedar Creek.
- Catchment 106: 11.00 ha of agricultural area in the southern portion of the Site draining south and eventually to Cedar Creek.

5.3 PROPOSED CONDITIONS HYDROLOGIC MODEL

The proposed development incorporates seven industrial lots and a SWM Facility Block, along with one new road. The proposed SWM Facility will be located in the southern portion of the Site and discharge mostly via infiltration, with a constructed conveyance channel (called the outlet channel) provided to convey high flows to Cedar Creek in the east.

The SWM Facility is proposed to provide water quality and quantity control for the entire 2509 Cedar Creek Road development. The drainage from the external agricultural lands to the west of the Site is to be routed around the perimeter of the Site via a swale (called the west road ditch), which will connect to the outlet channel to Cedar



Stormwater Management Design

Creek. The drainage from the external lands to the northwest of the Site will enter a storm sewer upon entry into the Site (called the By-Pass Storm Sewer) and be released east of the Site, where the existing flows drain.

Catchment parameters including impervious percentage, slope, and SCS Curve Numbers were calculated for each of the proposed catchments based on land use and soil type and are provided in Appendix D. All input and output files are provided in Appendix D. The delineation of the proposed drainage catchments is provided on Figure 4, Post-Development Drainage Plan, and is summarized as follows:

- Catchment 100: 55.94 ha of industrial property northwest of the Site and part of Highway 401, draining south through a culvert under Cedar Creek Road into the By-Pass Storm Sewer and discharging to the agricultural lands to the east.
- Catchment 101: 14.55 ha of external catchment containing a portion of Cedar Creek Road, a portion of industrial property, and a grassed area near Highway 401 off-ramp, entering the By-Pass Storm Sewer and discharging to the agricultural lands to the east.
- Catchment 102: 12.64 ha of external industrial area west of the Site, draining to private external SWM feature
 and overflowing into the west road ditch, where flow is conveyed around the SWM Facility to the outlet
 channel.
- Catchment 103: 4.52 ha of external industrial area west of the Site, draining east into the west road ditch, where flow is conveyed around the SWM Facility to the outlet channel.
- Catchment 104: 0.73 ha of external agricultural area northeast of the Site, draining west into the rear lot ditch, where flow is conveyed to the east inlet of the SWM Facility.
- Catchment 200: 0.14 ha in northwest corner of property comprising a small portion of the west road ditch, draining to the By-Pass Storm Sewer and discharging uncontrolled to the east.
- Catchment 201: 0.64 ha in the northwest corner of property containing a portion of the east road ditch and developed land, draining to the By-Pass Storm Sewer and discharging uncontrolled to the east.
- Catchment 202: 8.82 ha of developed area covering the east portion of the Site, draining to the rear lot ditch and entering the SWM Facility through the east forebay.
- Catchment 203: 0.55 ha catchment on the east side of the Site containing the By-Pass Storm Sewer outlet and plunge pool, draining offsite to the east.
- Catchment 204: 4.92 ha of developed area, draining to the west into the east road ditch, entering the SWM Facility through the west forebay.
- Catchment 205: 1.63 ha SWM Facility Block.



Stormwater Management Design

- Catchment 206: 0.76 ha grassed swale (west road ditch), located on the far west side of the property, directing flows around the SWM Facility to the outlet channel at the southeast corner of the property.
- Catchment 207: 0.14 ha south of the SWM Facility, draining offsite to the south.
- Catchment 208: 1.13 ha of constructed conveyance channel (outlet channel), directing flows to Cedar Creek in the northeast.

Note that the private SWM feature in Catchment 102 has been modelled according to assumptions made based on LiDAR data and the surrounding soil characteristics.



5.4 PROPOSED SWM STRATEGY

The proposed SWM strategy for the 2509 Cedar Creek Road development incorporates minor and major system conveyance via grassed swales (east road ditch and rear lot ditch) to the proposed SWM Facility for water quality and quantity control. Infiltration has been incorporated on a lot-level basis where possible, as well as within the end of pipe SWM Facility. The SWM strategy has been developed in accordance with the objectives and criteria previously listed.

5.4.1 Stormwater Management Facility Design

Runoff from the majority of the proposed development drains into an infiltration facility complete with two forebays located in each inlet to the facility. The location of this proposed SWM Facility was selected for a variety of reasons including the following:

- This is an existing low point on the Site where water naturally drains overland offsite.
- This location is the most efficient use of land for the future development of the Site and minimizes the cut/fill impacts of development.

The proposed SWM Facility is designed to provide water quantity and quality control for 16.10 ha of land (including 0.73 ha of external agricultural land) as well as infiltration to simulate natural conditions of the Site and aid in groundwater recharge. As outlined in the preliminary criteria, the SWM Facility is required to provide 'enhanced' water quality treatment prior to discharging downstream.

The SWM Facility is designed to infiltrate all minor storms including the 10-year event, while major storm events greater than the 10-year storm will be attenuated in the infiltration cell, eventually discharging to Cedar Creek through the outlet channel at rates below existing conditions. The SWM Facility forebays will provide initial water quality treatment and isolation of sediment deposition for ease of cleanout as well as to minimize transport of fines from entering and clogging the infiltration cell. The infiltration cell will provide further water quality treatment through infiltration of most runoff events. Since the basin will be sized to infiltrate up to the 10-year storm event, it can be assumed it will also provide over 80% TSS removal prior to discharge downstream. Additionally, the MECP infiltration basin volume requirement for quality control based on an enhanced level of treatment is 608 m³, whereas this facility contains over 7000 m³ of infiltration volume.

In addition to the water quality benefit described above, the SWM Facility (including forebays and infiltration cell) will provide water quantity storage as well as enhance groundwater recharge. To provide a conservative estimate during the design of water quantity control infrastructure in the SWM Facility, any infiltration that will occur in the conveyance swales (east road ditch and rear lot ditch) was ignored in the modelling, leading to more runoff entering the SWM Facility. The preliminary design of the SWM Facility has maximum ponding elevations of 302.69 m above sea level (ASL) and 302.85 m ASL during the 100-year and Regional Storm Events, respectively. This leads to a depth of 0.19 m and 0.35 m above the maximum infiltration depth during the 100-year and Regional Storm Event, respectively. Thus, ponding height from the bottom of the infiltration cell is



Stormwater Management Design

1.19 m for the 100-year event and 1.35 m for the Regional Storm Event. Although the height of water in the SWM Facility exceeds the recommended maximum of 0.6 m for infiltration facilities for these storm events, the more frequent storm events (25 mm and 2-year) remain under this height and thus compaction that would limit the functionality of the infiltration basin is not expected. The freeboard to the top of pond for 100-year storm event is 0.31 m. For all events greater than the 10-year (25-year, 50-year, 100-year, and the Regional Storm), the flows are conveyed though the overflow weir and enter the outlet channel to Cedar Creek. The weir elevation has been set to provide sufficient infiltration volumes while ensuring infiltration drawdown times do not exceed 48 hours. The 1.2 m deep forebays have a sediment storage capacity of 129 m³ and 190 m³ for the west forebay and east forebay respectively, at a maximum depth of sediment at 0.5 m, providing an expected cleanout frequency of approximately once every 9 years for the west forebay and 7 years for the east forebay. The forebay length required to provide appropriate dispersion and settling length for the 5-year inlet flow is 30 m and 52 m and the length provided is approximately 44 m and 54 m, for the west forebay and east forebay respectively. Detailed design calculations are provided in Appendix D.

The SWM Facility is proposed to be drained by a single outflow weir once the infiltration volume is exceeded. Flows that pond to an elevation higher than the infiltration depth will discharge over the weir into the outlet channel to Cedar Creek. This will occur for events greater than the 10-year storm event. Details on the SWM Facility design and operating characteristics are summarized in Table 2 and Table 3 respectively, and the detailed stage-storage-discharge analysis for the proposed SWM Facility is provided in Appendix D. Additionally, a detailed drawing of the SWM Facility is included on Drawing C-410 (Appendix B).

Overall, the SWM Facility will provide an 'enhanced' level of water quality control through inlet forebays and the subsequent infiltration cell. The SWM Facility will enhance infiltration across the Site to maintain groundwater recharge while providing a total drawdown of <48 hours for all storm events. Design characteristics for the proposed SWM Facility are summarized in Table 2, with calculations provided in Appendix D.



Table 2: SWM Facility Design Characteristics

Parameter	Basin Characteristics	
Total Contributing Area (quality and quantity)	16.10 ha	
Total Percent Impervious to SWM Facility (includes external agricultural area – catchment 104)	78%	
Forebay Parameters:		
West forebay		
Required Forebay Length/Provided Forebay Length	30 m / 44 m	
Forebay Depth	1.2 m	
Sediment Storage Volume Provided	129 m³	
Cleanout Frequency	9.0 years	
East forebay		
Required Forebay Length/Provided Forebay Length	52 m / 54 m	
Forebay Depth	1.2 m	
Sediment Storage Volume Provided	190 m³	
Cleanout Frequency	7.1 years	
Infiltration Cell Details:		
Infiltration Cell Top of Ponding Elevation	302.5 m	
Infiltration Cell Bottom Elevation	301.5 m	
Infiltration Depth	1 m	
Infiltration Footprint	5,524 m ²	
Maximum Infiltration Drawdown	43.9 hours	
Total Depth of SWM Facility	1.5 m	
Outlet Structure Details:		
Overflow Weir Crest Invert/ Length / Side Slopes (H:V)	302.50 m / 3 m / 10:1	

The operating characteristics of the SWM Facility are summarized in Table 3. Detailed modelling files are found in Appendix D.

Table 3: SWM Facility Operating Characteristics

Storm Event	25 mm	2-year	5-year	10- year	25- year	50-year	100- year	Regional
Proposed Peak Flow Rate to SWM Facility (m³/s)	1.725	2.661	3.587	4.502	5.227	5.952	6.807	2.235
Proposed Peak Flow Rate from the SWM Facility (m³/s)	0.000	0.000	0.000	0.000	0.115	0.322	0.631	2.145
Maximum Total Storage Volume (m³)	2,158	3,378	5,054	6,250	7,479	8,016	8,524	9,857
Maximum Ponding elevation (m)	301.83	302.01	302.24	302.40	302.56	302.62	302.69	302.85
Infiltration Drawdown Time (hrs.)	13.5	21.1	31.5	39.0	43.9	43.9	43.9	43.9

Target peak flow rates to the east and south as well as peak flow rates for proposed conditions are summarized in Table 4 while detailed modelling files are included in Appendix D. Note that in the models, catchment 104 is modelled as an "internal" catchment because the flows are being directed to the SWM Facility, even though it is not within the Site boundary. As observed in Table 4, water quantity targets from the Site have been met as the proposed peak flow rates from the Site to the east and south are at or below target levels. However, when considering the flows from external catchments that flow through the Site as well as internal catchments (collectively referred to as the "Study Area"), proposed flows to the east are slightly higher (≤3% increase for all storms up to and including the 100-year storm event). This is because flows from a large external catchment (Catchment 103) are being redirected around the Site to discharge to the east in the proposed conditions, whereas in existing conditions, the flows exit the Site to the agricultural lands to the south. However, these flows are all discharging to the same Cedar Creek system, with more of the flow now discharging further upstream, into the wetland area around Cedar Creek. Since flows from only a small area (Catchment 207) from the study area are being discharged south of the Site in the proposed conditions, the total flows to the Cedar Creek system will be much lower than existing conditions. Infiltration through the west road ditch and through the outlet channel to the east has also not been considered, so the actual increase in peak flow will be lower than what is shown in the model. Additionally, there is a larger external area east of the Site draining to the discharge point to the Cedar Creek system, which will further minimize the overall effect of the small increase from the Site flowing east.

Table 4: Existing and Proposed Flow Rates

Storm Event	25 mm	2-year	5-year	10- year	25-year	50-year	100-year	Regional
Existing Peak Flow Rate (PFR) from Site Towards East (m³/s)	0.081	0.148	0.283	0.399	0.553	0.684	0.836	0.989
Existing PFR from Site Towards South (m³/s)	0.078	0.146	0.278	0.389	0.544	0.673	0.823	1.242
Existing PFR from Study Area Towards East (m³/s)	2.284	3.920	6.604	8.840	12.689	16.169	19.26	11.995
Existing PFR from Study Area Towards South (m³/s)	0.435	0.662	0.895	1.133	1.350	1.554	1.819	1.755
Proposed PFR from Site Towards East (m³/s)	0.071	0.109	0.155	0.202	0.242	0.374	0.705	2.375
Proposed PFR from Site Towards South (m³/s)	0.001	0.003	0.005	0.007	0.010	0.013	0.016	0.015
Proposed PFR from Study Area Towards East (m³/s)	2.311	4.001	6.766	9.079	12.737	16.538	19.839	14.011
Proposed PFR from Study Area Towards South (m³/s)	0.001	0.003	0.005	0.007	0.010	0.013	0.016	0.015

5.5 OTHER SWM FEATURES

There are four grassed swales (ditches) on the Site (west road ditch, east road ditch, rear lot ditch, and the outlet channel). These swales are designed to convey flow around the perimeter of the Site and to Cedar Creek. Grassed swales are known to provide infiltration and water quality benefits as the water travels over the pervious area. However, the amount of infiltration and sediment removal efficiency the swale can achieve is hard to predict, thus these additional benefits have not been accounted for, providing a conservative SWM Facility design. All grassed swales have been sized to convey the largest peak flows from the modelled events (100-year or Regional Storm Event). Details on the swale design can be found in Appendix D.

Additionally, a plunge pool and spreader swale has been provided following the outlet from the By-Pass Storm Sewer on the east border of the Site (Catchment 203). The plunge pool will help dissipate the energy from the pipe and provide more infiltration potential while the spreader swale will help to release the flows over a greater surface area, reducing the erosion potential to the neighbouring external lands. Details of the plunge pool and spreader swale will be designed at a future design stage. The use of a perforated pipe system in the By-Pass Storm Sewer also will be investigated in future design stages to provide the potential for infiltration into the surrounding soils before daylighting into the plunge pool.

5.6 ADDITIONAL DESIGN CONSIDERATIONS

5.6.1 Infiltration

The geotechnical work performed by Stantec identifies a predominant soil of sands across the Site with smaller areas of gravel and silts. Based on the results of the *Preliminary Geotechnical Investigation* (Stantec, 2024), it can be concluded that the soils are generally suitable for infiltration. Additionally, infiltration testing conducted as a part of the *Hydrogeological Assessment* confirms this conclusion (Stantec, 2024). Locations with higher silt content have lower infiltration rates, as expected, whereas locations with higher amounts of non-cohesive sand and gravel (such as the south portion of the Site) have higher infiltration rates, presenting favorable conditions for on-site infiltration.

In general, the sandy soils onsite have coefficients of permeability of about 2.0x10⁻³ cm/sec. The infiltration rates for these soils are estimated to have an unfactored infiltration rate of approximately 100 mm/hr, which is representative of the soils in the location of the proposed infiltration facility. Applying a safety factor of 3.5 (LID Manual, 2010) leads to a preliminary infiltration rate of approximately 29 mm/hr. The suitability of existing soils should be assessed at the proposed elevation of any infiltration facility on a lot-by-lot basis following completion of site grading.

To promote infiltration, it is proposed that all rooftops throughout the development be directed to soak-away pits sized to retain runoff from the 25 mm event. Additionally, flows from the Site will be conveyed to the SWM Facility through swales, promoting infiltration, especially during smaller rainfall events.



5.6.2 End-Of-Pipe Infiltration

As mentioned previously, the proposed SWM Facility will be designed as an infiltration facility comprising of two dry forebays to provide initial water quality treatment and isolation of sediment at each inlet, followed by the main infiltration cell. The proposed SWM Facility provides additional retention volume to increase the groundwater recharge and decrease the excess runoff volume to the surrounding lands. The proposed system will be operational all year round. As this Site is outside of any Well Head Protection Areas (WHPAs), infiltration of winter runoff is assumed to not pose a significant risk to any drinking water sources. Additionally, infiltration of the winter runoff as opposed to directing this downstream via surface flow will help reduce the impact of salt on the aquatic vegetation. However, a chloride impact assessment has been conducted and will be provided under separate cover.

The infiltration cell functions by setting the SWM Facility outlet to the outlet channel to Cedar Creek above the base of the infiltration cell to provide a 'dead' ponding depth/volume that will then infiltrate through the amended soil and existing sandy soil layer. To determine this outlet elevation, the SWM Facility was modelled in SWMHYMO with infiltration as the only outflow value. The infiltration cell in the SWM Facility has a footprint of 5,524 m², which leads to an outflow rate of 0.044 m³/s using the factored infiltration rate of 29 mm/hr. Above the infiltration volumes or 'dead' storage volumes, water will be attenuated and released to the outlet channel to Cedar Creek via the outflow weir. This volume provides active storage to attenuate the large storm events.

The facility infiltrates all frequent storms (the 25 mm rainfall event alone represents approximately 80% of the annual precipitation volume), therefore, infiltration of this volume will make a significant contribution to the Site infiltration, leading to an overall infiltration surplus and aiding in groundwater recharge. A water balance analysis was completed as part of the *Hydrogeological Investigation*, documented under separate cover (Stantec, 2024). Further investigation/analysis will be necessary at the detailed design and site plan stages to confirm site water balance, infiltration rates, and depth to high groundwater levels at the base of the proposed infiltration facilities; however, it is assumed that as most of the Site is being infiltrated, the water balance targets will be maintained.

5.7 SWM FACILITY LINER

As discussed in the *Preliminary Geotechnical Investigation Report* (Stantec, 2024), the soils within the proposed SWM Facility Block include mainly sandy soils with the high groundwater level measured to be >5 m below the existing ground surface. Thus, due to the favorable soil conditions and resulting proposed infiltration measures, no liner is recommended for any portion of the SWM Facility. This will also allow the forebays to provide additional infiltration that has not been accounted for.



Erosion and Sediment Control

6.0 EROSION AND SEDIMENT CONTROL

The erosion and sediment control strategy has been developed and is to be implemented during the construction process, in order to minimize the potential for offsite discharge of sediment and the resultant negative environmental impacts. This plan will focus on the protection of the downstream areas.

6.1 EROSION POTENTIAL

The Toronto and Region Conservation Authority's Erosion and Sediment Control Guide for Urban Construction (2019) was used to determine the erosion potential of the Site. The erosion potential is based on slope gradient, slope length, and soil texture and is then used to determine the appropriate erosion control methods, as follows:

- Site Slopes: Generally gentle (< 2%) to moderate (2-10%) average slope is approximately 2%.
- Slope Lengths: Long (generally greater than 30 m).
- Erodibility Classification: High erodibility rate for silty sand and low erodibility rate for sandy soils.

Therefore, based on this classification the Site has moderate to high erosion potential, depending on the specific location within the Site.

6.2 PRELIMINARY EROSION AND SEDIMENTATION CONTROL PLAN

The following approach to erosion and sediment control onsite has been prepared to minimize the potential impacts associated with onsite erosion and/or offsite transport of sediment to downstream areas.

Prior to any grading or servicing works commencing onsite, erosion and sedimentation control measures shall be implemented as detailed on the Pre-grading, Erosion and Sedimentation Control Plans (prepared during detail design). The erosion and sedimentation controls will include the following items:

- Steep slopes (>3:1) shall have erosion blankets.
- Light and/or heavy-duty silt fencing will be erected on all site boundaries where there is potential for runoff
 to be discharged offsite, to protect adjacent downstream lands from migration of sediment in overland flow.
 The location of this fencing will be adjacent to the limit of grading. Silt fence attached to paige wire fencing
 will be installed periodically throughout the Site adjacent to sensitive areas. Silt fencing should be erected
 before grading begins to protect adjacent and downstream areas from migration of sediment in overland
 flow.
- Storm service outlets will be installed during servicing and roadworks construction to provide lot level dead and live storage where appropriate.



Erosion and Sediment Control

- Erosion control berms/swales will be located in appropriate (critical) areas to divert flows to temporary sediment basins.
- A construction entrance feature ("mud-mat") will be provided at all site entrances to minimize the offsite transport of sediment via construction vehicles.
- Runoff will be directed to a temporary sedimentation facility via swales to minimize untreated runoff discharged from the Site.
- The temporary sedimentation facility should not be sited in the location of the proposed permanent SWM Facility as it may inhibit the function of the final SWM Facility as an infiltration basin.
- Swales constructed onsite will have temporary rock check dams to help attenuate flows and encourage deposition of suspended sediment where appropriate.
- All disturbed areas where construction is not expected for 30 days shall be re-vegetated with 50 mm of topsoil and hydro-seeding according to OPSS 572.
- During construction, all catchbasins are to be sealed until roads are paved to prevent sediment deposition in the catchbasins' sumps and conveyance of silt to the SWM Facility.
- An Erosion Control Implementation Schedule will be included with the Detailed Erosion and Sedimentation Control Plan, prepared in conjunction with the pre-grading application and/or final engineering design.
- Following completion of construction and site stabilization, all erosion and sediment control measures and accumulated sediment are to be removed.

Infiltration facilities are particularly vulnerable to failure during the construction phase for two reasons. First, if the construction sequence is not followed correctly, construction sediment can clog the facility. In addition, heavy construction can result in compaction of the soil which can then reduce the soil's infiltration rate. For this reason, adequate erosion and sediment controls upstream of the infiltration facility and soak-away pits as well as a careful construction sequence will need to be implemented. This will be developed at detail design prior to construction.

The erosion control measures shall be maintained in good repair during the entire construction period and shall only be removed as contributing drainage areas are restored and stabilized. In addition, the condition of erosion control works, their overall performance, and any repairs, replacement, or modifications to the installed item shall be noted in the Monitoring Reports submitted to the GRCA and the Township. The Monitoring Reports should be submitted bi-monthly (quarterly during periods of inactivity or house construction) and should be based on inspection completed bi-weekly or after any significant rainfall events (>13 mm), whichever is more frequent.



Erosion and Sediment Control

6.3 MONITORING, MAINTENANCE AND MITIGATION

Monitoring and maintenance activities are an important part of a SWM Plan to ensure that the designed features continue to operate as intended. A Monitoring Program should be established in consultation with the Region of Waterloo, Township of North Dumfries, and the Ministry of Environment, Conservation and Parks and incorporated into the Final Stormwater Management Plan at the detailed design stage.



Utilities

7.0 UTILITIES

7.1 GRANDBRIDGE ENERGY

Grandbridge Energy stated that they have 3-phase power that runs along Cedar Creek Road. These services will be extended to service the subject lands, therefore, there are no constraints for providing hydro service to the proposed development.

7.2 BELL CANADA

Bell has an existing fibre ped on the opposite side of Earl Thompson with conduit crossing that goes down Earl Thompson. These services will be extended to service the subject lands, therefore, there are no constraints for providing Bell service to the proposed development.

7.3 ROGERS CABLE

Rogers has aerial fiber along Earl Thompson Road as well as having aerial fiber on the South side of HWY 97/Cedar Creek Road. Service for the subject lands would be provided off Earl Thompson Road; therefore, there are no constraints for providing Bell service to the proposed development.

7.4 ENBRIDGE

Enbridge has indicated that gas is currently located within the neighborhood. Once a demand for the future industrial lots is determined, a capacity review will need to be undertaken.

7.5 UTILITY SUMMARY

Internal hydro services, Bell, Rogers cable lines and gas mains for the development would be buried in a joint trench within the Subject Plan.



Conclusions and Recommendations

8.0 CONCLUSIONS AND RECOMMENDATIONS

8.1 CONCLUSIONS

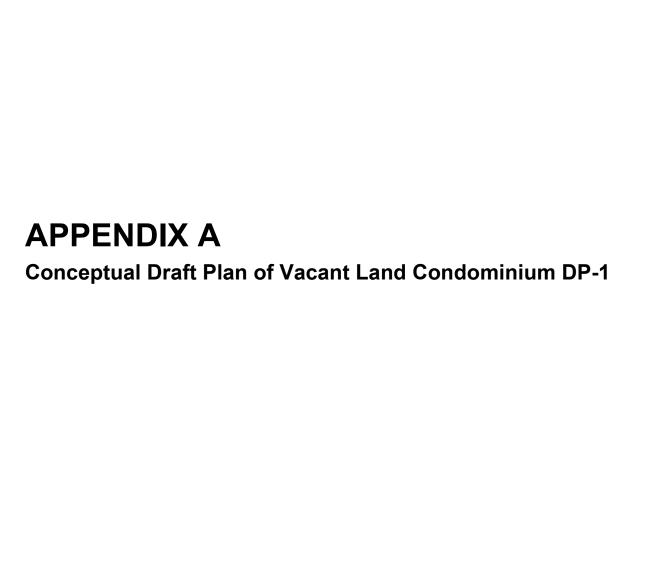
Based on the finding of this Report, it is concluded that:

- The proposed 2509 Cedar Creek Road can be adequately serviced by municipal sewage, storm drainage, water services and utilities.
- The proposed SWM features provides water quantity and water quality control for the proposed 2509 Cedar Creek Road industrial development.
- The proposed SWM Facility provides sufficient storage to attenuate post-development discharge to maintain existing target flow rates.
- Along with the end-of-pipe infiltration facility, lot level soak-away pits should be incorporated to infiltrate the
 first 25 mm of clean roof runoff where possible to help promote at-source infiltration across the Site and aid
 in groundwater recharge.

8.2 RECOMMENDATIONS

- This Report be circulated to the Municipalities and various approval agencies in support of Draft Plan of Subdivision Approval.
- Detailed grading and servicing design drawings be prepared, a Final Stormwater Management Report and Erosion Settlement Control Plan be completed once the Draft Plan of development for 2509 Cedar Creek Road has been approved to support construction.







APPENDIX B

Existing Conditions Plan C-050

Preliminary Profiles Plan C-200, C-201 & C-202

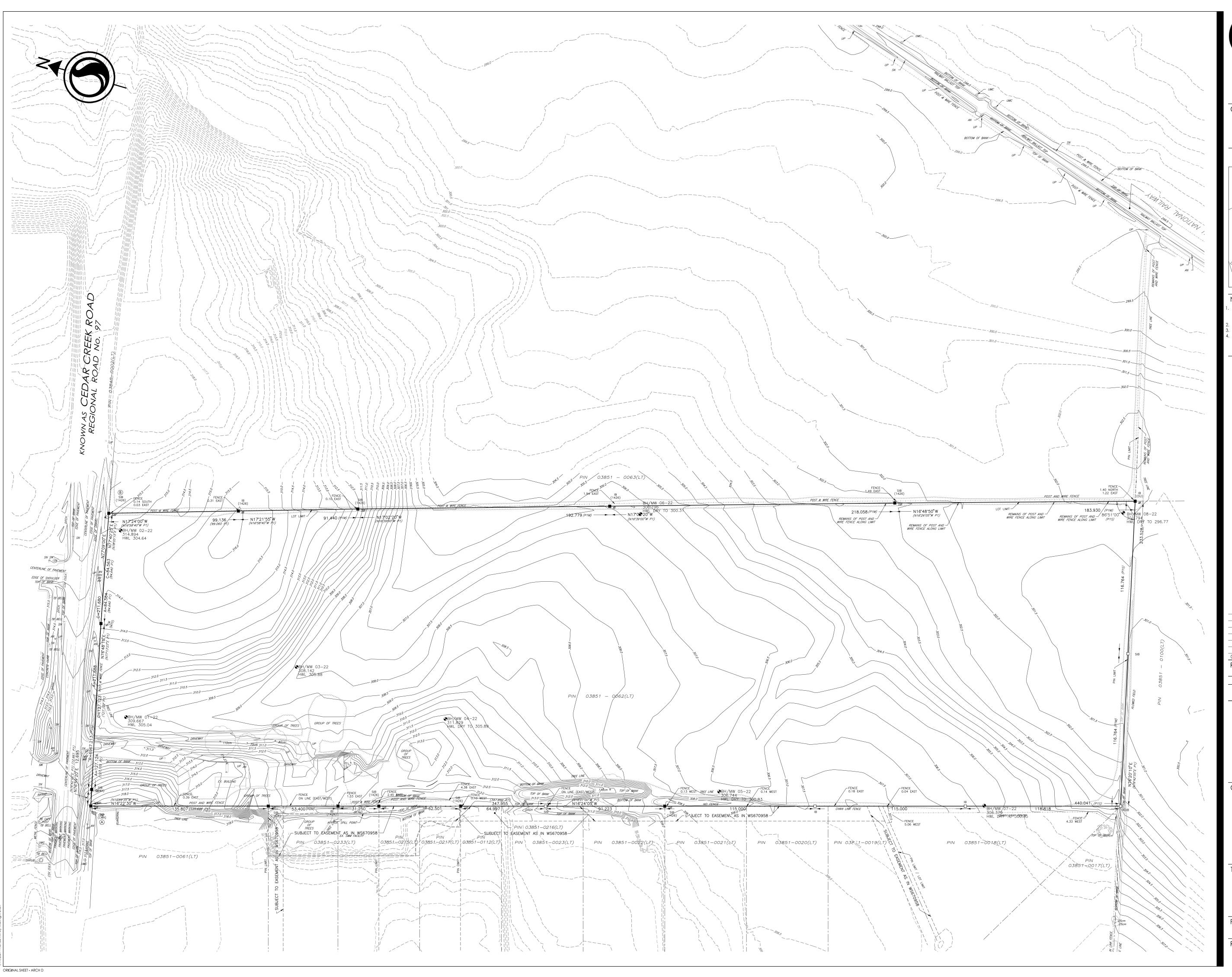
Preliminary Servicing and Grading Plan C-400, C-401 & C-402

Prelim. Grading Plan Outlet Ditch Sta 0+000 To 0+320, C-403

Prelim. Grading Plan Outlet Ditch Sta 0+320 To End, C-404

Stormwater Management Facility Plan C-410

Preliminary Cut/Fill Plan C-900





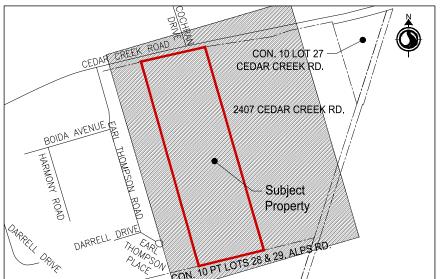
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Notes

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 DRAFT PLAN PREPARED BY STANTEC CONSULTING LTD., DATED JANUARY 2024.
 CALCULATED PLAN PREPARED BY STANTEC CONSULTING LTD., DATED JANUARY 2024.
 TOPOGRAPHICAL SURVEY PREPARED BY STANTEC CONSULTING LTD., DATED APRIL 2022. ADDITIONAL TOPOGRAPHICAL INFORMATION BY STANTEC CONSULTING LTD., DATED MAY 2022 AND JUNE 2022.

Legend

	EXISTING
PROPERTY LINE	
existing contour	305.0
CONTOUR (M.N.R.F LIDAR 2018)	305.0- IDENT
BOREHOLE/MONITORING WELL (WITH GROUND ELEVATION, AND HIGH WATER LEVEL)	H ⊕BH/MW 02-22 314.894 HWL 304.64
TREES	O/o
EASEMENT	
UTILITY POLE	UP_{\circ}
FENCE	— × — ×
existing dripline	
EXISTING DITCH	
existing storm/culve	RT⊁
existing sign	→ <i>SN</i>
EXISTING ANCHOR	AN
existing gas marker	[®] UMG
STANDARD IRON BAR	□ <i>SIB</i>
Iron bar	■ /B

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CEDAR CREEK ROAD HOLDINGS INC.

2509 CEDAR CREEK ROAD, AYR

TOWNSHIP OF NORTH DUMFRIES, ON

Title

EXISTING CONDITIONS PLAN

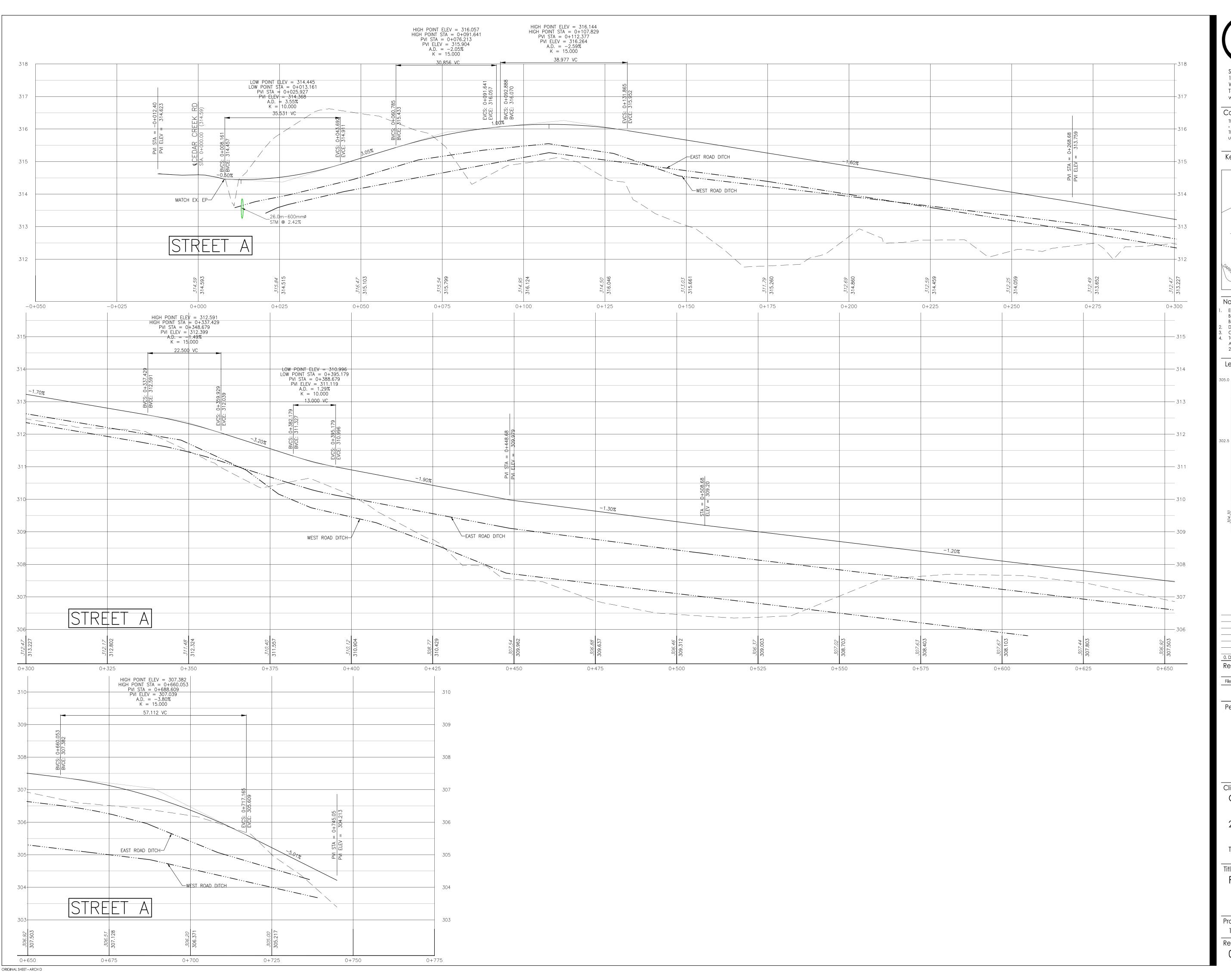
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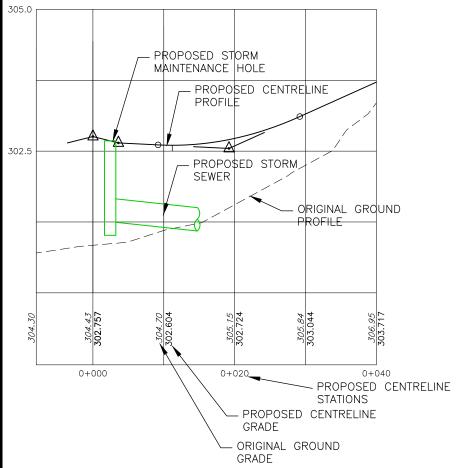
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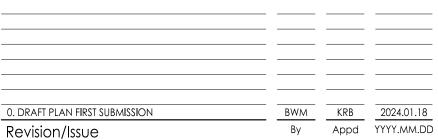
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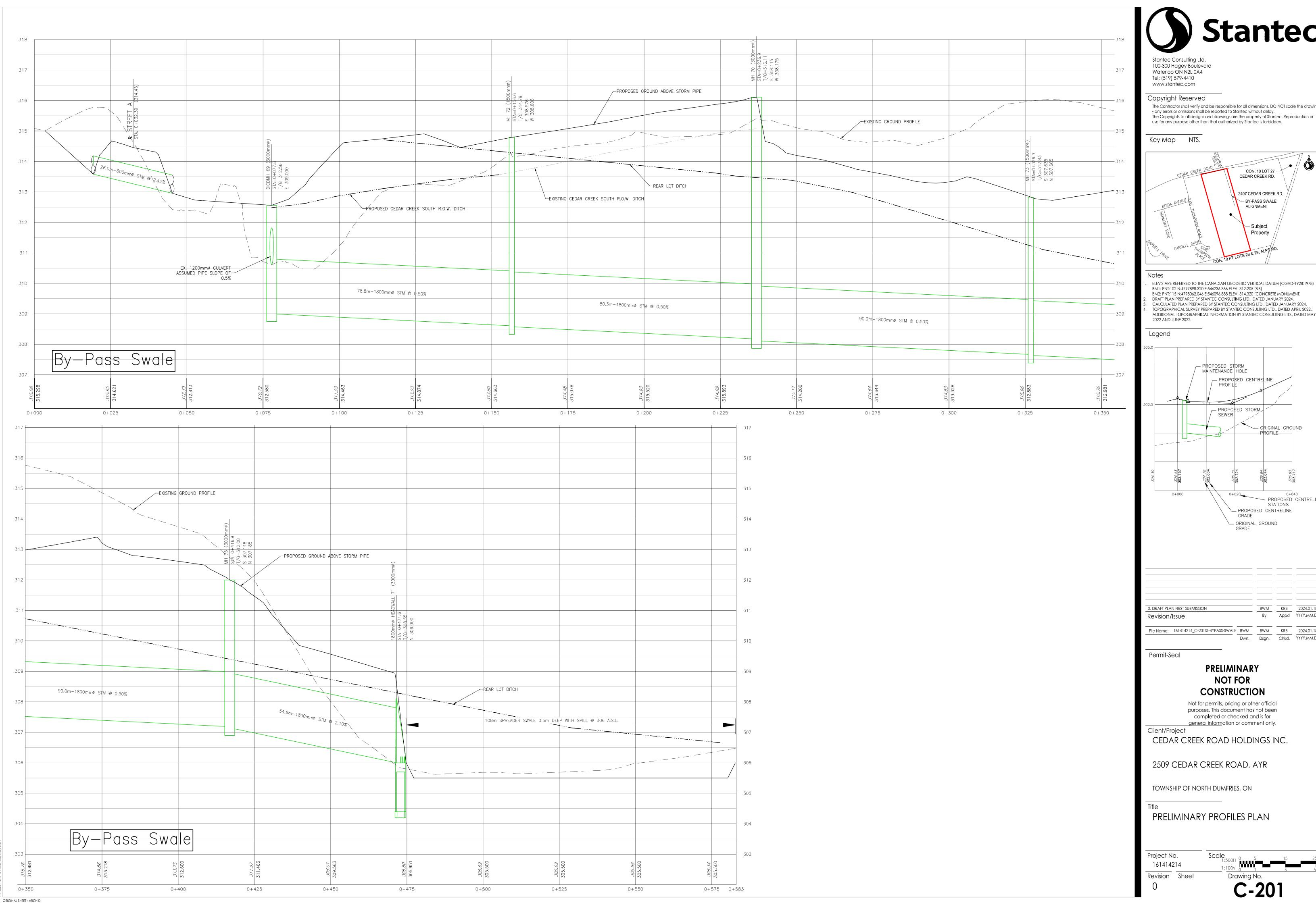
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PRELIMINARY PROFILES PLAN

Project No. 161414214 Revision Sheet

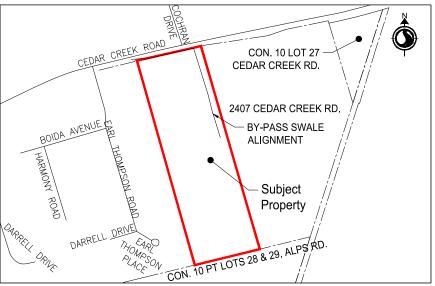




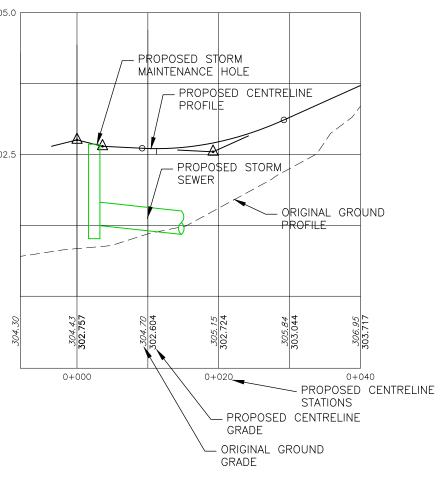
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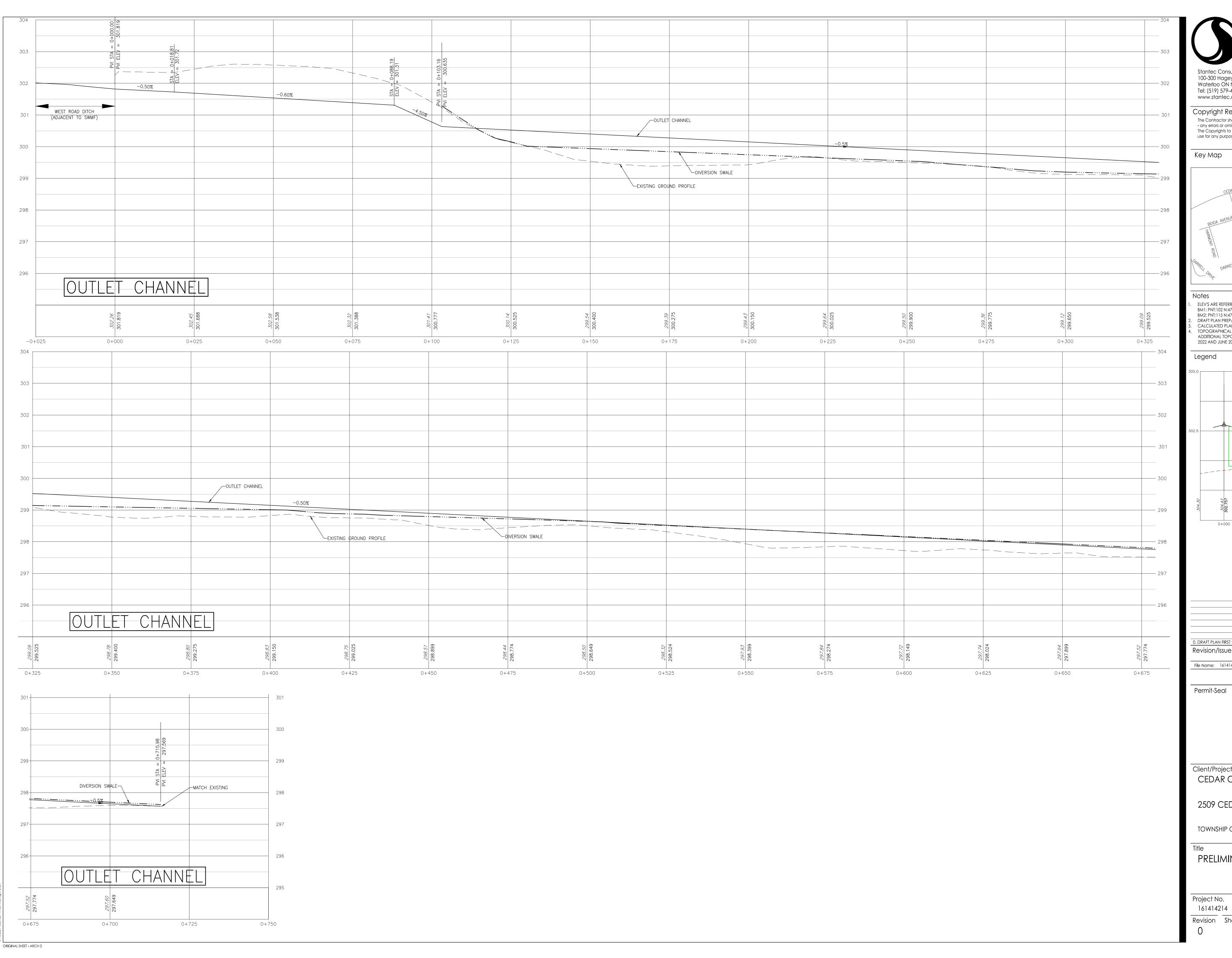
CEDAR CREEK ROAD HOLDINGS INC.

2509 CEDAR CREEK ROAD, AYR

TOWNSHIP OF NORTH DUMFRIES, ON

PRELIMINARY PROFILES PLAN

Project No. 161414214 Revision Sheet

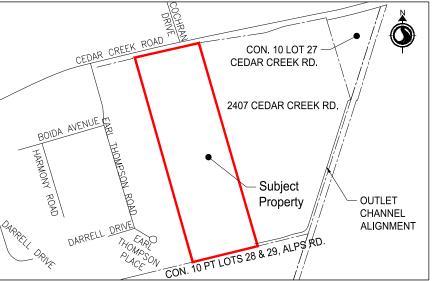




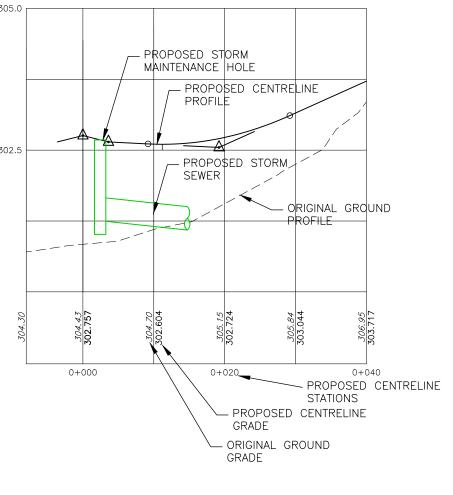
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Key Map NTS.



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 File Name:
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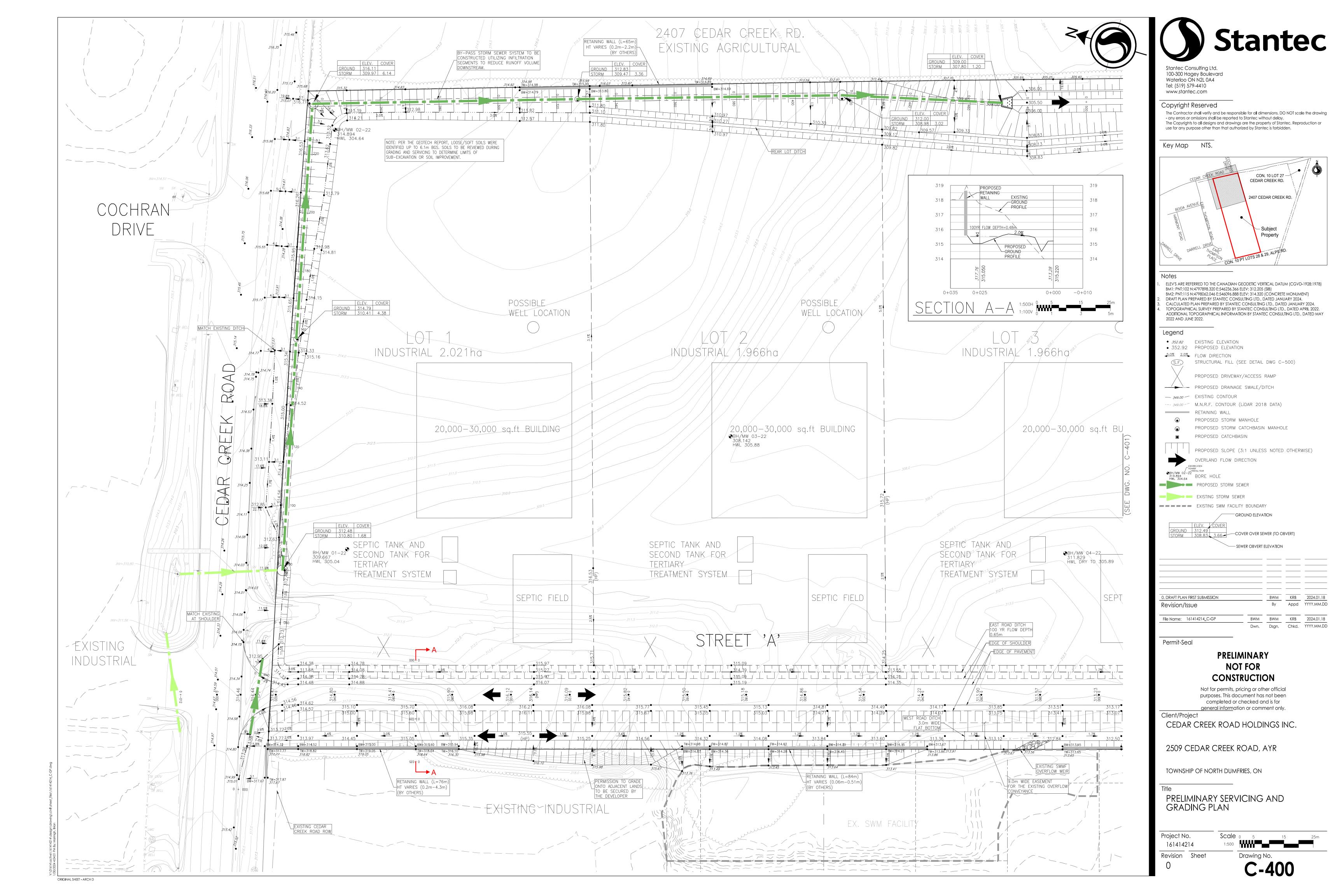
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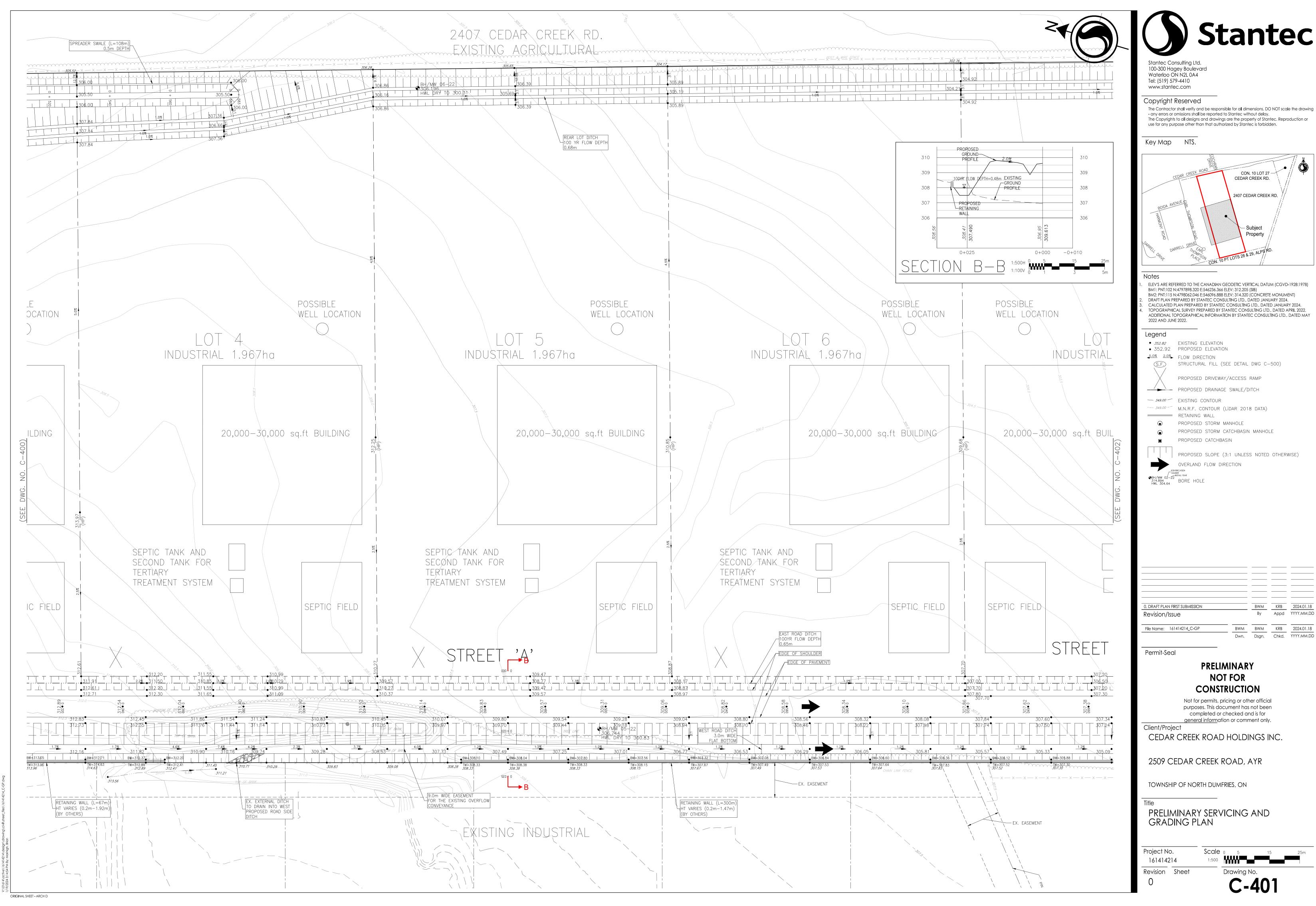
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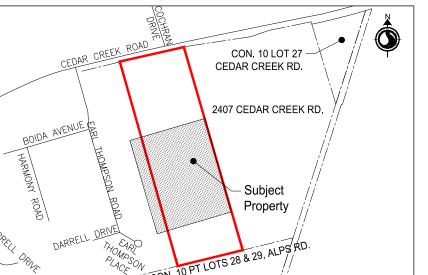
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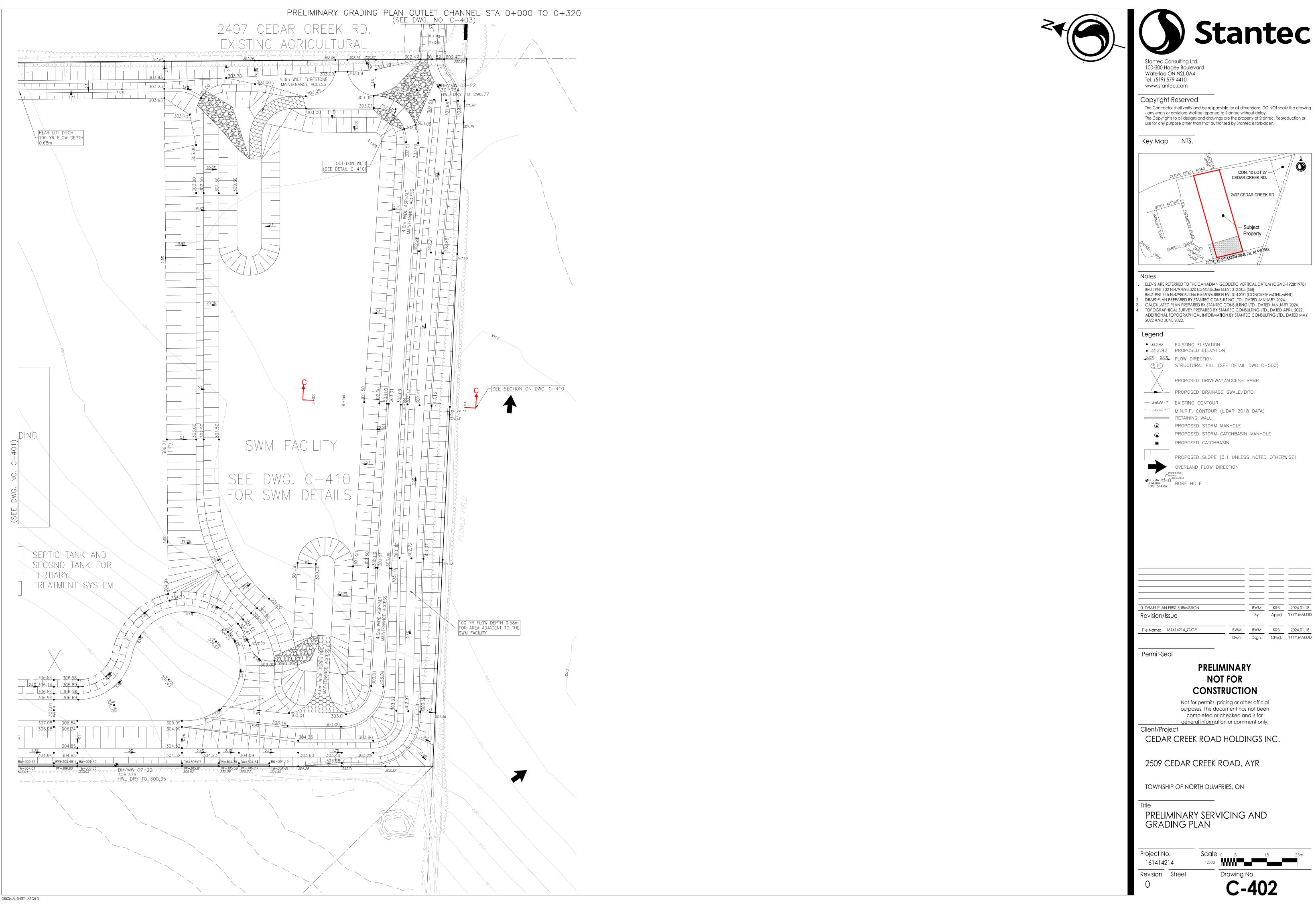




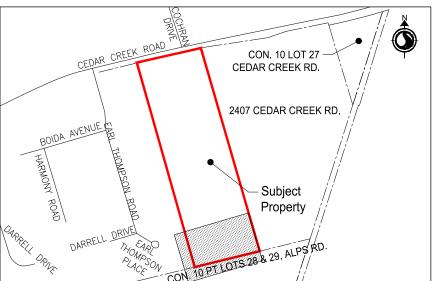


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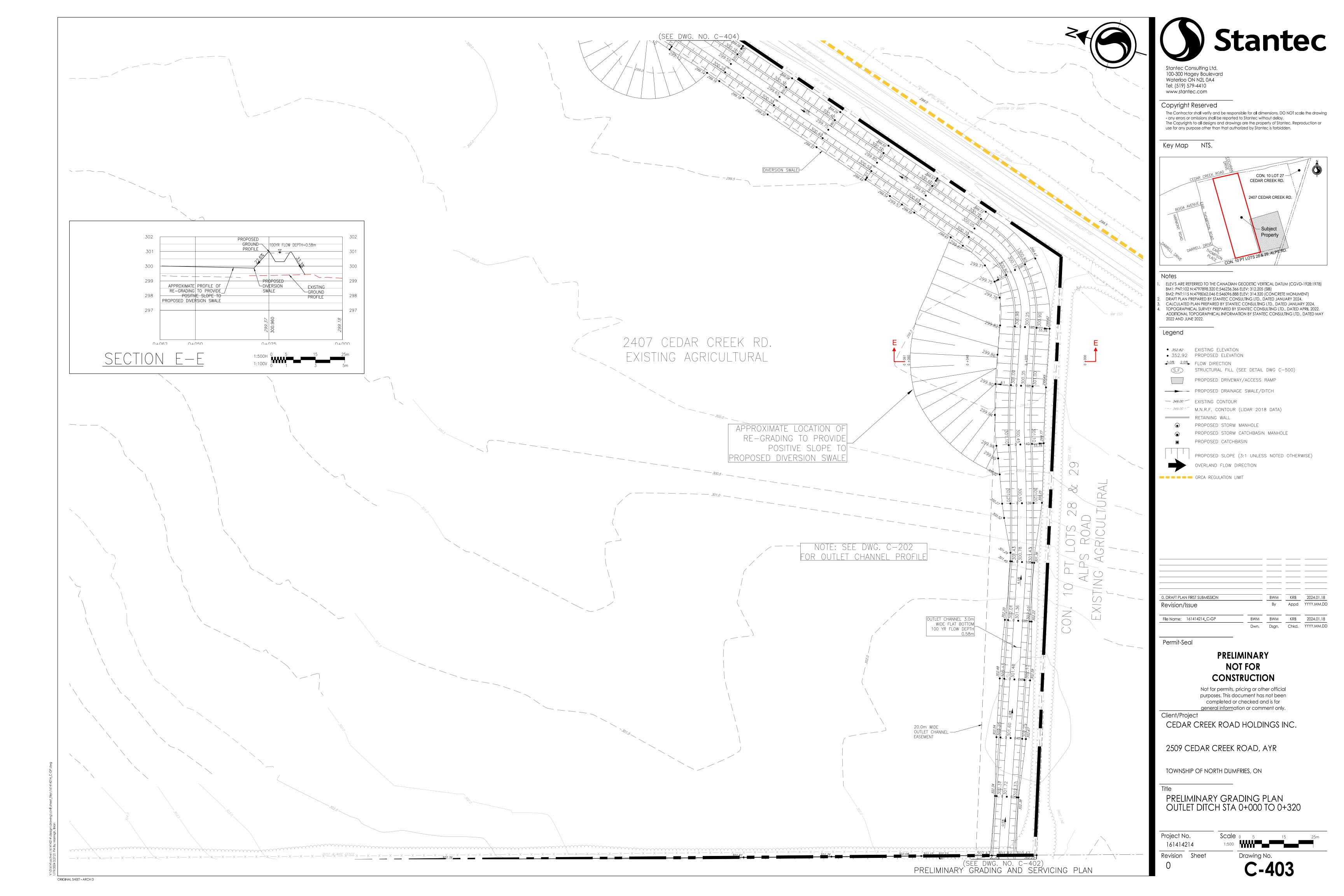


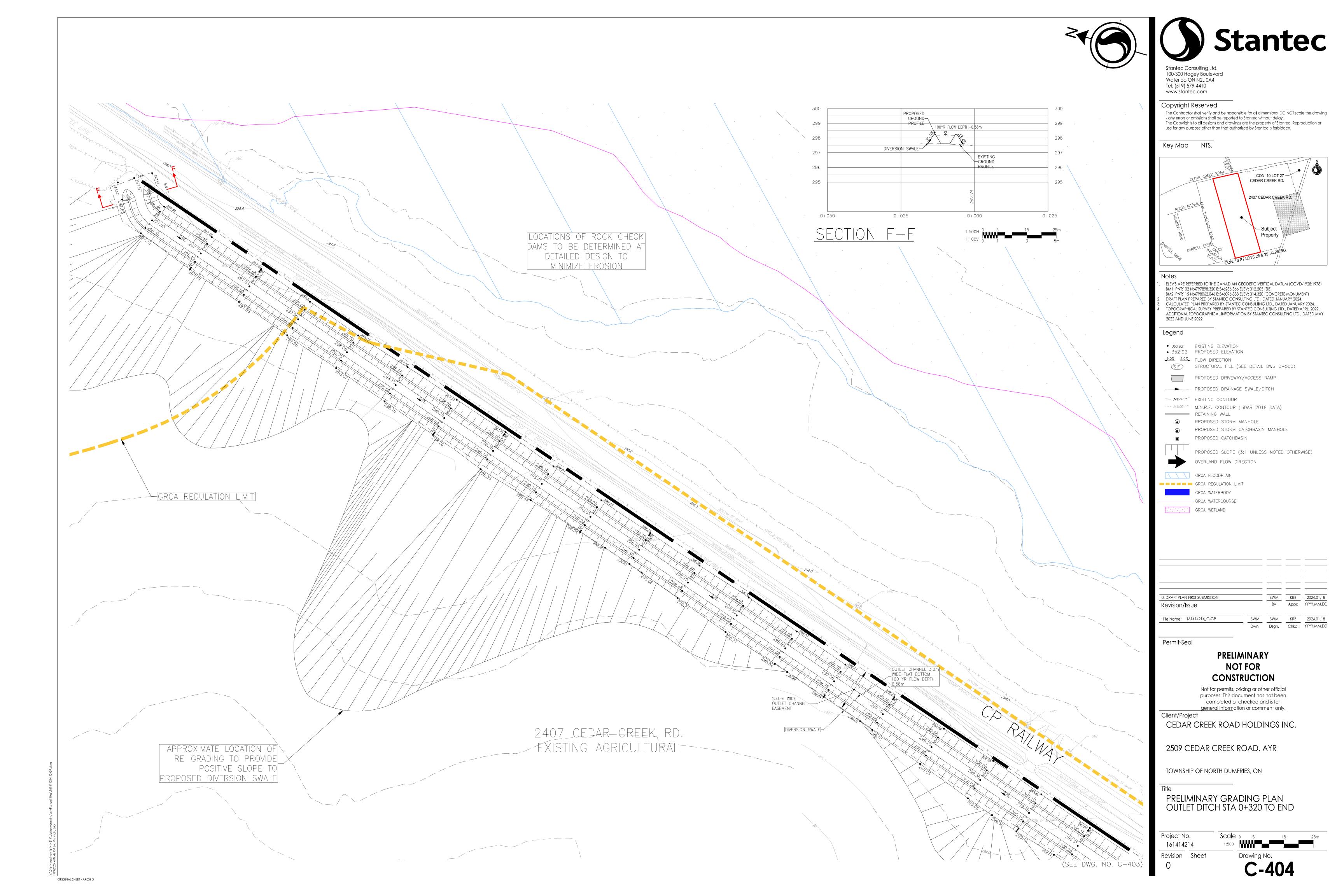
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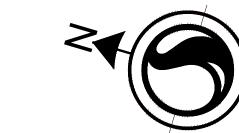
PROPOSED SLOPE (3:1 UNLESS NOTED OTHERWISE)

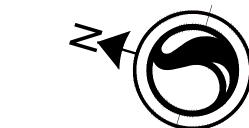
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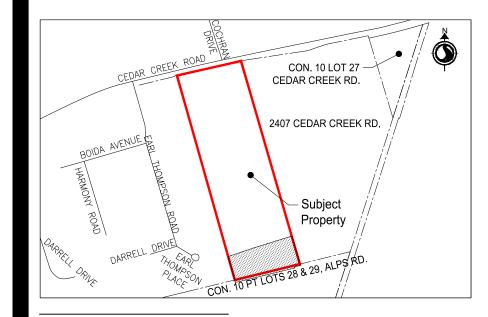




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• 352.82 EXISTING ELEVATION • 352.92 PROPOSED ELEVATION

5.0% 2.0% FLOW DIRECTION (S.F.) STRUCTURAL FILL (SEE DETAIL DWG C-500)

PROPOSED DRAINAGE SWALE (SEE DETAIL DWG C-500) — 349.00 — EXISTING CONTOUR

PROPOSED SLOPE (3:1 UNLESS NOTED OTHERWISE) OVERLAND FLOW DIRECTION

D. DRAFT PLAN FIRST SUBMISSION

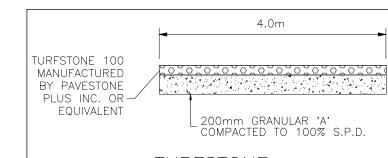
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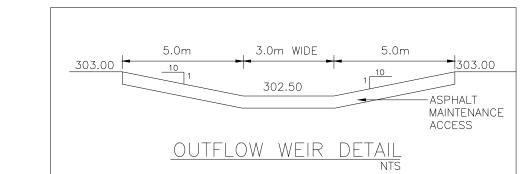
Permit-Seal

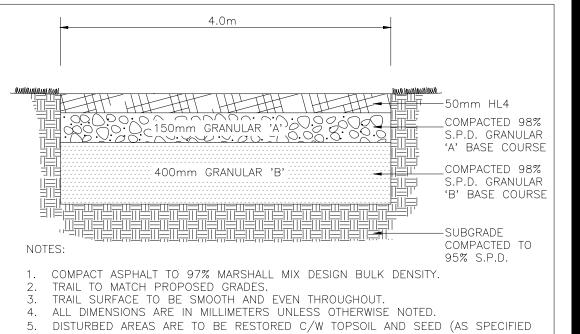
RETAINING WALL





TURFSTONE

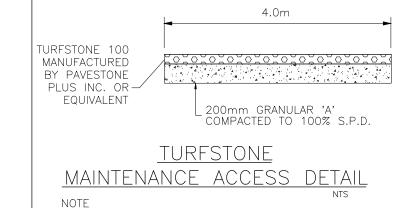




IN THE LANDSCAPE PLANS). TOPSOIL IS TO BE FINE GRADED AND BOX SCRAPPED WITH ALL AREAS HAVING POSITIVE DRAINAGE.

6. MINIMUM 10.0m RADIUS
7. MAX SLOPE 10:1 ASPHALT MAINTENANCE ACCESS/WALKWAY DETAIL

	300.30
POND BOTTOM (FOREBAYS)	300.30
POND BOTTOM (INFILTRATION CELL)	301.50
QUALITY EXTENDED DETENTION (25mm)	301.83
2 YEAR WATER LEVEL	301.90
5 YEAR WATER LEVEL	302.24
100 YEAR WATER LEVEL	302.69
REGIONAL WATER LEVEL	302.85



-MIN. RADIUS TO BE 10.0m (11.5m CENTERLINE)
-MAX. SLOPE TO BE 10:1
-TURFSTONE AND PERMEABLE PAVER TO BE INSTALLED IN
ACCORDANCE WITH MANUFACTURERS RECOMMENDATIONS

CEDAR CREEK ROAD HOLDINGS INC. 2509 CEDAR CREEK ROAD, AYR TOWNSHIP OF NORTH DUMFRIES, ON

STORMWATER MANAGEMENT FACILITY PLAN

Project No. 161414214 Drawing No. Revision Sheet

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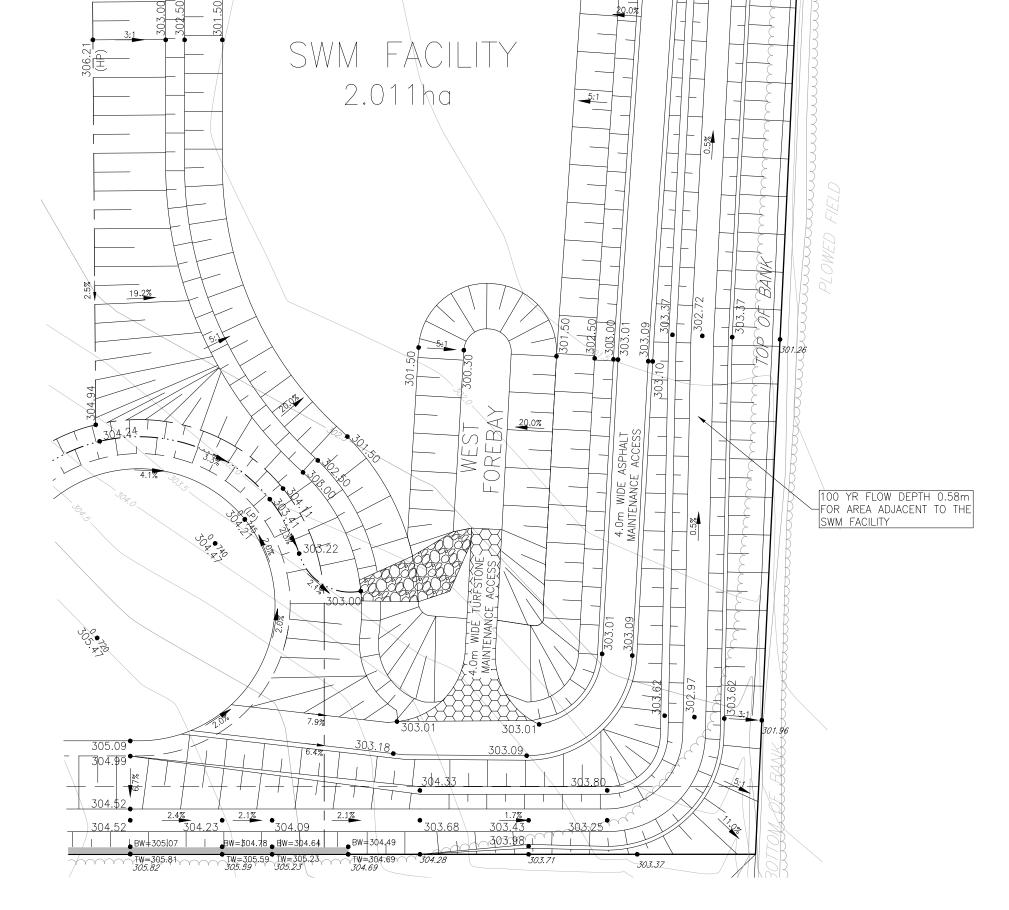
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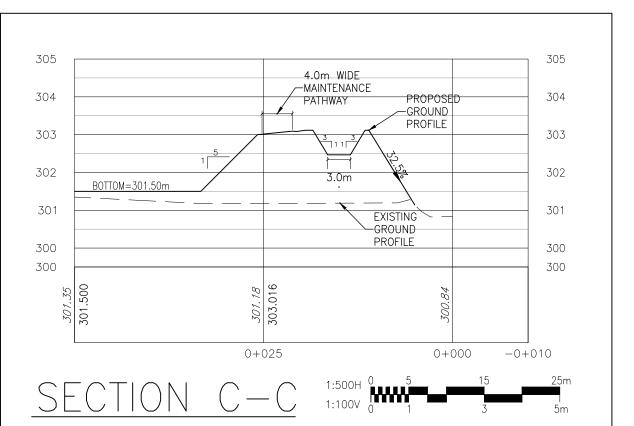


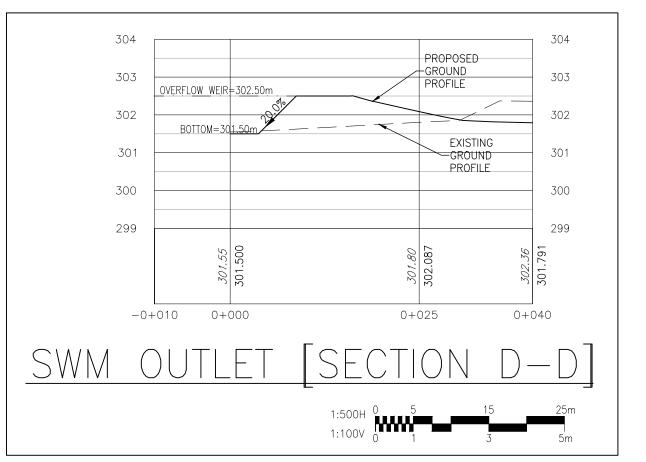
2407 CEDAR CREEK RD.

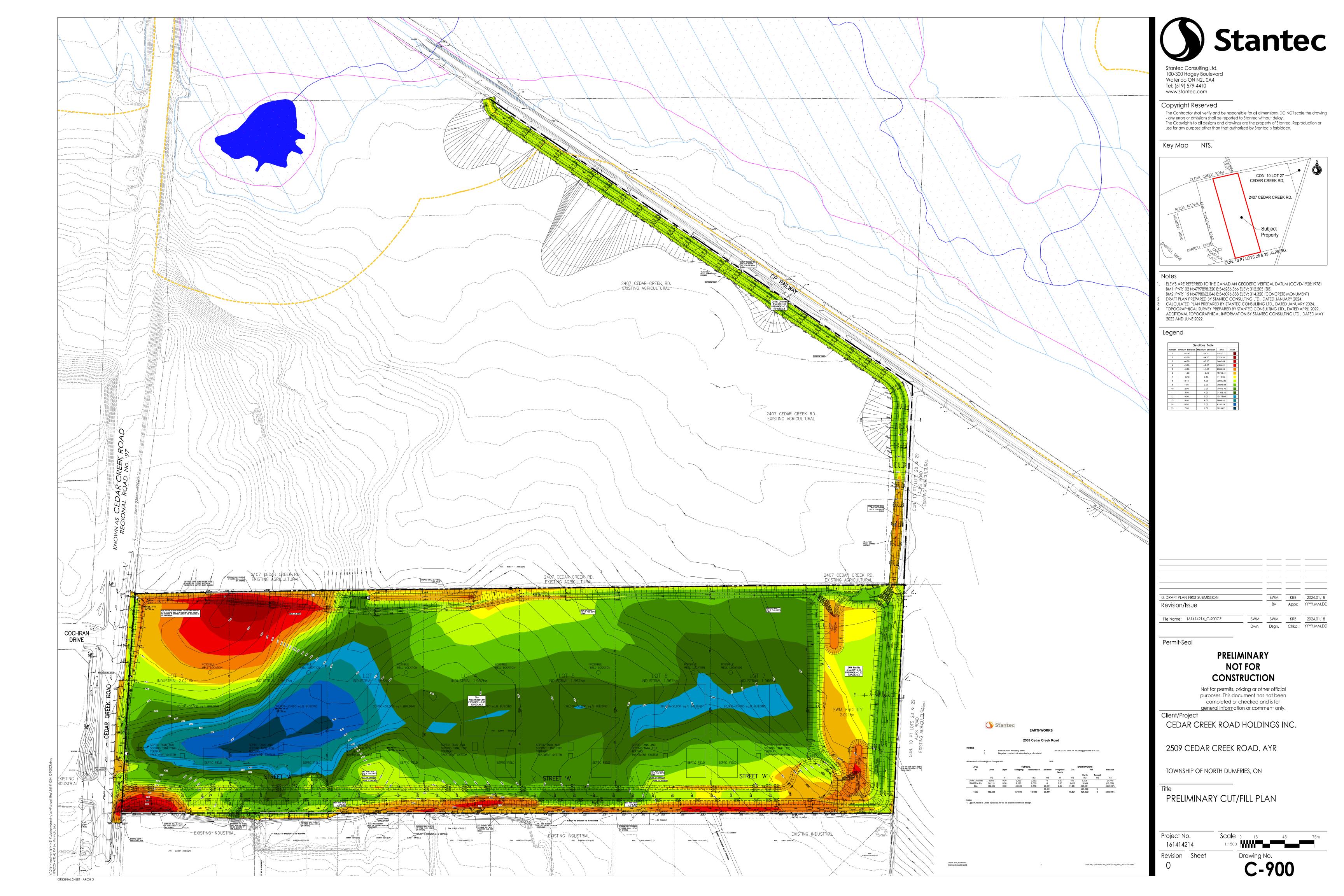
EXISTING AGRICULTURAL

4.0m WIDE TURFSTONE
MAINTENANCE ACCESS

(SEE DETAIL C-410)







APPENDIX C

2509 Cedar Creek Road, Ayr ON - Water and Sewage System Feasibility Study Dated January 24, 2024

APPENDIX C – WATER AND SEWAGE SYSTEM FEASIBILITY STUDY

From:



Memo

To: Kevin Brousseau, L.E.T., C.E.T.

Jean Hébert, P. Eng.

Principal, Practice Leader - Community

Stantec Ottawa Office

Development

Stantec Waterloo Office

Project/File: 1614-14214

Date: January 24, 2024

Reference: 2509 Cedar Creek Road, Ayr ON - Water and Sewage System Feasibility Study

Our review of the underground water conditions and land available at the seven proposed industrial lots at 2509 Cedar Creek Road concluded that the potential number of employees per site would vary from 24 to 84, depending on the soils characteristics at a given lot, and on the type of sewage treatment retained (conventional septic system or tertiary treatment system) by the landlord. In summary, the tertiary treatment system would allow an increase in serviced population (by about one half), compared to the conventional septic system, and would depend on the location of the commercial lot, as per the following chart.

Lot No.	1	2	3	4	5	6	7
No of employees With conventional septic system	37	37	24	37	56	56	56
No of employees With tertiary treatment system	59	59	40	59	84	84	84

The above is developed on the assumption that the absorption area, including the septic field, and an infiltration gallery for the drinking water system process wastewater, are to be set within a 20 m by 30 m area.

To support higher number of employees at a given commercial lot, the landowner would have to allocate more room for the absorption area, which implies allocating less room for the building and/or the parking space.

Best regards,

STANTEC CONSULTING LTD.

P.Eng. (ON) PEO No. 90272949

Jean Hébert P.Eng.

Senior Environmental Engineer

Phone: (613) 725-5562 Mobile: 613-294-4264 jean.hebert@stantec.com

APPENDIX C-1 – Septic System Assessment Methodology

The serviced population has been established based on daily design sewage flow rates and septic system design parameters as per the Ontario Building Code – Part 8 – Septic Systems, hereafter referred to as the OBC, as follows.

- Flow rate per employee per 8-hour shift = 75 L/d per employee

- Flow rate per toilet accessible to truckers = 950 L/d/toilet

Office building: allocate one employee per 9.3 m² (100 sq. ft) = 75 L/d per employee

Soils characteristics have been assessed from well record datasheets for wells located north and west of the proposed commercial sites, available at https://www.ontario.ca/page/map-well-records

The time of percolation, i.e., the number of minutes for water to travel by one cm into the soils, has been deduced for each of the future lots, based on the type of soils at the nearby wells. That information will be updated prior to detailed design phase, using data from geotechnical and hydrogeological reports to be issued by Stantec.,

The theoretical time of percolation, as reported in the following table, extracted from Table 2-8 of the Sewerage System Standard Practice Manual (Version 2) prepared by the British Columbia Onsite Sewage Association, and from Supplementary Standard SB-6 (Percolation Time and Soil Descriptions) from the Government of Ontario's On-Site Sewage Systems Regulations, is deemed to be relatively conservative. On-site percolation tests <u>would have to be conducted</u> prior to detailed design phase, to validate those values, although the actual value could be slightly better (i.e., water may flow faster). Table 1 on next page presents the percolation time for different types of soils.

The OBC includes various options for private sewage disposal systems. The conventional septic system consists of a two-compartment septic system, followed by a septic bed, fed either by gravity (should site topography allows it) or with an effluent pump. The gravity system is the most economical where soils consist of sand, as it is the case at most of the industrial lots; however, requires the largest septic field footprint.

The tertiary system is an advanced treatment system with a modified septic tank, used as a digester, followed by a biofilter tank, a recirculation pump, and an effluent pump feeding a modified septic field. The treatment process normally occurs within the septic field; with a tertiary system the treatment process, would be accommodated in the modified septic tanks, with the final septic field footprint reduced up to one third in size. This would allow for an increase in the number of employees at a given industrial lot, for the same septic field footprint.

Septic field can be positioned as close as 3.0 m from the property limit, so the septic field could be set much closer to the property limit than shown on the typical arrangement sketch on Drawings C-400 to C-401.

Table C-1: Estimated Percolation Rate based on Soil Type

Soil Type	Percolation Rate (min/cm)
Sand	7
Silty Sand	14
Sandy Silt	28
Silt	28
Fine silt	28
Clayed sand	35
Clayey Silt	35
Silty Clay-Silt	35
Sandy Clay	35
Silty Clay	35
Clay	35

Office wastewater normally has ammonia concentration about 50% higher than typical residential wastewater, as it cannot rely on dishwasher, shower, and source of wastewater other than toilets and sinks to dilute sewage water. The septic field area is based on final ammonia disposal. For such reasons, the septic field area for an industrial building should be increased by 50%, compared to the result obtained while applying OBC design rules, which were developed for residential housing.

Process wastewater generated by various well water treatment equipment (iron filter, water softener, reverse osmosis) could be disposed of at an infiltration gallery, at a rate of 100 L/m²/d. The nature of such process wastewater for this case is reviewed under Appendix C-2.

Horizontal gap (spacing) between infiltration gallery and septic field should be minimum 5 m, to avoid interference between both systems. Figure C-1 on next page shows how the infiltration gallery and the septic field could be set within a 20 m by 30 m absorption area:

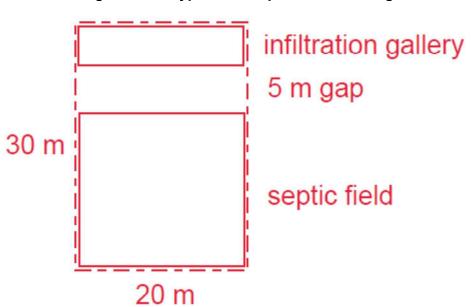


Figure C-1 – Typical Absorption Area Setting

Any lot with combined flow rate (sewage flow and process wastewater flow) below 10,000 L/d is to be subject to approval by local authority, while any lot with higher daily flow rate would imply an application to the Ontario Ministry of the Environment, Conservation and Parks (MECP). This corresponds to 54 employees, at 75 L per 8-hour shift each, plus one trucker toilet at 950 L per day.

For reference, typical precast concrete septic tanks in Ontario are designed and fabricated for a one-meter burial depth, measured from the top of the slab to the highest ground surface elevation, above the tank and up to 5 meters measured horizontally from the tank exterior walls. Special order tanks designed for two-meter burial depth, measured above tank and up to seven meters from the tank wall, are available upon request, with an additional cost below \$2,000 per tank. This safety parameter applies to ground surface usage, i.e., that no vehicle, and particularly no commercial truck, shall be allowed to drive over within the above-defined limits. The issue is that the vehicle load distributed by the soils would impact the tank walls, at the risk of exceeding the wall strength.

APPENDIX C-2 – Site Specific Conditions

Here are the site-specific conditions affecting the septic system capacity assessment.

Drawings C-400 to C-402 show the proposed building, septic tank and septic field setting at Lot no. 1 to Lot 7.

Most of the site is to be occupied by a parking lot, and office building approximately 1,858 to 2,787 m² range (20,000 to 30,000 ft²).

A location allocated to support an absorption area of 20 m by 30 m would be required. This area would include a reverse osmosis concentrate disposal gallery (refer to discussion below) and the septic field (downstream either a conventional septic system tank or a tertiary treatment system group of tanks). The inclusion of an infiltration gallery will be required, on the following basis.

From **Table 2** - Summary of Groundwater Analytical Results - Hydrogeological Investigation in Support of Official Plan and Zoning Bylaw Amendments Site: 2509 Cedar Creek Road, Ayr ON, at the end of this Appendix C-2, well water in the local aquifer have chloride, hardness, sodium, iron and total dissolved solids considerably above aesthetic limit, which would require water to be treated with a water softener and a reverse osmosis filter, followed by calcium carbonate contact vessel to reduce filtered water corrosiveness. Depending on well water quality, an iron filter may be required. Such treatment process implies that, for every liter of drinking water produced, about 1.3 liter of process wastewater would be generated as follows: 1 L of concentrate from the reverse osmosis filter, continuously during water production, 0.15 L for iron filter backwash overnight, and 0.15 L brine regeneration volume overnight at the water softener. This process wastewater should be directed to an infiltration gallery, separated from the septic field, as there is practically no organic loading in that water. Such gallery would be part of the 20 m X 30 m absorption area, as shown on **Figure C-1** above.

Drawings C-400 to C-402 show the proposed absorption field (including the septic field, the infiltration gallery for process wastewater, and 5-m gap in between) located toward the front end of the industrial lot. Should gravity flow installation from the building sewer to the septic tank then to the absorption field be unachievable, a pump would be required to convey either raw sewage to the septic tank or septic tank effluent to the septic field.

An alternative to avoid installing such pump(s), the septic tank and the absorption field could be installed toward the back of the industrial sites, as ground surface generally slopes down, as shown on Drawings C-400 to C-402. This configuration implies to set the well at the front of the

lot, and to configure the parking lot around the septic tank and septic field, considering the later should be at least 15 meters from the top of the drainage ditch.

About the infiltration gallery:

The reverse osmosis concentrate is released on a continuous basis during water production process, while the iron filter backwash water and water softener brine are released at high flow rates, for a few minutes at a time. Those process wastewater would need an equalization tank and pumping system, to dose such water at a lower flow rate to the infiltration gallery. Concentrate and brine may be collected into the same basin, while iron fitter backwash water would be collected into a separate tank, working as a clarifier. After a few hours of settling, clarified water would be pumped to the infiltration gallery, at a reduced flow rate. Iron sludge at the bottom of the tank would be pumped out by a sewage vacuum truck on a year basis.

Absorption field and various tank locations, with required protection perimeters, would be reviewed at detailed design phase of each industrial lot, once final use, building size and the number of employees has been confirmed.

Table 2
Summary of Groundwater Analytical Results
Hydrogeological Investigation in Support of Official Plan and Zoning Bylaw Amendments Site: 2509 Cedar Creek Road, Ayr ON

Sample Location Sample Date			111 Earl Tho 13-May-22	mpson Road 13-May-22 WG-161414214-	121 Earl Thompson Road 13-May-22	13-May-22	Creek Road 13-May-22 WG-161414214-	13-May-22	Creek Road 13-May-22 WG-161414214-
Sample ID			WG-161414214- 20220513-SH3	20220513-SH3 Lab-Dup	WG-161414214- 20220513-SH2	WG-161414214- 20220513-SH4	20220513-SH4 Lab-Dup	WG-161414214- 20220513-SH1	20220513-SH1 Lab-Dup
Sampling Company			STANTEC	STANTEC	STANTEC	STANTEC	STANTEC	STANTEC	STANTEC
Laboratory			BV	BV	BV	BV	BV	BV	BV
Laboratory Work Order			C2D0478	C2D0478	C2D0478	C2D0478	C2D0478	C2D0478	C2D0478
Laboratory Sample ID			SPU232	SPU232	SPU231	SPU233	SPU233	SPU230	SPU230
Sample Type	Units	ODWS		Lab Replicate			Lab Replicate		Lab Replicate
General Chemistry		l			<u> </u>				
Alkalinity, Bicarbonate (as CaCO3)	mg/L	n/v	290	-	260	260	-	250	_
Alkalinity, Carbonate (as CaCO3)	mg/L	n/v	2.8	-	2.2	2.8	-	2.7	-
Alkalinity, Total (as CaCO3)	mg/L	30-500 ^E	300	300	270	260	-	250	-
Ammonia (as N)	mg/L	n/v	<0.050	-	<0.050	<0.050	-	<0.050	<0.050
Anion Sum	me/L	n/v	21.7	-	54.1	8.24	-	7.81	_
Cation Sum	me/L	n/v	22.5	-	55.1	8.48	-	8.12	-
Chloride	mg/L	250 ^c	520 ^C	-	1,700 ^c	54	-	40	-
Dissolved Organic Carbon (DOC)	mg/L	5 ^c	0.71	-	0.56	0.47	-	<0.40	-
Electrical Conductivity, Lab	µmhos/cm	n/v	2,400	2,400	6,100	810	-	760	<u>-</u>
Hardness (as CaCO3)	mg/L	80-100 ^E	590 ^E	-	870 ^E	350 ^E	-	360 ^E	-
Ion Balance	%	n/v	1.74	-	0.880	1.43	-	1.90	-
Langelier Index (at 20 C)	none	n/v	1.09	_	1.01	1.01	-	0.995	_
Langelier Index (at 4 C)	none	n/v	0.843	-	0.772	0.759	-	0.747	-
Nitrate (as N)	mg/L	10.0 _d ^B	3.69	-	0.97	5.97	-	7.06	-
Nitrite (as N)	mg/L	1.0 _d ^B	<0.010	_	<0.010	<0.010	_	<0.010	_
Orthophosphate (as P)	mg/L	n/v	0.012	_	<0.010	<0.010	<u>-</u>	<0.010	_
pH, lab	s.u.	6.5-8.5 ^E	8.01	8.03	7.95	8.07	_	8.06	_
Saturation pH (at 20 C)	none	n/v	6.92	_	6.93	7.06	_	7.06	_
Saturation pH (at 4 C)	none	n/v	7.17	_	7.18	7.31	_	7.31	_
Sulfate	mg/L	500 _h c	42	_	58	53	_	55	_
Total Dissolved Solids (Calculated)	mg/L	500 ^c	1,200 ^c	_	3,100 ^c	460	_	440	_
Total Suspended Solids	mg/L	n/v	2	2	2	1	_	<1	_
Microbiological Analysis	1 0	•	•		•			•	
Escherichia coli (E.Coli)	cfu/100mL	0 ^A	0	-	0	0	-	0	_
Total Coliform Background	cfu/100mL	n/v	0	_	0	17	_	0	_
Total Coliforms	cfu/100mL	0 ^A	0	_	0	1 ^A	-	0	<u>-</u>
Metals	•	•	•		!			•	
Aluminum	mg/L	0.1 ^E	<0.0049	_	<0.0049	0.0077	0.0055	0.0093	_
Antimony	mg/L	0.006 ^B	<0.00050	_	<0.00050	<0.00050	<0.00050	<0.00050	<u>_</u>
Arsenic	mg/L	0.000	<0.0010		<0.0010	<0.0010	<0.0010	<0.0010	
Barium	mg/L	1 ^B	0.29	-	0.28	0.088	0.091	0.098	-
Beryllium	mg/L	n/v	<0.00040	_	<0.00040	<0.00040	<0.00040	<0.00040	_
Boron	mg/L	5 ^B	0.014	-	0.014	0.012	0.012	0.011	_
Cadmium	mg/L	0.005 ^B	<0.00090	_	<0.00090	<0.00090	<0.00090	<0.00090	<u>-</u>
Calcium	mg/L	n/v	150	-	230	96	97	98	_
Chromium	mg/L	0.05 ^B	<0.0050	<u> </u>	<0.0050	<0.0050	<0.0050	<0.0050	<u>-</u>
Cobalt	mg/L	n/v	<0.0050		<0.0050	<0.0050	<0.0050	<0.0050	
Copper	mg/L	10°	0.013		0.013	<0.00090	<0.00090	0.0010	
Iron	1	0.3 ^c	<0.10		0.11	0.35 ^C	0.35 ^c	<0.10	
	mg/L			_					_
Lead	mg/L	0.01 ^B	<0.00050	-	<0.00050	<0.00050	<0.00050 <0.0050	<0.00050	_
Lithium Magnesium	mg/L mg/L	n/v n/v	0.0070 50		0.013 74	<0.0050 26	<0.0050	<0.0050 29	
Manganese	mg/L	0.05 ^c	0.0037		0.0047	<0.0020	<0.0020	<0.0020	
Molybdenum	mg/L	n/v	<0.0050	-	0.00056	<0.0020	<0.0020	<0.0020	_
•	1		<0.00030	_		<0.00030	<0.00050	<0.00030	_
Nickel	mg/L	n/v		_	<0.0010				_
Phosphorus	mg/L	n/v	<0.10	-	<0.10	<0.10	<0.10	<0.10	-
Potassium	mg/L	n/v	2.3	-	4.1	1.2	1.2	1.5	-
Selenium	mg/L	0.05 ^B	<0.0020	-	<0.0020	<0.0020	<0.0020	<0.0020	-
Silicon	mg/L	n/v	6.2	-	6.6	5.9	5.9	6.5	-
Silver	mg/L	n/v	<0.000090	-	<0.000090	<0.000090	<0.000090	<0.000090	-
Sodium	mg/L	200 _g ^C 20 _g ^D	250 ^{CD}	-	860 ^{CD}	34 ^D	33 ^D	19	-
Strontium	mg/L	n/v	0.27	-	0.65	0.46	0.45	0.49	-
Thallium	mg/L	n/v	<0.000050	-	<0.00050	<0.000050	<0.000050	<0.000050	-

Notes:

ODWS Technical Support Document for Ontario Drinking Water Standards, Objectives and Guidelines (MOE, 2006), in support of O.Reg 169/03 (January 1, 2018)

- A Schedule 1 Microbiological Standards (expressed as a maximum)
- B Schedule 2 Chemical Standards (expressed as a maximum acceptable concentration)
- C ODWS Table 4 Chemical/Physical Objectives and Guidelines, Aesthetic Objectives
- ODWS Table 4 Medical Officer of Health Reporting Limit
- DDWS Table 4 Chemical/Physical Objectives and Guidelines, Operational Guidelines

6.5^A Concentration exceeds the indicated standard.

- 15.2 Measured concentration did not exceed the indicated standard.
- <0.50 Laboratory reporting limit was greater than the applicable standard.
- <0.03 Analyte was not detected at a concentration greater than the laboratory reporting limit.</p>
- n/v No standard/guideline value.
- Parameter not analyzed / not available.



Table 2
Summary of Groundwater Analytical Results
Hydrogeological Investigation in Support of Official Plan and Zoning Bylaw Amendments Site: 2509 Cedar Creek Road, Ayr ON

Sample Location			111 Earl Tho	mpson Road	121 Earl Thompson Road	2396 Cedar	Creek Road	2407 Cedar	Creek Road
Sample Date			13-May-22	13-May-22	13-May-22	13-May-22	13-May-22	13-May-22	13-May-22
Sample ID Sampling Company Laboratory Laboratory Work Order Laboratory Sample ID Sample Type	Units	ODWS	WG-161414214- 20220513-SH3 STANTEC BV C2D0478 SPU232	WG-161414214- 20220513-SH3 Lab-Dup STANTEC BV C2D0478 SPU232 Lab Replicate	WG-161414214- 20220513-SH2 STANTEC BV C2D0478 SPU231	WG-161414214- 20220513-SH4 STANTEC BV C2D0478 SPU233	WG-161414214- 20220513-SH4 Lab-Dup STANTEC BV C2D0478 SPU233 Lab Replicate	WG-161414214- 20220513-SH1 STANTEC BV C2D0478 SPU230	WG-161414214- 20220513-SH1 Lab-Dup STANTEC BV C2D0478 SPU230 Lab Replicate
- The sample type	01110	05.10		Zaz Hophoato			Zas Hophoato		
Titanium	mg/L	n/v	<0.0050	-	<0.0050	<0.0050	<0.0050	<0.0050	-
Uranium	mg/L	0.02 ^B	0.00066	-	0.00099	0.00042	0.00038	0.00051	-
Vanadium	mg/L	n/v	<0.00050	-	<0.00050	<0.00050	<0.00050	<0.00050	-
Zinc	mg/L	5 ^c	0.018	-	0.019	0.027	0.027	0.015	-

Where both nitrate and nitrite are present, the total of the two should not exceed 10 mg/L (as nitrogen).

The aesthetic objective for sodium in drinking water is 200 mg/L. The local Medical Officer of Health should be notified when the sodium concentrati exceeds 20 mg/L so that this information may be communicated to local physicians for their use with patients on sodium restricted diets.

When sulfate levels exceed 500 mg/L, water may have a laxative effect on some people.

APPENDIX C-3 – Septic System Assessment

The maximum possible office floor space $(30,000 \text{ sq. ft} = 2,787 \text{ m}^2)$ could support at maximum 300 employees, at 9.3 m² (100 sq. ft) office space per each employee (from the Ontario Building Code), for a total of 22,477 L/d. It is understood that a major portion of the building area is to be allocated for industrial activity, so the net area used as office space, and the corresponding number of employees, would be much lower than the above. Assuming that half of the building area is allocated for office space, the balance being for industrial usage, then the net serviceable population would be between 100 and 150 employees.

Large number of parking spots would be required for so many employees. For reference, one of the largest business centers in that neighborhood, Farrow at 106 Earl Thompson Road, has about 120 parking spaces. To review the ultimate parking space capacity per lot, we verify what each lot could service, considering the absorption field allocation of 600 $m^2 = 20 \text{ m X } 30 \text{ m}$ as per typical sketch in Figure C-1, in terms of number of employees. Those are based on the following assumptions:

- Unit flow rate per employee per 8-hour shift is 75 liters (from Ontario Building Code)
- Unit flow rate for the trucker toilet is 950 liters per day (from Ontario Building Code).
- Total flow rate is twice the theoretical domestic sewage flow rate, to consider concentrate release by the reverse osmosis filter.
- A 50% safety factor has been applied.
- Tertiary treatment is provided, to maximize hydraulic loading, and serviced population, within the septic field.

Table C-2: Estimated Maximum Number of Employees per Industrial Lot, for a 20 m X 30 m Septic Field

Lot	Percolation	Max number of	Corresponding daily flow
No.	Time	employees, for a 20	rate, including Reverse
	(min/cm)	m X 30 m septic field	Osmosis concentrate (L/d)
1	10	59	10750
2	10	59	10750
3	14	40	7900
4	10	59	10750
5	7	84	14500
6	7	84	14500
7	7	84	14500

Note: Lot no. 8 is dedicated to the stormwater management pond and will not have a septic system.

It is possible to reach higher number of employees, by maximizing the ground level area dedicated to parking space while still maintaining adequate buffer up to the property limit, the building, the septic system, and the stormwater ditches. The following table shows an estimate of the maximum number of employees at each lot, with the corresponding daily sewage flow rate.

Table C-3: Estimated Maximum Number of Employees per Industrial Lot, based on parking space capacity.

Lot No.	Maximum number of cars	Corresponding daily flow rate, including Reverse Osmosis concentrate (L/d)
1	159	25750
2	173	27850
3	159	25750
4	180	28900
5	180	28900
6	194	31000
7	187	29950

Those values are above the estimated capacity of the theoretical 20 m X 30 m septic field. Practically, each site could be developed to support such number of employees, provided the septic field area be increased accordingly at the front end of the lot.

Beyond these surface land occupancy issues, we shall consider the impact of converting most of the lot surface into impermeable surface (at the building, parking lot and driveway). This would reduce the net transfer of rainwater to the aquifer, with associated impact on the aquifer regeneration capacity.

APPENDIX D

SCS Curve Number Determination SWM Facility Design Calculations SWMHYMO Input and Output Files Swale Sizing Calculations

2509 Cedar Creek Road (161414214) NRCS (SCS) Curve Number Determination

		TABLE	OF CURVE	NUMBERS	(CN's)				
		Hydrologic Soil Type							Manning's
Land Use		Α	AB	В	BC	С	CD	D	'n'
Meadow	"Good"	30	44	58	64.5	71	74.5	78	0.40
Woodlot	"Fair"	36	48	60	66.5	73	76	79	0.40
Gravel		76	80.5	85	87	89	90	91	0.30
Lawns	"Good"	39	50	61	67.5	74	77	80	0.25
Pasture/Range		58	61.5	65	70.5	76	78.5	81	0.17
Crop		66	70	74	78	82	84	86	0.13
Fallow (Bare)		77	82	86	89	91	93	94	0.05
Impervious		98	98	98	98	98	98	98	0.01

		HYDROLO						
				ologic Soil				
Catchment	Α	AB	В	BC	С	CD	D	TOTAL
Estable a Constitute								
Existing Conditions		100						100
105								
106		100						100
103		100						100
102		100						100
100		40			60			100
104		100						100
/		100						100
101		100						100
Proposed Conditions								
200		100.0						100
201		100.0						100
202		100.0						100
203		100.0						100
204		100.0						100
205		100.0						100
206		100.0						100
208		100.0						100
207		100.0						100
102		100.0						100
103		100.0						100
100		40.0			60.0			100
104		100.0						100
101		100						100

			LAND	USE (%)					
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Impervious	Total
Existing Conditions									
105						95		5	100
106						100			100
103				20				80	100
102				20				80	100
100				20				80	100
104						100			100
/						100			100
101				40				60	100
Proposed Conditions									
200				100					100
201				10				90	100
202				10				90	100
203				100					100
204				10				90	100
205				85				15	100
206				100					100
208				100				0	100
207				100					100
102				20				80	100
103				20				80	100
100				20				80	100
104						100			100
101				40				60	100

			CU	RVE NUMB	ER (CN)					
Catchment	Meadow	Woodlot	Gravel	Lawns	Pasture Range	Crop	Fallow (Bare)	Impervious	Weighted CN	Pervious CN
Existing Conditions										
105	0	0	0	0	0	67	0	5	71	70
106	0	0	0	0	0	70	0	0	70	70
103	0	0	0	10	0	0	0	78	88	50
102	0	0	0	10	0	0	0	78	88	50
100	0	0	0	13	0	0	0	78	91	64
104	0	0	0	0	0	70	0	0	70	70
/	0	0	0	0	0	70	0	0	70	70
101	0	0	0	20	0	0	0	59	79	50
Proposed Conditions										
200	0	0	0	50	0	0	0	0	50	50
201	0	0	0	5	0	0	0	88	93	50
202	0	0	0	5	0	0	0	88	93	50
203	0	0	0	50	0	0	0	0	50	50
204	0	0	0	5	0	0	0	88	93	50
205	0	0	0	43	0	0	0	15	57	50
206	0	0	0	50	0	0	0	0	50	50
208	0	0	0	50	0	0	0	0	50	50
207	0	0	0	50	0	0	0	0	50	50
102	0	0	0	10	0	0	0	78	88	50
103	0	0	0	10	0	0	0	78	88	50
100	0	0	0	13	0	0	0	78	91	64
104	0	0	0	0	0	70	0	0	70	70
101	0	0	0	20	0	0	0	59	79	50

^{**} AMC II assumed
** Hydrological Soil Group taken from MTO Drainage Manual for each soil type

2509 Cedar Creek Road (161414214) **SWMHYMO Parameters**

Existing Conditio

Area Description	Catchment ID	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Start of path elevation	End of path elevation	Slope (%)	Length (m)	Pervious RC	Tc (hrs)	Tp (hrs)
Agricultural area in the north portion of the site with house and driveway, draining to agricultural land to the east and eventually to creek	105	DESIGN NASHYD	7.06	71	0.05		316.0	305.5	3.5%	300	0.22	0.55	0.33
Agricultural area in the south portion of the site draining to agricultural land to the south and eventually to creek	106	DESIGN NASHYD	11.00	70	0.00		314.0	301.0	2.2%	600	0.22	0.91	0.54
External catchment west of the site, containing a portion of existing industrial property, draining east into the site and ultimately flowing south	103	DESIGN STANDHYD	4.52	50	0.80	0.50	319.0	310.0	5.3%	170			
Large external catchment west of site, containing exisiting industrial property draining into private SWM feature and then onto site and ultimately flowing south	102	DESIGN STANDHYD	12.64	50	0.80	0.50	338.0	315.0	3.1%	750			
Large external catchment of industrial property and part of Hwy 401 north of the site, draining south into the site and flowing out to the east.	100	CALIB STANDHYD	55.94	64	0.80	0.50	335.0	311.5	1.6%	1500	Pervious Slope = 2%, Pervious Length = 30m	MNP: 0.25, MNI: 0.02	IAper: 5mm IAimp: 2mn
External agricultural area to the north-east of site draining to site and subsequently to agricultural area to the east	104	DESIGN NASHYD	0.73	70	0.00		318.0	314.5	3.5%	100	0.22	0.32	0.19
External catchment containing some of Cedar Creek Road, some industrial property, and a grassed area near Hwy 401 off-ramp, entering site in the north and draining overland to the east.	101	DESIGN STANDHYD	14.55	50	0.60	0.48	338.0	313.5	2.3%	1050			

Proposed Conditions	1					1	1 01 1 1			-		1	T
Area Description	Catchment ID	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Start of path elevation	End of path elevation	Slope (%)	Length (m)	Pervious RC	Tc (hrs)	Tp (hrs)
Small catchment in in northwest corner of property comprising a small portion of the West Road Ditch, draining to storm sewer and discharging uncontrolled to the east	200	DESIGN NASHHYD	0.14	50	0.00				1.5%	90	0.15	0.43	0.26
Small catchment in the northwest corner of property containing a portion of the East Road Ditch and developed land, draining to storm sewer and discharging uncontrolled to the east.	201	DESIGN STANDHYD	0.64	50	0.90	0.50			2.0%	75			
Large catchment of developed area covering the east portion of the site, draining to Rear Lot Ditch and entering the SWMF through the East Forebay	202	DESIGN STANDHYD	8.82	50	0.90	0.80			2.0%	115			
Small catchment on the east side of the site containing By Pass Storm Sewer outlet and plunge pool, draining offsite to the east	203	DESIGN NASHYD	0.55	50	0.00				2.0%	10	0.15	0.13	0.08
Large catchment of impervious area, draining to the west and into the East Road Ditch, entering the SWMF through the West Forebay.	204	DESIGN STANDHYD	4.92	50	0.90	0.80			2.0%	80			
SWM pond, located in south portion of the property	205	DESIGN NASHYD	1.63	57	0.15				2.0%	200	0.15	0.58	0.35
Grassed swale (West Road Ditch), located on the far west side of the property, directing flows around the SWMF and to the Outlet Channel at the southeast corner of the property.	206	DESIGN NASHYD	1.22	50	0.00				1.5%	900	0.15	1.35	0.81
Constructed conveyance channel (Outlet Channel), directing flows to Cedar Creek in the northeast	208	DESIGN NASHYD	1.13	50	0.00	0.00	302.00	296.50	0.01	725.00	0.22	1.41	0.85
Small catchment south of the SWMF, draining offsite to the south	207	DESIGN NASHYD	0.14	50	0.00				2.0%	7	0.15	0.11	0.07
Large external industrial area west of site, draining into private SWM feature and then entering swale, routing flows around SWMF to conveyance channel to Cedar Creek.	102	DESIGN STANDHYD	12.64	50	0.80	0.50	338.00	315.00	3.1%	750			
External catchment west of the site, containing a portion of existing industrial property, draining east into the site and ultimately flowing south to swale around SWM pond	103	DESIGN STANDHYD	4.52	50	0.80	0.50	319.00	310.00	5.3%	170			
Large external catchment of industrial property and part of Hwy 401 north of the site, draining south into the site and flowing out to the east.	100	CALIB STANDHYD	55.94	64	0.80	0.50	335.00	311.50	1.6%	1500	Pervious Slope = 2%, Pervious Length = 30m	MNP: 0.25, MNI: 0.02	IAper: 5mm, IAimp: 2mm
external catchment at the northeast corner of the site, draining to the site and following rear-lot swale, entering SWMF at its northeast inlet.	104	DESIGN NASHYD	0.73	70	0.00		318.0	314.5	3.5%	100	0.22	0.32	0.19
External catchment containing some of Cedar Creek Road, existing industrial property, and a grassed area near Hwy 401 off-ramp, entering storm sewer on site and draining to the east.	101	DESIGN STANDHYD	14.55	50	0.60	0.48	338.00	313.50	2.3%	1050			
						1							

78% Total to SWM Pond 16.10 Total developed area to SWM pond

Notes:

CN calculated for perviou	is areas only for DESIGN STANDHYD. CN is a weighted average for DESIGN NASHYD		
TIMP		Total per	cent impervious
XIMP		Percent i	mpervious directly connected
Time of Concentration ca	alculated using the Airport Method	Tc = [3.2 Where:	26 (1.1-C) L ^{0.5}]/S ^{0.33} C = Runoff Coefficient = 0.22 or 0.15 according to MTO Design chart 1.07 for 'cultivated' or 'lawn' on sandy soil L = Length of Overland Flow (m) S = Slope (%)
Time to Peak (hr)		- Tp = 0.6	Тс

2509 Cedar Creek Road (161414214) Stormwater Management Facility Design Calculations

						Rating Curve						Volume Estimati	on				
				Infiltra [.]	tion	Sur	face Dischar	ge		Pond		Infiltrati	on Basin		Overflow		
	Elevation		Infiltration	Volume	Infiltration Drawdown	Surface Discharge	Active	Surface Drawdown	Total Storage	Total Drawdown	Elevation	Area	Total Volume	Elevation	Spillway	Total Flow	Parameters
	(m)		(m³/s)		(hrs)	(m³/s)	(m³)	(hrs)	(m³)	(hrs)	(m)	(m²)	(m³)	(m)	(m³/s)		
Maximum sedimentation depth	301.50		0.044						23		301.50	5524	23	301.50			High Flow Weir
	301.60	0.10	0.044	653	4.1				653	4.1	301.60	6381	653	301.60			Spillway Invert (m) Top of Berm (m)
	301.70	0.20	0.044	1299	8.1				1,299	8.1	301.70	6538	1,299	301.70			302.50 303.00
	301.80	0.30	0.044	1960	12.2				1,960	12.2	301.80	6696	1,960	301.80			Spillway Length @ Invert (m) Max. Flow Depth (m)
	301.90	0.40	0.044	2638	16.5				2,638	16.5	301.90	6855	2,638	301.90			3 0.50
	302.00	0.50	0.044	3331	20.8				3,331	20.8	302.00	7014	3,331	302.00			Side Slopes (ratio of H:V) Topwidth
	302.10	0.60	0.044	4041	25.2				4,041	25.2	302.10	7173	4,041	302.10			10.00 13.00
	302.20	0.70	0.044 0.044	4766 5506	29.8 34.4				4,766 5,506	25.2 25.2	302.20 302.30	7329 7481	4,766 5,506	302.20 302.30			Weir Coefficient (Rectangle) Weir Coeff. (Triangle)
	302.30	0.80	l l														1.70 1.30
	302.40	0.90	0.044	6262	39.1				6,262	25.2	302.40	7631	6,262	302.40			Infiltration
Weir elevation	302.50	1.00	0.044	7033	43.9				7,033	25.2	302.50	7780	7,033	302.50			Infiltration Footprint (m²)
	302.60	1.10				0.202	785	2.2	7,818	27.4	302.60	7928	7,818	302.60	0.202	0.202	5524
	302.70	1.20				0.689	1,586	2.7	8,618	27.9	302.70	8072	8,618	302.70	0.689	0.689	Factored Infiltration Rate (mm/hr)
	302.80	1.30				1.479	2,400	2.9	9,432	28.1	302.80	8213	9,432	302.80	1.479	1.479	29
	302.90	1.40				2.606	3,228	3.0	10,261	28.2	302.90	8353	10,261	302.90	2.606	2.606	Infiltration Rate (m³/s)
Top of pond	303.00	1.50				4.101	4,070	3.0	11,103	28.3	303.00	8489	11,103	303.00	4.101	4.101	0.044

Notes:

Drawdown Time Calculations Greater than 0.1 m above the permanent pool

 $T=[v_2-v_1]/[(Q_2+Q_1)/2]/3600$

where

T=drawdown time in hours

v₂=starting pond volume v₂=ending pond volume

Q₂=starting flow

Q₁=ending flow

From 0.0 to 0.1 m above the permanent pool

 $T=[v_2-v_1]/[(Q_{2j}]/3600$

where

T=drawdown time in hours

v₂=starting pond volume

v₂=ending pond volume Q₂=starting flow

Weir Equation Used: $Q = C_{wb}^*L^*H^{1.5} + C_{wt}^*S^*H^{2.5}$

L = bottom width of spillway H = head above weir invert

S = side slopes (ratio of H:V)

 C_{wt} = weir coefficient (triangular) C_{wb} = weir coefficient (broad-crested)

Sharp crested semi-circular weir equation

Sharp crested semi-circular weir equation $Q=C^*D^{2.5*}(H/D)^{1.88}$

where

C = sharp crested semi-circular weir coefficient

D = diameter of orifice

H = head above orifice invert Note: used when water elevation is below 3/4 of the orifice diameter

Orifice Flow Calculations: Orifice flow equation

 $Q = C_*A_*(2_*g_*H)^{0.5}$ where

C = orifice coefficient

A = area of orifice

g = acceleration due to gravity

H = head above centre line of orifice

Note: used when water elevation is above 3/4 of the orifice diameter

2509 Cedar Creek Road (161414214)

External Stormwater Management Facility Design Calculations*

Classadia a											Volume Estimo	JIIOH					
П			Infiltro	ation	Sur	face Dischar	ge	Total	Pond		Infiltro	ation Basin		Overflow			
Elevation		Infiltration	Volume	Infiltration Drawdown	Surface Discharge	Active	Surface Drawdown	Total Storage	Total Drawdown	Elevation	Area	Total Volume	Elevation	Spillway	Total Flow	Paramete	ers
(m)		(m³/s)		(hrs)	(m³/s)	(m³)	(hrs)	(m³)	(hrs)	(m)	(m²)	(m³)	(m)	(m³/s)			
312.00		0.018	438	6.9						312.00	1,750	438	312.00			High Flow Weir	
312.10	0.10	0.018	639	10.1				438	10.1	312.10	2,286	639	312.10			Spillway Invert (m)	Top of Berm (m)
312.20	0.20	0.018	861	13.7				639	13.7	312.20	2,142	861	312.20			313.20	314.00
312.30	0.30	0.018	1100	17.5				861	17.5	312.30	2,649	1,100	312.30			Spillway Length @ Invert (m)	Max. Flow Depth (m)
312.40	0.40	0.018	1340	21.3				1,100	21.3	312.40	2,142	1,340	312.40			10	0.80
312.50	0.50	0.018	1610	25.6				1,340	25.6	312.50	3,265	1,610	312.50			Side Slopes (ratio of H:V)	Topwidth
312.60	0.60	0.018	1884	29.9				1,610	29.9	312.60	2,219	1,884	312.60			3.00	14.80
312.70 312.80	0.70	0.018 0.018	2171 2474	34.5				1,884 2,171	30.1 30.2	312.70 312.80	3,507 2,567	2,171 2,474	312.70			Weir Coefficient (Rectangle)	Weir Coeff. (Triangle)
	0.80			39.3				·		l			312.80			1.70	1.30
312.90	0.90	0.018	2778	44.1				2,474	30.2	312.90	3,507	2,778	312.90			Infiltration	
313.00	1.00	0.018	3094	49.1				2,778	30.3	313.00	2,811	3,094	313.00			Infiltration Footprint (m²)	
313.10	1.10	0.018	3427	54.4				3,094	30.3	313.10	3,844	3,427	313.10			1750	
313.20	1.20	0.018	3759	59.7				3,427	30.3	313.20	2,811	3,759	313.20			Factored Infiltration Rate (mm/hr)	
313.30	1.30				0.550	366	0.18	3,759	30.3	313.30	4,506	4,125	313.30	0.550	0.550	36	
313.40	1.40				1.590	756	0.29	4,125	30.3	313.40	3,289	4,515	313.40	1.590	1.590	Infiltration Rate (m³/s)	
313.50	1.50				2.986	1,145	0.33	4,515	29.9	313.50	4,506	4,905	313.50	2.986	2.986	0.018	
313.60	1.60				4.695	1,535	0.36			313.60	3,289	5,294	313.60	4.695	4.695		
313.70	1.70				6.700	1,959	0.38			313.70	5,184	5,718	313.70	6.700	6.700		•
313.80	1.80				8.988	2,407	0.40			313.80	3,781	6,166	313.80	8.988	8.988		
313.90	1.90				11.555	2,855	0.41			313.90	5,184	6,615	313.90	11.555	11.555		
314.00	2.00				14.397	3,304	0.42			314.00	3,781	7,063	314.00	14.397	14.397		
												· ·					

Notes:

Drawdown Time Calculations Greater than 0.1 m above the permanent pool

 $T=[v_2-v_1]/[(Q_2+Q_1)/2]/3600$

where

T=drawdown time in hours v₂=starting pond volume

v₂=ending pond volume

 Q_2 =starting flow Q_1 =ending flow

From 0.0 to 0.1 m above the permanent pool

 $T=[v_2-v_1]/[(Q_{2j}]/3600$

where

T=drawdown time in hours v₂=starting pond volume

v₂=ending pond volume

Q₂=starting flow

*External SWM Facility modelled according to assumptions made based on LiDAR data and the surrounding soil characteristics

Weir Equation Used: $Q = C_{wb}^*L^*H^{1.5} + C_{wt}^*S^*H^{2.5}$

where

L = bottom width of spillway H = head above weir invert

S = side slopes (ratio of H:V) C_{wt} = weir coefficient (triangular)

C_{wb} = weir coefficient (broad-crested)

Sharp crested semi-circular weir equation

Sharp crested semi-circular weir equation

 $Q=C*D^{2.5}*(H/D)^{1.88}$

where

C = sharp crested semi-circular weir coefficient

D = diameter of orifice

H = head above orifice invert

Note: used when water elevation is below 3/4 of the orifice diameter

Orifice Flow Calculations: Orifice flow equation

Q = $C_*A_*(2*g_*H)^{0.5}$ where

C = orifice coefficient

A = area of orifice

g = acceleration due to gravity

H = head above centre line of orifice

Note: used when water elevation is above 3/4 of the orifice diameter

2509 Cedar Creek Road (161414214) Sediment Forebay Sizing Calculations Using MOE - SWMPD Manual (2003)

East Forebay				
Dispersion Length	y _s = total depth of sediment in forebay (m)	y _s =	0.5	
Dist = 8Q/dv	Q = inlet flow (m3/s)	Q =	2.294	Note 1.
= 52 m	d = depth of perm pool in forebay above y _s (m)	d =	0.7	
	v _f = desired vel in forebay (m/s)	$v_f =$	0.5	
West Forebay)			0.5	
Dispersion Length	y _s = total depth of sediment in forebay (m)	y _s =	0.5	
Dist = 8Q/dv	Q = inlet flow (m3/s)	Q =	1.323	Note 1.
= 30 m	d = depth of perm pool in forebay above y _s (m)	d =	0.7	
	v _f = desired vel in forebay (m/s)	$v_f =$	0.5	
East Forebay				
Cleanout Frequency				
Table 5.3 MOEE SWMPP Guidelines	A _{sew} = Contributing Sewer Area (ha)	$A_{sew} =$	9.55	
	Imp = Percent Impervious (%)	Imp =	80%	
cleanout = Vol/(load*A _{sew} *effic)	load = Sediment Loading (m³/ha)	load =	3.4	
= 7.3 years	effic = Removal Efficiency (%) - Level 1	effic =	80%	
	Targ = Cleanout Frequency Target (years)	Targ =	7	
Therefore, Cleanout Frequency Satisfied	Vol = Sediment volume (m³)	Vol =	190	Note 2.
West Forebay Cleanout Frequency				
Table 5.3 MOEE SWMPP Guidelines	A _{sew} = Contributing Sewer Area (ha)	$A_{sew} =$	4.92	
	Imp = Percent Impervious (%)	Imp =	80%	
cleanout = Vol/(load*A _{sew} *effic)	load = Sediment Loading (m³/ha)	load =	3.4	
= 9.6 years	effic = Removal Efficiency (%) - Level 1	effic =	80%	
	Targ = Cleanout Frequency Target (years)	Targ =	7	
TI (01-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	Vol = Sediment volume (m³)	Vol =	129	Note 2.
Therefore, Cleanout Frequency Satisfied				

Peak inlet flows to SWM facility based on SWMHYMO modelling (5-year storm)
 Volume of bottom 0.5 m depth, the maximum sediment accumulation depth

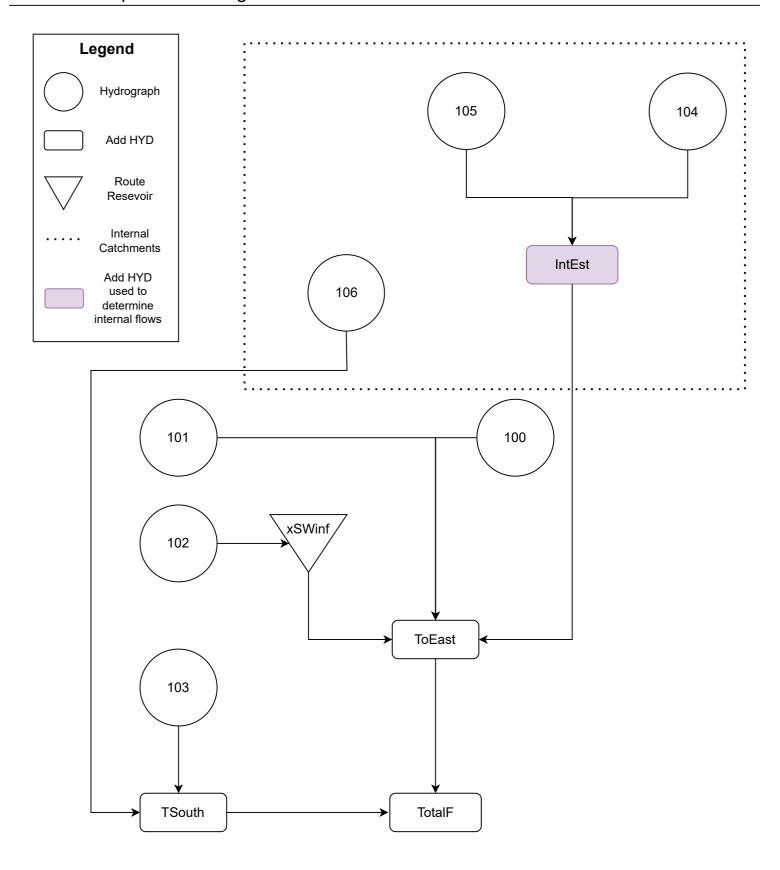
2509 Cedar Creek Road (161414214)

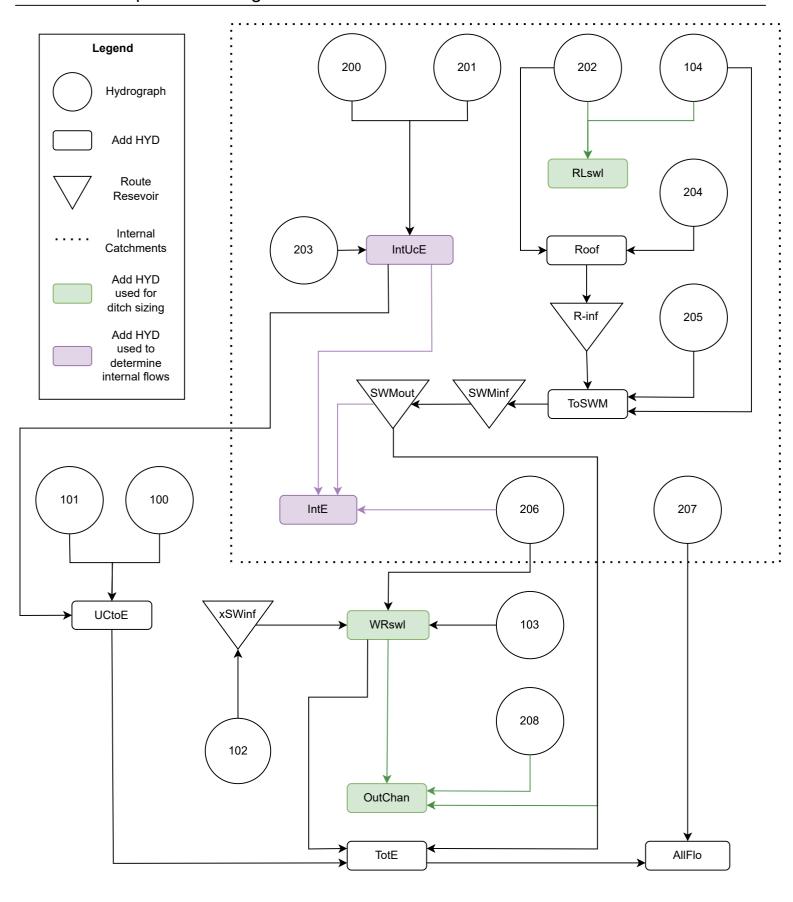
Stormwater Quality Volumetric Requirements (Future Conditions)

				Water Quality Unit Volume Requirements	Water Quality Volume Requirements
Drainage Area (ha) ²	Total % Imp.	Level	Facility Type	Total Unit Volume (m³/ha)	Total MOE Volume
16.10	78%	Enhanced	Infiltration	38	608

¹ Water quality unit volume requirements based on Table 3.2, Stormwater Management Planning & Design Manual (MOE 2003)

² Drainage Area for Quality control represents total storm sewer drainage area to SWM Facility and includes the area of the SWM block itself and external area draining onto site





```
000033 *# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214] 00004> *# Date :01-25-2024 000050 *# Modeller : [Amy Kyle, Water Resources Specialist] 000065 *# Company : Stantec Consulting Ltd. (Waterloo) 000070 *# License #: 4730904
TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1]
["Kit25mm.4hr"] <--storm filename, one per line for NSTORM
  00015> START
  00016> *%
00017> *%
Existing internal area draining to the east
                                                                     ID=[1], NHYD=["105"], DT=[1]min, AREA=[7.06] (ha),
DW=[0](cms), CN/C=[71], TP=[0.33]hrs,
RAINFALL=[, , , ] (mm/hr), END=-1
  00028> DESIGN NASHYD
                           Small external area entering site from east and draining south / east
                                                                      ID=[2], NHYD=["104"], DT=[1]min, AREA=[0.73](ha), DWF=[0](cms), CN/C=[70], TP=[0.19]hrs, RAINFALL=[, , , , ](mm/hr), END=-1
                                                                          Total existing area draining to the east
  00044> ADD HYD
                                                                      IDsum=[3], NHYD=["IntEst"], IDs to add=[1+2]
                                                                     Existing internal area draining to the south
                                                                     ID=[4], NHYD=["106"], DT=[1]min, AREA=[11.00](ha),
DWF=[0](cms), CN/C=[70], TP=[0.54]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
                         Total Pre-Development Drainage Area (Including Large External Catchments)
 00058> *#
                         External industrial catchment and part of Hwy 401, draining south into the site and flowing south / east.
                                                                   00063> CALIB STANDHYD
00064>
00065>
00066>
00067>
00072> *#
00073> *# External cat
00074> *# indus
00075> *#
00075> *#
00077> *#-----
00078> DESIGN STANDHYD
00079>
00080>
00081> *$-------
00082> *#
                        External catchment containing a portion of Cedar Creek Road, a portion of industrial area, and a grassed area near Hwy 401 off-ramp, draining south into site and flowing south / east.
                                           00082> *#
00083> *# External catchment west of site, containing exisiting industrial
00084> *# property draining into private SWM feature and then onto site flowing east
  00086> *#-----
00087> DESIGN STANDHYD
                                                                     ID=[7], NHYD=["102"], DT=[1]min, AREA=[12.64](ha),
XIMP=[0.50], TIMP=[0.80], DWF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[3.1](%), RAINFALL=[, , , , ](mm/hr), END=-1
 00088>
                                                                             Infiltration in External SWM Feature
                                                                     IDout=[8], NHYD=["xSWinf"], IDin=[7],
RDT=[1](min),
TABLE of ( OUTFLOW-STORAGE ) values
                                                                                                                    OUTFLOW-STORAGE ) va

(cms) - (ha-m)

0.0 , 0.0 ]

0.018 , 0.0438 ]

0.018 , 0.3759 ]

-1 , -1 ] (ma
                                                                                     [ -1 , -1 ] (max twenty pts)

IDovf=[9], NHYDovf=["OVF-xI"]
 00103>
10011= "OVF-XI"]

00105> *$

00105> *$

00105> *$

00105> *$

00105> *$

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1001
                                                                     ID=[1], NHYD=["103"], DT=[1]min, AREA=[4.52](ha),
XIMP=[0.50], TIMP=[0.80], DWF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[5.3](%), RAINFALL=[, , , , ](mm/hr), END=-1
  00116> DESIGN STANDHYD
00117>
  00118>
                                                                                               Total Flows to the south
                                       | IDsum=[2], NHYD=["TSouth"], IDs to add=[4+1]
                                                                  Total Flows from site (eventually to Cedar Creek)
```

00128> *#	
00129> *# 00130> ADD HYD	IDsum=[3], NHYD=["TotalF"], IDs to add=[5+2]
00130> ADD HID 00131> *%	IDSUM=[3], NHID=["TOTAIF"], IDS to add=[3+2]
001312 *%	
00132> 0	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[2]
00133> SIAKI	["Kit2yr.3hr"] <storm filename,="" for="" line="" nstorm="" one="" per="" t<="" td=""></storm>
00135> *%	Interpresent Continue Conti
00136> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[5]
00137> *	["Kit5yr.3hr"] <storm filename,="" for="" line="" nstorm="" one="" per="" t<="" td=""></storm>
00138> *%	
00139> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[10
00140> *	["Kit10yr.3hr"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""></storm>
00141> *%	
00142> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[25
00143> *	["Kit25yr.3hr"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""></storm>
00144> *%	
00145> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[50
00146> *	["Kit50yr.3hr"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""></storm>
00147> *%	
00148> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[10
00149> *	["Kit100yr.3hr"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""></storm>
00150> *%	
00151> START	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[50
00152> *	["hurhaz48.stm"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""></storm>
00153> *%	
00154> FINISH	

00155>

00160>

00168> 00169>

00186> 00187> 00188> 00189>

00190> 00191> 00192> 00193> 00194>

00199>

00200> 00201>

00216>

00230>

```
00128>
00129>
00003) *# Froject Name: [2509 Cedar Creek Road SWM - Ayr, ON] Froject #: [161414214] 00004) *# Date : 01/25/2024 00005) *# Modeller : [Amy Kyle, Water Resources Specialist] 00006) *# Company : Stantec Consulting Ltd. (Waterloo) 00007) *# License # : 4730904
                                                                                                                                                                                                                             00130>
                                                                                                                                                                                                                            00133> *#-----
00134> ROUTE RESERVOIR
00135>
00136>
00137>
00138>
00139>
                                                                                                                                                                                                                             00140>
                                                                                                                                                                                                                             00141>
                                                               TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1]
["Kit25mm.4hr"] <--storm filename, one per line for NSTORM
 00015> START
                                                                                                                                                                                                                             00142>
 00016> *%
00017> *%---
00144>
00145> *#-----
00146> *#
00147> *# West Roa
00148> *#
00148> *#
00149> *#
00150> *#-----
00151> DESIGN NASHYD
00152>
                             Small portion of West Road Ditch draining offsite to the east through By-Pass Storm Sewer(BPSS)
 00028>
                                                                                                                                                                                                                             00155> *#
00156> *#
                                                                 ID=[1], NHYD=["200"], DT=[1]min, AREA=[0.14](ha),
DWF=[0](cms), CN/C=[50], TP=[0.26]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
 00029> DESIGN NASHYD
                                                                                                                                                                                                                             00158> *#-----
00159> DESIGN NASHYD
00033> +#
00034> +# Proposed developed catchment draining offsite to the east through BPSS
00035> +#
                                                                                                                                                                                                                             00160>
00036> *#-----
00037> DESIGN STANDHYD
                                                                  ID=[2], NHYD=["201"], DT=[1]min, AREA=[0.64](ha),
XIMP=[0.50], TIMP=[0.90], DWF=[0](cms), LOSS=[2],
SLOPE=[2](%), RAINFALL=[, , , , ](mm/hr), END=-1
 00041> *#
00042> *# Proposed internal grassed area and plunge pool draining offsite to the east
00043> *#
 00044> *#--
                                                                 ID=[3], NHYD=["203"], DT=[1]min, AREA=[0.55](ha),
DWF=[0](cms), CN/C=[50], TP=[0.08]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
 00045> DESIGN NASHYD
 00046>
00047>
                                        Total internal area draining onto agricultural area to the east
                                                                  IDsum=[5], NHYD=["IntUcE"], IDs to add=[1+2+3]
                                                     Proposed industrial lots draining to Rear Lot Ditch
 00058>
                                                                  ID=[6], NHYD=["202"], DT=[1]min, AREA=[8.82](ha),
XIMP=[0.80], TIMP=[0.90], DWF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[2](%), RAINFALL=[, , , , ](mm/hr), END=-1
 00059> DESIGN STANDHYD
00063> *#
00064> *# External
00065> *#
00066> *#------
00067> DESIGN NASHYD
                                                                                                                                                                                                                            00190>
00191>
00192>
                         External agricultural area draining onsite and entering Rear Lot Ditch
                                                                  ID=[7], NHYD=["104"], DT=[1]min, AREA=[0.73](ha), DWF=[0](cms), CN/C=[70], TP=[0.19]hrs, RAINFALL=[, , , ](mm/hr), END=-1
                                    Total area entering Rear Lot Ditch and entering SWMF at East inlet
 00073> *#
                                                                                                                                                                                                                             00200> ADD HYD
 00074> *#
 Proposed industrial lots draining to East Road Ditch within catchment, and new internal roadway
                                                                 ID=[1], NHYD=["204"], DT=[1]min, AREA=[4.92](ha),
XIMP=[0.80], TIMP=[0.90], DWF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[2](%), RAINFALL=[, , , , ] (mm/hr), END=-1
                                          Rooftop infiltration lumped together and sized for 25mm runoff volume from an assumed 0.15ha rooftop area per lot (7 lots)
00087> *#
00088> *#
00089> *#
00090> *#-
                                                                                                                                                                                                                             00215> *#-----
00216> ROUTE RESERVOIR
                                                                                                                                                                                                                                                                                              IDout=[5],
00091> ADD HYD
00092> *%------
00093> ROUTE RESERVOIR
00094>
                                                                  IDsum=[2], NHYD=["Roof"], IDs to add=[1+6]
                                                                00098>
00099>
                                                                                                                                                                                                                             00230> *#
00231> *#-----
00232> DESIGN STANDHYD
00103> *#
00104> *#
                                                       Proposed SWM facility catchment (infiltration basin)
00105> *
00105> *#-----
00106> DESIGN NASHYD
00107>
00108>
00109> *#----
00110> *#
00111> *#
00112> *#
                                                                  ID=[9], NHYD=["205"], DT=[1]min, AREA=[1.63](ha), DWF=[0](cms), CN/C=[57], TP=[0.35]hrs, RAINFALL=[, , , , ](mm/hr), END=-1
                                                                                                                                                                                                                             00235> *#
00236> *#
00237> *#
                                                                                All flows entering SWM facility
00112> *#
00113> *#----
00114> ADD HYD
00115> *%----
                                                                                                                                                                                                                             00240> ADD HYD
00241> *#-----
00242> DESIGN NASHYD
                                                                  \label{eq:idsum} \mbox{IDsum=[6], NHYD=["ToSWM"], IDs to add=[10+7+9]}
                                                                         Infiltration Portion of SWM facility
00118> *#
                                                                                                                                                                                                                             00245>
                                                                                                                                                                                                                             00246> *#
00247> *#
                                                                 | IDout=[7], NHYD=["SWMinf"], IDin=[6], RDT=[1](min), TABLE of ( OUTFLOW-STORAGE ) values
 00120> ROUTE RESERVOIR
00121>
00122>
                                                                                                            JUTE/LOW-STUCKAGE, (Cms) - (ha-m) (Cms) - (ha-m) (O.0 ) (O.0 ) (O.044, O.0653] (O.044, O.7033] (O.044, O.7033] (Cms) (Cm
```

```
IDovf=[8], NHYDovf=["OVF-I"]
                                                Active Storage Portion of SWM facility
                                                                  NHYD=["SWMout"], IDin=[8],
                                                                of ( OUTFLOW-STORAGE ) values
                                                                           (cms) - (ha-m)
0.0 , 0.0 ]
0.202 , 0.0785
                                                                              0.689 , 0.1586
1.479 , 0.2400
4.101 , 0.4070
                                                                                                     (max twenty pts)
                                                       [ -1 , -1 ]
IDovf=[2], NHYDovf=["OVF"]
                     West Road Ditch, conveying external drainage from the west around the proposed SWM facility to Outlet Channel
                                             ID=[2], NHYD=["206"], DT=[1]min, AREA=[1.22](ha),
DWF=[0](cms), CN/C=[50], TP=[0.81]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
                        Grassed area south of SWM facility draining offsite to the south
                                             ID=[10], NHYD=["207"], DT=[1]min, AREA=[0.14](ha),
DWF=[0](cms), CN/C=[50], TF=[0.07]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
                                          Total Flows to the east from internal catchments
                         IDsum=[7], NHYD=["IntE"], IDs to add=[5+1+2]
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
                                            | Ind=[3], NHYD=["100"], DT=[1](min), AREA=[55.94](ha), XIMF=[0.50], TIMF=[0.80], DWF=[0](cms), LOSS=[2], SCS curve number CN=[64], Pervious surfaces: IAper=[5](mn), SLFP=[2](%), Forevious surfaces: IAper=[6](mn), MNF=[0.25], SCP=[0](min), Impervious surfaces: IAimp=[2](mm), SLFI=[1.6](%), LGI=[1500](m), MNI=[0.02], SCI=[0](min), RAINFALL=[, , , ](mm/hr), END=-1
 00188> *# External catchment containing a portion of Cedar Creek Road, a portion
00189> *# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
                                             D=[7], NHYD=["101"], DT=[1]min, AREA=[14.55](ha),
XIMF=[0.48], TIMF=[0.60], DWF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[2.3](%), RAINFALL=[, , , , ](mm/hr), END=-1
                     Total area draining offsite to east onto agricultural area to the east
                                         IDsum=[9], NHYD=["UCtoE"], IDs to add=[5+3+7]
00200> ADD HYD IDsum=[9], NHYD=["UCtoE"], IDs to add=[5+3+7]
00201> *#
00202> *#
00203> *#
Large external catchment west of site containing industrial property,
00204> *# draining into private SWM feature and then into West Road Ditch, routing
00205> *#
00206> *#
00206> *#
                                             ID=[4], NHYD=["102"], DT=[1]min, AREA=[12.64](ha), XIMP=[0.50], TIMP=[0.80], DWF=[0](cms), LOSS=[2], CN=[50], SLOPE=[3.1](%), RAINFALL=[, , , , ](mm/hr), END=-1
                                                  Infiltration in External SWM Feature
                                                                  NHYD=["xSWinf"], IDin=[4],
                                             RDT=[1] (min),
TABLE of ( OUTFLOW-STORAGE ) values
                                                      TABLE OI ( OUTFLOW-STORAGE ) values (cms) - (ha-m) [ 0.0 , 0.0 ] [ 0.018 , 0.0438 ] [ 0.018 , 0.3759 ] [ -1 , -1 ] (max twenty pts) IDOvf=[6], NHYDovf=["OVF-XI"]
D=[7], NHYD=["103"], DT=[1]min, AREA=[4.52](ha),
XIMP=[0.50], TIMP=[0.80], DMF=[0](cms), LOSS=[2], CN=[50],
SLOPE=[5.3](%), RAINFALL=[, , , , ](mm/hr), END=-1
                                             Total Flows through West Road Ditch
                                              IDsum=[8], NHYD=["WRswl"], IDs to add=[6+7+2]
                                             ID=[5], NHYD=["208"], DT=[1]min, AREA=[1.13](ha),
DMF=[0](cms), CN/C=[50], TP=[0.85]hrs,
RAINFALL=[, , , ](mm/hr), END=-1
                                            Total Flows through Outlet Channel
                                             IDsum=[3], NHYD=["OutChan"], IDs to add=[1+8+5]
                                            Total Flows to the east (eventually to Cedar Creek)
```

00256>	ADD HYD	 IDsum=[4], NHYD=["TotE"], IDs to add=[1+8+9]	00382> 00383>
00258> 00259> 00260>	*# *# *#	Total Flows from the Site	00384> 00385> 00386> 00387>
00261> 00262>	*# ADD HYD	 IDsum=[6], NHYD=["AllFlo"], IDs to add=[4+10]	00388> 00389>
00264> 00265>	START *		00390> 00391> 00392>
00266> 00267> 00268>	*% START *		00393> 00394> 00395>
00269> 00270> 00271>	*% START *		00396> 00397> 00398>
00272> 00273> 00274>	*% START *	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[25] ["Kit25yr.3hr"] <storm filename,="" for="" line="" nstorm="" one="" per="" t<="" td=""><td>00399> 00400> 00401></td></storm>	00399> 00400> 00401>
00275> 00276> 00277>	*% START *	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[50]	00402> 00403> 00404>
00278> 00279> 00280>	*% START *		00405> 00406> 00407>
00281> 00282> 00283>	*% START *	TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[500 ["hurhaz48.stm"] <storm filename,="" for="" line="" nstorm<="" one="" per="" td=""><td>00408> 00409> 00410></td></storm>	00408> 00409> 00410>
00284>	*% FINISH		00411> 00412> 00413>
00287> 00288> 00289>			00414> 00415>
00290> 00291> 00292>			
00293> 00294>			
00295> 00296> 00297>			
00298> 00299> 00300>			
00301> 00302> 00303>			
00304> 00305> 00306>			
00307> 00308> 00309>			
00310> 00311> 00312>			
00313> 00314>			
00315> 00316> 00317>			
00318> 00319> 00320>			
00321> 00322> 00323>			
00324> 00325> 00326>			
00327> 00328>			
00329> 00330> 00331>			
00332> 00333> 00334>			
00335> 00336> 00337>			
00338> 00339> 00340>			
00341> 00342> 00343>			
00344> 00345>			
00346> 00347> 00348>			
00349> 00350> 00351>			
00352> 00353> 00354>			
00355> 00356> 00357>			
00358> 00359>			
00360> 00361> 00362>			
00363> 00364> 00365>			
00366> 00367> 00368>			
00369> 00370> 00371>			
00372> 00373>			
00374> 00375> 00376>			
00377> 00378> 00379>			
00380> 00381>			

```
______
                               000
                                      999
 SSSSS
              М
                Н
                  Н
                    Υ
                       Y M
                            М
                                           999
         W
                                                =======
      WWW
           MM MM
                Н
                  Н
                     YY
                         MM MM
                                 0
                                      9
                                        9
                                          9
                                             9
                              0
 SSSSS
      WWW
           M M M
                HHHHH
                      Υ
                         M M M
                              0
                                 0
                                   ##
                                                Ver 4.05
                Н
                         Μ
                            Μ
                                 0
                                      9999
                                           9999
                                                Sept 2011
       W W
           Μ
              Μ
                  Н
                      Υ
 SSSSS
                                        9
       W W
              Μ
                Н
                               000
                                             9
                                                =======
                                        9
                                             9
                                                # 4730904
     StormWater Management HYdrologic Model
                                      999
                                           999
***********************************
******
        A single event and continuous hydrologic simulation model
******
          based on the principles of HYMO and its successors
                  OTTHYMO-83 and OTTHYMO-89.
***********************************
****** Distributed by:
                  J.F. Sabourin and Associates Inc.
******
                  Ottawa, Ontario: (613) 836-3884
*****
                  Gatineau, Quebec: (819) 243-6858
******
                   E-Mail: swmhymo@ifsa.Com
***********************************
++++++ Licensed user: Stantec Consulting Ltd. (Kitchener)
++++++++
                 Kitchener
                                SERIAL#:4730904
                                                ++++++++
************************************
              +++++ PROGRAM ARRAY DIMENSIONS ++++++
*****
              Maximum value for ID numbers :
              Max. number of rainfall points: 105408
******
              Max. number of flow points
                                  : 105408
************************************
********
                 DETAILED OUTPUT
***********************************
                                  RUN COUNTER: 000239
       DATE: 2024-01-25
                     TIME: 15:08:53
************************************
* Input filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPre.dat
* Output filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPre.out
* Summary filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPre.sum
* User comments:
* 1:
 2:
```

_ -

```
001:0001-----
*#**********************************
   Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
         : 01-25-2024
   Date
*# Modeller
            : [Amy Kyle, Water Resources Specialist]
            : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
   25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
   and the Regional Event
*#*********************************
START
                 Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
                 Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
   TZERO =
           .00 hrs on
   METOUT=
           2 (output = METRIC)
   NRUN = 001
   NSTORM=
        # 1=Kit25mm.4hr
001:0002-----
READ STORM
                   Filename: 25 mm, 4hr Chicago Storm - Kitchener IDF
| Ptotal= 25.00 mm|
                   Comments: 25 mm, 4hr Chicago Storm - Kitchener IDF
           TIME
                 RAIN |
                         TIME
                              RAIN |
                                       TIME
                                             RAIN |
                                                    TIME
                                                           RAIN
            hrs
                mm/hr |
                         hrs
                              mm/hr
                                       hrs
                                            mm/hr
                                                     hrs
                                                          mm/hr
                                       2.08
                                            5.764
            .08
                 1.465
                         1.08
                              4.024
                                                    3.08
                                                          2.074
            .17
                1.540
                         1.17
                              4.814
                                       2.17
                                                    3.17
                                            4.969
                                                          1.977
            .25
                         1.25
                              6.025
                                       2.25
                                                    3.25
                 1.625
                                            4.374
                                                          1.889
            .33
                 1.720
                         1.33
                              8.114
                                       2.33
                                            3.913
                                                   3.33
                                                          1.810
            .42
                 1.829
                         1.42 12.526
                                       2.42 3.545
                                                    3.42
                                                          1.737
            .50
                 1.955
                         1.50 27.198
                                       2.50 3.245
                                                    3.50
                                                          1.671
            .58
                2.101 |
                         1.58 74.855
                                       2.58 2.994
                                                    3.58
                                                          1.610
                                       2.67
            .67
                 2.274
                         1.67
                             31.410 |
                                            2.782
                                                    3.67
                                                          1.553
            .75
                 2.482
                         1.75
                             16.819
                                      2.75 2.601
                                                   3.75
                                                          1.501
                                       2.83
            .83
                 2.736
                         1.83 11.357
                                            2.443
                                                    3.83
                                                          1.453
            .92
                 3.055
                         1.92
                             8.563
                                       2.92
                                            2.305
                                                   3.92
                                                          1.408
                 3.468
                         2.00
                             6.882 | 3.00
                                            2.183 | 4.00
           1.00
                                                          1.366
```

```
001:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#------|
*#
*#
          Existing internal area draining to the east
*#
*#-----|
----- U.H. Tp(hrs)= .330
  Unit Hyd Qpeak (cms)= .817
  PEAK FLOW (cms)=
TIME TO PEAK (hrs)= 2.000
(mm)= 4.340
  PEAK FLOW (cms) = .073 (i)
  TOTAL RAINFALL
           (mm) = 25.000
  RUNOFF COEFFICIENT =
               .174
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0004-----
*#
*#
  Small external area entering site from east and draining south / east
*#-----|
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
         (cms) = .010 (i)
  PEAK FLOW
  TIME TO PEAK
              1.817
          (hrs)=
              4.172
  RUNOFF VOLUME
           (mm) =
           (mm) =
  TOTAL RAINFALL
              25.000
  RUNOFF COEFFICIENT =
               .167
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
001:0005-----
*#------
*#
          Total existing area draining to the east
*#
*#-----|
_____
| ADD HYD (IntEst ) | ID: NHYD
                        QPEAK TPEAK
                    AREA
                                R.V.
                                    DWF
_____
                   (ha) (cms) (hrs) (mm)
7.06 .073 2.00 4.34
                                   (cms)
                                   .000
          ID1 01:105
         +ID2 02:104
                    .73 .010 1.82 4.17
                                   .000
          ______
                  7.79 .081 1.97 4.32
          SUM 03:IntEst
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0006-----
*#
*#
         Existing internal area draining to the south
*#-----|
DESIGN NASHYD | Area (ha)= 11.00 Curve Number (CN)=70.00
           Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 04:106 DT= 1.00 |
           U.H. Tp(hrs) = .540
-----
  Unit Hyd Qpeak (cms)= .778
         (cms)=
  PEAK FLOW
              .078 (i)
             2.283
  TIME TO PEAK
         (hrs)=
             4.173
  RUNOFF VOLUME
          (mm) =
  TOTAL RAINFALL
          (mm) =
              25.000
  RUNOFF COEFFICIENT =
               .167
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
______
001:0007-----
*# Total Pre-Development Drainage Area (Including Large External Catchments)
```

```
*#-----|
*#
*# External industrial catchment and part of Hwy 401, draining south into the
*#
                   site and flowing south / east.
*#------
______
                   Area (ha) = 55.94
| CALIB STANDHYD |
| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
                       IMPERVIOUS
                                   PERVIOUS (i)
   Surface Area (ha)=
                                    11.19
                         44.75
                 (mm)= 2.00
(%)= 1.60
(m)= 1500.00
   Dep. Storage (mm)=
                                     5.00
   Average Slope (%)=
                                    2.00
   Length
                                   30.00
                                    .250
   Mannings n
                         .020
                        35.29
                                   17.90
   Max.eff.Inten.(mm/hr)=
                         22.00
            over (min)
                                   34.00
                      22.13 (ii) 33.94 (ii)
22.00 34.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                                     .03
   Unit Hyd. peak (cms)=
                          .05
                                               *TOTALS*
                                   .32
2.20
                        1.75
1.92
   PEAK FLOW
                (cms)=
                                                 1.952 (iii)
   TIME TO PEAK
               (hrs)=
                                                1.933
   RUNOFF VOLUME
                ( mm ) =
                         23.00
                                    6.60
                                               14.800
                        25.00
   TOTAL RAINFALL (mm)=
                                   25.00
                                               25.000
   RUNOFF COEFFICIENT =
                          .92
                                     .26
                                                 .592
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
                  Ia = Dep. Storage (Above)
        CN* = 64.0
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
```

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
IMPERVIOUS PERVIOUS (i)
                       8.73
Surface Area
           (ha)=
                                     5.82
Dep. Storage
                                     1.50
              (mm) =
                          .80
              (%)=
Average Slope
                         2.30
                                     2.30
                        311.45
Length
                (m) =
                                   40.00
                        .013
Mannings n
                                    .250
                       74.85
                                    3.89
Max.eff.Inten.(mm/hr)=
         over (min)
                        4.00
                                   29.00
                       4.42 (ii) 29.21 (ii)
4.00 29.00
Storage Coeff. (min)=
Unit Hyd. Tpeak (min)=
Unit Hyd. peak (cms)=
                                     .04
                          .26
                                                *TOTALS*
                       1.04
1.62
24.20
                                     .04
PEAK FLOW
             (cms)=
                                                 1.041 (iii)
TIME TO PEAK (hrs)=
                                    2.12
                                                 1.617
RUNOFF VOLUME
             ( mm ) =
                                    2.59
                                                12.965
TOTAL RAINFALL (mm)=
                       25.00
                                   25.00
                                                25.000
RUNOFF COEFFICIENT =
                         .97
                                     .10
                                                  .519
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
001:0009-----
*#
*# External catchment west of site, containing exisiting industrial
*# property draining into private SWM feature and then onto site flowing east
*#
*#-----|
______
DESIGN STANDHYD | Area (ha)= 12.64
IMPERVIOUS
                             PERVIOUS (i)
   Surface Area (ha)=
Dep. Storage (mm)=
                    10.11
                               2.53
                  .80
3.10
290.29
                               1.50
   Average Slope (%)=
                               3.10
                            40.00
              (m) =
   Length
   Mannings n
                     .013
                              .250
   Max.eff.Inten.(mm/hr)=
                     74.85
                              19.51
                     4.00 16.00
3.87 (ii) 15.77 (ii)
          over (min)
   Storage Coeff. (min)=
                     4.00 16.00
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                      .29
                               .07
```

```
*TOTALS*
PEAK FLOW (cms)=
                      .97
                                    .08
                                                1.002 (iii)
            (hrs)=
                   1.62
24.20
25.00
TIME TO PEAK
                        1.62
                                    1.87
                                                1.617
RUNOFF VOLUME
             (mm) =
                                   4.72
                                               14.463
              (mm) =
                                  25.00
TOTAL RAINFALL
                                               25.000
RUNOFF COEFFICIENT =
                                   .19
                                                .579
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
*#-----|
                  Infiltration in External SWM Feature
*#
*#------|
-----
ROUTE RESERVOIR
                   Requested routing time step = 1.0 min.
| IN>07:(102 )
| OUT<08:(xSWinf) |
                   ====== OUTLFOW STORAGE TABLE ======
                   OUTFLOW STORAGE | OUTFLOW STORAGE
                                    (cms) (ha.m.)
                     (cms) (ha.m.)
                                  .018 .3759E+00
                      .000 .0000E+00
                      .018 .4380E-01 |
                                        .000 .0000E+00
                     AREA QPEAK TPEAK
(ha) (cms) (hrs)
12.64 1.002 1.617
12.64 .018 1.583
   ROUTING RESULTS
                                                R.V.
                                                (mm)
   INFLOW >07: (102 )
                                               14.463
  OUTFLOW<08: (xSWinf)
OVERFLOW<09: (OVF-xI)
                                               14,463
                                       .000
                       .00
                                .000
                                                 .000
              TOTAL NUMBER OF SIMULATED OVERFLOWS =
              CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                 .00
               PERCENTAGE OF TIME OVERFLOWING (%)=
                                                 .00
                    FLOW REDUCTION [Qout/Qin](%)=
               PEAK
                                                1.797
                                        (min)=
               TIME SHIFT OF PEAK FLOW
              MAXIMUM STORAGE USED
                                      (ha.m.)=.1636E+00
```

001:0011-----

```
*#
*#
              Total existing area draining to the east
*#-----|
_____
| ADD HYD (ToEast ) | ID: NHYD
                          AREA
                               QPEAK
                                     TPEAK
                                          R.V.
                                               DWF
------
                          (ha)
                                (cms) (hrs) (mm)
                                               (cms)
                          55.94
             ID1 02:100
                                1.952 1.93 14.80
                                               .000
            +ID2 03:IntEst 7.79
                               .081 1.97 4.32
                                               .000
            +ID3 06:101
                         14.55 1.041 1.62 12.96
                                               .000
            +ID4 09:0VF-xI
                           .00
                               .000 .00 .00
                                               .000
**DRY**
             ______
             SUM 05:ToEast 78.28 2.284 1.92 13.42
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0012-----
*#------
*# External catchment west of the site, containing a portion of existing
*# industrial property, draining east into the site and flowing south.
*#
*#-----|
_____
DESIGN STANDHYD
               Area
                    (ha) = 4.52
50.00
                           PERVIOUS (i)
                   IMPERVIOUS
   Surface Area (ha)=
Dep. Storage (mm)=
                   3.62
                              .90
                             1.50
                     .80
                   5.30
   Average Slope
             (%)=
                             5.30
                  173.59
   Length
              (m) =
                            40.00
                             .250
   Mannings n
                    .013
                  74.85
   Max.eff.Inten.(mm/hr)=
                            22.59
          over (min)
                    2.00
                             12.00
   Storage Coeff. (min)=
                     2.42 (ii)
                             11.97 (ii)
   Unit Hyd. Tpeak (min)=
                            12.00
                    2.00
                             .09
   Unit Hyd. peak (cms)=
                     .49
                                     *TOTALS*
                             .04
                                       .430 (iii)
   PEAK FLOW
             (cms) =
                     .42
   TIME TO PEAK
             (hrs)=
                     1.58
                             1.78
                                      1.583
```

RUNOFF VOLUME TOTAL RAINFALI RUNOFF COEFFIC	L (mm)=	25.00	25.		14.46 25.00 .57	0	
CN* = ! (ii) TIME STI	E STORAGE CO	Dep. Stora LD BE SMALI EFFICIENT.	age (Abo	ve) UAL			
*# *# *# *#		Total Flows	s to the	south			'
ADD HYD (TSouth) ID: N ID1 04:10		(ha)	QPEAK (cms) .078	(hrs)	(mm)	(cms)
	+ID2 01:10	3	4.52	.430	1.58	14.46	.000
		====== outh	15.52	•===== •435	1.58	7.17	.000
NOTE: PEAK FLO	WS DO NOT IN	CLUDE BASEI	FLOWS IF A	ANY.			
*# *# *#	Total Flows		•			•	
*# ADD HYD (TotalF			AREA				 DWF
	ID1 05:To		(ha)	(cms) 2.284	(hrs)	(mm)	(cms)
	+ID2 02:TS	outh	15.52	.435	1.58	7.17	.000

_____ SUM 03:TotalF 93.80 2.426 1.92 12.38 .000

```
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0015-----
 ** END OF RUN:
***********************************
START
               Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
               Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
  TZERO = .00 hrs on
         2 (output = METRIC)
  METOUT=
  NRUN = 002
  NSTORM=
       # 1=Kit2yr.3hr
002:0002-----
*#**********************
*# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
*# Date
         : 01-25-2024
*# Modeller
          : [Amy Kyle, Water Resources Specialist]
  Company
*#
          : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
  for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*#****************************
002:0002-----
                 Filename: 2-yr, 3hr Chicago Storm - Kitchener IDF
I READ STORM
| Ptotal= 34.27 mm|
                 Comments: 2-yr, 3hr Chicago Storm - Kitchener IDF
```

```
.17
            3.094 l
                   .92 36.885
                             1.67 7.027
                                       2.42
                                            3.501
                  1.00 109.401
                             1.75 6.286
         .25
            3.409
                                       2.50
                                            3.326
                             1.83 5.694
         .33
            3.803
                  1.08 47.437
                                      2.58
                                            3.169
         .42 4.314 | 1.17 26.381 |
                             1.92 5.211 | 2.67
                                            3.028
                             2.00 4.807 | 2.75
           5.002 | 1.25 18.051 |
         .50
                                           2.899
         .58 5.982 | 1.33 13.687 |
                            2.08 4.466 2.83
                                          2.783
         .67 7.493 | 1.42 11.030 |
                             2.17 4.173 | 2.92
                                            2.676
         .75 10.127
                  1.50 9.251
                            2.25 3.920 3.00
                                            2.578
002:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#-----|
*#
*#
            Existing internal area draining to the east
*#------
-----
| DESIGN NASHYD |
              Area (ha)= 7.06 Curve Number (CN)=71.00
| 01:105 DT= 1.00 |
               Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
      ----- U.H. Tp(hrs)=
                        .330
  Unit Hyd Qpeak (cms)= .817
  PEAK FLOW
           (cms)=
                 .134 (i)
  TIME TO PEAK
            (hrs)=
                 1.433
                 7.867
  RUNOFF VOLUME
            (mm) =
  TOTAL RAINFALL
             (mm) =
                 34.271
  RUNOFF COEFFICIENT =
                  .230
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0004-----
*#
*#
   Small external area entering site from east and draining south / east
*#-----|
-----
                    (ha)= .73 Curve Number (CN)=70.00
| DESIGN NASHYD |
             Area
| 02:104 DT= 1.00 |
              Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
```

TIME

hrs

.08

RAIN

mm/hr |

2.837

TIME

RAIN

hrs mm/hr

.83 15.850

TIME RAIN

hrs mm/hr |

1.58 7.979

TIME

hrs

2.33

RAIN

mm/hr

3.697

```
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)=
                  .147
  PEAK FLOW (cms)= .018 (i)
TIME TO PEAK (hrs)= 1.250
  RUNOFF VOLUME
            (mm) =
                 7.583
  TOTAL RAINFALL (mm)=
                 34.271
  RUNOFF COEFFICIENT =
                  .221
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0005-----
*#------
*#
*#
             Total existing area draining to the east
*#------|
| ADD HYD (IntEst ) | ID: NHYD AREA
                              QPEAK TPEAK R.V.
                                             DWF
                         (ha) (cms) (hrs) (mm) (cms)
7.06 .134 1.43 7.87 .000
-----
            ID1 01:105
                         .73 .018 1.25 7.58 .000
            +ID2 02:104
            ______
            SUM 03:IntEst
                         7.79 .148 1.42 7.84
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0006-----
*#
*#
            Existing internal area draining to the south
*#-----|
DESIGN NASHYD | Area (ha)= 11.00 Curve Number (CN)=70.00
| 04:106 DT= 1.00 |
               Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)= .540
  Unit Hyd Qpeak (cms)= .778
  PEAK FLOW (cms) = .146 (i)
```

```
TIME TO PEAK (hrs)=
RUNOFF VOLUME (mm)=
                         1.733
7.583
                          7.583
                         34.271
TOTAL RAINFALL (mm)=
RUNOFF COEFFICIENT =
                         .221
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

02:0007					
-					
‡=====================================					
‡ Total Pre-Develop ‡=======					
# #					
" ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '					
# External industr	ial catch	nment and p	art of Hwy 40	1, draining so	uth into the
#			g south / eas		
#					
#					
CALTE CTANEUVE		(1)	FF 04		
CALIB STANDHYD 02:100 DT= 1.00	Area	1 (na)=	55.94 90.00 Din	(%)-	EQ QQ
		ar rmb(%)=	90.00 DII	· · · COIIII · (%)=	30.00
		IMPERVIOL	JS PERVIOUS	(i)	
Surface Area	(ha)=			(-)	
Dep. Storage					
Average Slope					
_			30.00		
Mannings n	=	.020	.250		
Marria CC Tratara /	/ laa \	FO 21	27.61		
Max.eff.Inten.(
Storage Coeff.	(min) (min)=	18 11	27.00 (ii) 26.90	(ii)	
Unit Hyd. Tpeak		18.00	27.00	(11)	
Unit Hyd. peak			.04		
, ,	` ,			*TOTALS	*
PEAK FLOW	(cms) =	2.84	.68	3.293	(iii)
TIME TO PEAK RUNOFF VOLUME TOTAL RAINFALL	(hrs)=	1.27	1.50	1.300	
RUNOFF VOLUME	(mm)=	32.27	11.65	21.959	
TOTAL RAINFALL	(mm)=	34.27	34.27	34.2/1	
RUNOFF COEFFICI	ENT =	.94	.34	.641	

- $CN^* = 64.0$ Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
002:0008-----
*# External catchment containing a portion of Cedar Creek Road, a portion of
        industrial area, and a grassed area near Hwy 401 off-ramp,
*#
*#
          draining south into site and flowing south / east.
*#
*#-----|
                         (ha) = 14.55
DESIGN STANDHYD
                   Area
| 06:101 DT= 1.00 |
                 Total Imp(%)= 60.00 Dir. Conn.(%)=
                                                  48.00
                       IMPERVIOUS
                                  PERVIOUS (i)
   Surface Area
                 (ha)=
                        8.73
                                   5.82
                                    1.50
   Dep. Storage
                 (mm) =
                          .80
                        2.30
   Average Slope
                 (%)=
                                    2.30
   Length
                 (m) =
                        311.45
                                   40.00
   Mannings n
                          .013
                                    .250
   Max.eff.Inten.(mm/hr)=
                       109.40
                                   8.66
            over (min)
                         4.00
                                  22.00
   Storage Coeff. (min)=
                          3.80 (ii) 21.80 (ii)
   Unit Hyd. Tpeak (min)=
                          4.00
                                  22.00
                                    .05
   Unit Hyd. peak (cms)=
                          .29
                                             *TOTALS*
   PEAK FLOW
                (cms) =
                         1.57
                                    .08
                                               1.587 (iii)
   TIME TO PEAK
                (hrs)=
                         1.03
                                    1.42
                                               1.033
   RUNOFF VOLUME
                (mm) =
                         33.47
                                   4.80
                                              18.562
                         34.27
   TOTAL RAINFALL
                 (mm) =
                                   34.27
                                              34.271
   RUNOFF COEFFICIENT =
                         .98
                                    .14
                                               .542
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0009-----
*# External catchment west of site, containing exisiting industrial
```

*# property draining into private SWM feature and then onto site flowing east

*#-----|

------| DESIGN STANDHYD | Area (ha)= 12.64

```
| 07:102 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00
                             IMPERVIOUS PERVIOUS (i)
    Surface Area (ha)=
Dep. Storage (mm)=
Average Slope (%)=
                              10.11
                                             2.53
                           .80
3.10
290.29
                                             1.50
                                             3.10
    Length
                     (m) =
                                           40.00
    Mannings n
                                             .250
                               .013
    Max.eff.Inten.(mm/hr)= 109.40
                                           40.60
                              3.00
                                            12.00
               over (min)
                           3.33 (ii) 12.20 (ii)
3.00 12.00
.35 .09
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
    Unit Hyd. peak (cms)=
                                                          *TOTALS*
                                            .17
    PEAK FLOW
                    (cms)=
                              1.52
                                                           1.577 (iii)
    TOTAL RAINFALL (mm)= 34.27
RUNOFF COEFFICIENT = .98
                   (hrs)=
                                            1.22
                                                           1.017
                                             8.38
                                                          20.926
                                            34.27
                                                          34.271
                                            .24
                                                           .611
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
002:0010-----
*#-----|
*#
                   Infiltration in External SWM Feature
*#-----|
ROUTE RESERVOIR
                     Requested routing time step = 1.0 min.
| IN>07:(102 )
OUT<08:(xSWinf) ======= OUTLFOW STORAGE TABLE =======
_____
                    OUTFLOW STORAGE | OUTFLOW STORAGE

    (cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    .018
    .3759E+00

    .018
    .4380E-01
    .000
    .0000E+00

                         AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) 12.64 1.577 1.017 20.926
    ROUTING RESULTS
                       12.64
12.64
    INFLOW >07: (102 )
   OUTFLOW<08: (xSWinf)
OVERFLOW<09: (OVF-xI)
                                          .967 20.926
.000 .000
                                 .018
                                  .000
                         .00
```

```
TOTAL NUMBER OF SIMULATED OVERFLOWS =
           CUMULATIVE TIME OF OVERFLOWS (hours) = PERCENTAGE OF TIME OVERFLOWING (%) =
                                     .00
                                     .00
           PEAK FLOW REDUCTION [Qout/Qin](%)=
           TIME SHIFT OF PEAK FLOW
                             (min) = -3.00
           MAXIMUM STORAGE USED
                            (ha.m.)=.2478E+00
002:0011-----
*#
*#
             Total existing area draining to the east
*#
*#-----|
| ADD HYD (ToEast ) | ID: NHYD
                         AREA
                             QPEAK
                                  TPEAK R.V.
                                            DWF
                             (cms) (hrs) (mm)
-----
                         (ha)
                                            (cms)
                         55.94 3.293 1.30 21.96
            ID1 02:100
                                            .000
           +ID2 03:IntEst 7.79 .148 1.42 7.84 .000
                    14.55 1.587 1.03 18.56 .000
           +ID3 06:101
           +ID4 09:0VF-xI .00
                              .000
                                   .00 .00
                                            .000
**DRY**
            ______
            SUM 05:ToEast 78.28 3.920 1.28 19.92
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0012-----
*#-----|
*# External catchment west of the site, containing a portion of existing
*# industrial property, draining east into the site and flowing south.
*#-----|
IMPERVIOUS PERVIOUS (i)
```

Surface Area Dep. Storage Average Slope Length Mannings n	(ha)= (mm)= (%)= (m)= =	3.62 .80 5.30 173.59 .013			
Max.eff.Inten.(nover Storage Coeff. Unit Hyd. Tpeak Unit Hyd. peak	(min) (min)= (min)=		9.00 (ii) 9.30	(ii)	
, ,	,			*TOTALS*	
PEAK FLOW	(cms)=	.63	.07	.655	(iii)
TIME TO PEAK	(hrs)=	1.00	1.17	1.000	
RUNOFF VOLUME	(mm)=	33.47	8.38	20.926	
TOTAL RAINFALL	(mm)=	34.27	34.27	34.271	
RUNOFF COEFFICI	ENT =	.98	.24	.611	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0013-----*#------*# *# Total Flows to the south *#-----| -----| ADD HYD (TSouth) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) -----(cms) 11.00 .146 1.73 7.58 ID1 04:106 .000 +ID2 01:103 4.52 .655 1.00 20.93 .000 ______ SUM 02:TSouth 15.52 .662 1.00 11.47 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0014-----

```
*#
*#
           Total Flows from site (eventually to Cedar Creek)
*#
*#------|
_____
| ADD HYD (TotalF ) | ID: NHYD
                         AREA
                              QPEAK TPEAK
                                        R.V.
                                            DWF
                         (ha) (cms) (hrs) (mm)
78.28 3.920 1.28 19.92
-----
                                            (cms)
            ID1 05:ToEast
                                            .000
           +ID2 02:TSouth 15.52 .662 1.00 11.47
                                            .000
            ______
            SUM 03:TotalF
                      93.80
                              4.170 1.27 18.52
                                            .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0015-----
002:0002-----
 ** END OF RUN: 4
************************************
START
          Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
------ Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
  TZERO = .00 hrs on
  METOUT= 2 (output = METRIC)
  NRUN = 005
  NSTORM=
      # 1=Kit5yr.3hr
005:0002-----
*#*********************************
*# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
      : 01-25-2024
```

```
Company
*#
          : Stantec Consulting Ltd. (Waterloo)
*#
  License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*#
  for the 2509 Cedar Creek Road SWM Facility
 The storm events modelled are:
*#
*#
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
005:0002-----
I READ STORM |
               Filename: 5-yr, 3hr Chicago Storm - Kitchener IDF
               Comments: 5-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 47.26 mm|
                    TIME
         TIME
             RAIN
                         RAIN
                               TIME
                                    RAIN |
                                          TIME
                                               RAIN
             mm/hr
                    hrs
                        mm/hr
                               hrs
                                   mm/hr |
                                          hrs
                                              mm/hr
         hrs
         .08
             3.031
                    .83 24.598
                               1.58 11.053
                                          2.33
                                              4.231
         .17
             3.380 l
                    .92 57.395
                              1.67 9.458
                                          2.42
                                              3.949
         .25 3.819 |
                    1.00 139.288
                              1.75 8.241
                                         2.50
                                              3.701
                              1.83 7.286
         .33
             4.385
                   1.08 72.741
                                         2.58
                                              3.483
         .42
             5.141
                              1.92 6.519
                   1.17 42.120
                                         2.67
                                              3.288
            6.195
         .50
                   1.25 28.378
                               2.00 5.892
                                         2.75
                                             3.114
            7.751
          .58
                   1.33 20.884
                               2.08 5.370
                                         2.83
                                             2.957
         .67 10.239
                   1.42 16.280 | 2.17 4.930 | 2.92
                                             2.815
                   1.50 13.216
                               2.25 4.554 | 3.00
         .75 14.725
                                              2.687
  ______
005:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#------
*#
*#
             Existing internal area draining to the east
*#-----|
| DESIGN NASHYD
                Area
                     (ha)=
                           7.06 Curve Number
                                         (CN) = 71.00
| 01:105 DT= 1.00 |
                     (mm) =
                          1.500
                              # of Linear Res.(N)= 3.00
                Ia
                U.H. Tp(hrs)=
                          .330
   Unit Hyd Qpeak (cms)=
                    .817
   PEAK FLOW
             (cms) =
                  .255 (i)
```

: [Amy Kyle, Water Resources Specialist]

*#

Modeller

```
(mm) = 47.258
  TOTAL RAINFALL
                .296
  RUNOFF COEFFICIENT =
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
______
005:0004-----
*#
*#
   Small external area entering site from east and draining south / east
*#-----|
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)= .035 (i)
TIME TO PEAK (hrs)= 1.250
  RUNOFF VOLUME
           ( mm ) =
               13.542
  TOTAL RAINFALL
           (mm) = 47.258
  RUNOFF COEFFICIENT =
                .287
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0005-----
*#------
*#
*#
           Total existing area draining to the east
*#------
| ADD HYD (IntEst ) | ID: NHYD AREA (ha)
                           QPEAK TPEAK R.V.
                                        DWF
                      (ha) (cms) (hrs) (mm)
7.06 .255 1.45 14.00
                                        (cms)
                                       .000
           ID1 01:105
                       .73 .035 1.25 13.54
           +ID2 02:104
                                        .000
           ______
           SUM 03:IntEst
                      7.79 .283 1.42 13.96
                                        .000
```

TIME TO PEAK (hrs)= 1.450

(mm) = 14.005

RUNOFF VOLUME

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
005:0006-----
*#
*#
           Existing internal area draining to the south
*#
*#------|
----- U.H. Tp(hrs)= .540
  Unit Hyd Opeak (cms)= .778
  PEAK FLOW
         (cms) = .278 (i)
           (hrs) = 1.717
  TIME TO PEAK
           (mm) = 13.542
  RUNOFF VOLUME
  TOTAL RAINFALL
            (mm) = 47.258
  RUNOFF COEFFICIENT =
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0007-----
*# Total Pre-Development Drainage Area (Including Large External Catchments)
*#------|
 External industrial catchment and part of Hwy 401, draining south into the
*#
             site and flowing south / east.
*#-----|
______
| CALIB STANDHYD |
            Area (ha) = 55.94
| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00
                IMPERVIOUS
                        PERVIOUS (i)
           (ha)= 44.75
  Surface Area
                        11.19
  Dep. Storage (mm)= 2.00
Average Slope (%)= 1.60
Length (m)= 1500.00
                         5.00
                         2.00
                         30.00
                 .020
                         .250
  Mannings n
               89.81 77.05
  Max.eff.Inten.(mm/hr)=
```

```
15.00
         over (min)
                                   22.00
Storage Coeff. (min)=
                      15.23 (ii) 21.82 (ii)
Unit Hyd. Tpeak (min)=
                      15.00
                                 22.00
                       .07
                                   .05
Unit Hyd. peak (cms)=
                                              *TOTALS*
                      4.46
                                  1.42
PEAK FLOW
             (cms)=
                                               5.512 (iii)
TIME TO PEAK
             (hrs)=
                       1.23
                                  1.42
                                               1.283
RUNOFF VOLUME
             ( mm ) =
                      45.26
                                  20.00
                                              32.629
TOTAL RAINFALL
              (mm) =
                      47.26
                                  47.26
                                              47.258
RUNOFF COEFFICIENT =
                        .96
                                   .42
                                                .690
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
005:0008-----
*# External catchment containing a portion of Cedar Creek Road, a portion of
*#
       industrial area, and a grassed area near Hwy 401 off-ramp,
         draining south into site and flowing south / east.
*#
*#-----|
_____
DESIGN STANDHYD | Area (ha)= 14.55
\mid 06:101 DT= 1.00 \mid Total Imp(%)= 60.00 Dir. Conn.(%)= 48.00
                               PERVIOUS (i)
                     IMPERVIOUS
   Surface Area
              (ha)=
                    8.73
                                 5.82
              (mm)=
   Dep. Storage
                       .80
                                 1.50
                    311.45
.013
   Average Slope
               (%)=
                                 2.30
                (m) =
   Length
                                 40.00
   Mannings n
                                 .250
   Max.eff.Inten.(mm/hr)=
                     139.29
                                19.01
           over (min)
                       3.00
                                17.00
                    3.45 (ii) 16.59 (ii)
3.00 17.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                        .34
   Unit Hyd. peak (cms)=
                                 .07
                                          *TOTALS*
   PEAK FLOW
               (cms) =
                       2.18
                                 .19
                                            2.214 (iii)
                                1.33
   TIME TO PEAK
               (hrs)=
                       1.02
                                           1.017
                      46.46
   RUNOFF VOLUME
              (mm)=
                                 8.80
                                          26.877
               (mm) =
                      47.26
                                47.26
                                          47.258
   TOTAL RAINFALL
   RUNOFF COEFFICIENT =
                       .98
                                 .19
                                            .569
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0009					
*#					
<pre>*# External catchme *# property draining</pre>					wing east
*# property draining	g Into pi I	vace Swii Tea	cui e anu chen o	iito site iio	wing east
*#					
					·
DESIGN STANDHYD	Area	(ha)=	12.64		
07:102 DT= 1.00	7 Tota	$1 \operatorname{Imp}(\%) = 3$	80.00 Dir. Co	nn.(%)= 50	.00
		TMPERVIOUS	PERVIOUS (i)		
Surface Area	(ha)=		• •		
Don Ctonago	(mm) _	90	1 50		
Average Slope Length	(%)=	3.10	3.10		
Length	(m)=	290.29	40.00		
Mannings n	=	.013	.250		
Max.eff.Inten.	(mm/hr)=	139.29	78.90		
	•	3.00			
Storage Coeff.	(min)=	3.02 (i	i) 9.82 (ii)		
Unit Hyd. Tpea	k (min)=	3.00	10.00		
Unit Hyd. peak	(cms)=	.37			
				TOTALS	
PEAK FLOW				2.179 (iii)
			1.20		
			14.68		
TOTAL RAINFALL				47.258	
RUNOFF COEFFIC	IENT =	.98	.31	.647	
(i) CN PROCE	NIDE CELEC	TED EAD DEDV	TOUS 1 OSSES.		
` '		= Dep. Stora			
(ii) TIME STE					
, ,	• •	DEFFICIENT.	LK OK LQOAL		
(iii) PEAK FLO			EFLOW IF ANY.		
(===)	2020				
005:0010					

```
*#
*#
               Infiltration in External SWM Feature
*#-----|
ROUTE RESERVOIR
                Requested routing time step = 1.0 min.
IN>07:(102 )
OUT<08:(xSWinf) ======= OUTLFOW STORAGE TABLE =======
                OUTFLOW STORAGE | OUTFLOW STORAGE
                  (cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | .018 .3759E+00
                   .018 .4380E-01
                                  .000 .0000E+00
   R.V.
                                          (mm)
                                         30.571
  OUTFLOW<08: (xSWinf) 12.64 .018 .917 30.570 OVERFLOW<09: (OVF-xI) .00 .000 .000 .000
                                         0
00.
            TOTAL NUMBER OF SIMULATED OVERFLOWS =
            CUMULATIVE TIME OF OVERFLOWS (hours)=
            PERCENTAGE OF TIME OVERFLOWING (%)=
                                          .00
            PEAK FLOW REDUCTION [Qout/Qin](%)= .826
            TIME SHIFT OF PEAK FLOW (min)= -6.00
            MAXIMUM STORAGE USED
                                (ha.m.)=.3695E+00
005:0011-----
*#
*#
               Total existing area draining to the east
*#-----|
| ADD HYD (ToEast ) | ID: NHYD
                                 QPEAK TPEAK R.V.
                            AREA
                                                  DWF
-----
                                  (cms) (hrs) (mm)
                            (ha)
                                                  (cms)
                            55.94 5.512 1.28 32.63
              ID1 02:100
                                                  .000
             +ID2 03:IntEst 7.79 .283 1.42 13.96 .000
             +ID3 06:101 14.55 2.214 1.02 26.88 .000
             +ID4 09:0VF-xI .00 .000
                                        .00 .00
                                                   .000
**DRY**
              ______
              SUM 05:ToEast 78.28 6.604 1.25 29.70 .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

# industrial property, draining east into # #	· ·	
DESIGN STANDHYD Area (ha)=		I
·		I
01.105 $01-1.00$ 10001 1000	4.52 80.00 Dir. Conn.(%)= 50.00	
IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)= 3.62	.90	
Dep. Storage (mm)= .80		
Average Slope (%)= 5.30		
Length (m)= 173.59		
Mannings n = .013		
Max.eff.Inten.(mm/hr)= 139.29	81.28	
over (min) 2.00		
Storage Coeff. (min)= 1.89 (i	i) 7.61 (ii)	
Unit Hyd. Tpeak (min)= 2.00	8.00	
Unit Hyd. peak (cms)= .58	.15	
	TOTALS	
PEAK FLOW (cms)= .82	.14 .881 (iii)	
	1.15 1.000	
	14.68 30.571	
TOTAL RAINFALL (mm)= 47.26		
RUNOFF COEFFICIENT = .98	.31 .647	
 (i) CN PROCEDURE SELECTED FOR PERV CN* = 50.0 Ia = Dep. Stora (ii) TIME STEP (DT) SHOULD BE SMALL THAN THE STORAGE COEFFICIENT. 	ge (Above) ER OR EQUAL	
(iii) PEAK FLOW DOES NOT INCLUDE BAS	EFLOW IF ANY.	
_		
- 05:0013		

Total Flows to the south

*#

ADD HYD (TSouth) ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
			(cms)			
	ID1 04:106	11.00	.278	1.72	13.54	.000
	+ID2 01:103	4.52	.881	1.00	30.57	.000
	SUM 02:TSouth	15.52			18.50	.000
NOTE: PEAK FLO	WS DO NOT INCLUDE BA	SEFLOWS IF	ANY.			
 -						
05:0014 -						
#						
# #	Total Flows from si	te (eventua	lly to Ce	edar Cre	ek)	
 #	-					
 ADD HYD (TotalF) ID: NHYD	AREA	OPEAK	TPEAK	R.V.	DWF
		(ha)	(cms)	(hrs)	(mm)	(cms)
	ID1 05:ToEast	78.28	6.604	1.25	29.70	.000
	+ID2 02:TSouth	15.52	.895	1.00	18.50	.000
	========= SUM 03:TotalF				27.85	
	WS DO NOT INCLUDE BA	SEFLOWS IF	ANY.			
NOTE: PEAK FLO						
NOTE: PEAK FLO						

```
l START
                  Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
                  Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
           .00 hrs on
   TZERO =
           2 (output = METRIC)
   METOUT=
   NRUN = 010
   NSTORM=
         # 1=Kit10yr.3hr
010:0002-----
*#*********************************
*#
   Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
*#
             : 01-25-2024
*# Modeller
             : [Amy Kyle, Water Resources Specialist]
*#
             : Stantec Consulting Ltd. (Waterloo)
   Company
*# License #
             : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
   The storm events modelled are:
   25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
   and the Regional Event
*#*********************************
010:0002-----
READ STORM
                    Filename: 10-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 56.28 mm|
                    Comments: 10-yr, 3hr Chicago Storm - Kitchener IDF
           TIME
                  RAIN |
                         TIME
                                RAIN |
                                        TIME
                                              RAIN |
                                                      TIME
                                                             RAIN
                 mm/hr
                          hrs
                               mm/hr |
            hrs
                                        hrs
                                             mm/hr
                                                       hrs
                                                            mm/hr
                          .83
            .08
                 3.160
                              29.808
                                        1.58 12.832
                                                      2.33
                                                            4.548
            .17
                 3.560
                          .92
                              70.748
                                        1.67 10.862
                                                      2.42
                                                            4.218
            .25
                          1.00 169.551
                                        1.75
                                                      2.50
                 4.067
                                             9.368
                                                            3.931
            .33
                 4.729
                                                      2.58
                         1.08 89.762
                                        1.83
                                            8.203
                                                            3.678
            .42
                         1.17 51.823
                                        1.92
                                             7.274
                                                      2.67
                 5.623
                                                            3.454
            .50
                 6.884
                         1.25 34.566
                                        2.00
                                              6.519
                                                      2.75
                                                            3.255
                                        2.08
            .58
                 8.770 l
                          1.33 25.132
                                              5.895
                                                      2.83
                                                            3.076
            .67
                11.826
                         1.42 19.351
                                        2.17
                                              5.372
                                                      2.92
                                                            2.915
```

```
.75 17.407 | 1.50 15.520 | 2.25 4.928 | 3.00 2.770
010:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#------|
*#
*#
            Existing internal area draining to the east
*#------|
DESIGN NASHYD
             Area (ha)= 7.06 Curve Number (CN)=71.00
| 01:105 DT= 1.00 |
              Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
 ----- U.H. Tp(hrs)=
                       .330
  Unit Hyd Qpeak (cms)=
                .817
           (cms)=
                .359
1.433
  PEAK FLOW
                 .359 (i)
            (hrs)=
  TIME TO PEAK
            (mm) =
  RUNOFF VOLUME
                18.931
  TOTAL RAINFALL
           (mm) =
                56.282
  RUNOFF COEFFICIENT =
                  .336
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
010:0004-----
*#
*#
   Small external area entering site from east and draining south / east
*#-----|
DESIGN NASHYD
              Area (ha)= .73 Curve Number (CN)=70.00
| 02:104 DT= 1.00 |
             Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)=
                .147
           (cms)=
  PEAK FLOW
                  .050 (i)
   TIME TO PEAK (hrs)=
                1.250
            (mm) =
   RUNOFF VOLUME
                18.339
  TOTAL RAINFALL
           (mm) = 56.282
   RUNOFF COEFFICIENT =
                 .326
```

010:0005-----*#------| *# Total existing area draining to the east *#-----| | ADD HYD (IntEst) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) 7.06 .359 1.43 18.93 (cms) ID1 01:105 .73 .050 1.25 18.34 +ID2 02:104 .000 ______ SUM 03:IntEst 7.79 .399 1.42 18.88 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 010:0006-----*# *# Existing internal area draining to the south *#------| | DESIGN NASHYD | Area (ha)= 11.00 Curve Number (CN)=70.00 ----- U.H. Tp(hrs)= .540 Unit Hyd Qpeak (cms)= .778 (cms)= PEAK FLOW .389 (i) 1.717 TIME TO PEAK (hrs)= RUNOFF VOLUME (mm) =18.340 TOTAL RAINFALL (mm) = 56.282RUNOFF COEFFICIENT = .326 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0007-----

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
*# Total Pre-Development Drainage Area (Including Large External Catchments)
*#-----|
*#
*# External industrial catchment and part of Hwy 401, draining south into the
*#
                  site and flowing south / east.
*#
*#------|
                  Area
| CALIB STANDHYD |
                        (ha) = 55.94
| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
                                                 50.00
                      IMPERVIOUS
                                 PERVIOUS (i)
   Surface Area
                (ha)=
                       44.75
                                  11.19
   Dep. Storage
                (mm) =
                         2.00
                                   5.00
   Average Slope
                (%)=
                        1.60
                                   2.00
   Length
                 (m) =
                       1500.00
                                  30.00
   Mannings n
                                   .250
                        .020
                     112.83
   Max.eff.Inten.(mm/hr)=
                                111.58
           over (min)
                       14.00
                                  20.00
                     13.90 (ii) 19.59 (ii)
14.00 20.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                                    .06
                         .08
                                            *TOTALS*
                        5.73
   PEAK FLOW
               (cms) =
                                  2.08
                                              7.366 (iii)
                        1.22
   TIME TO PEAK
               (hrs)=
                                  1.38
                                              1.267
   RUNOFF VOLUME
                (mm) =
                       54.28
                                  26.44
                                             40.362
   TOTAL RAINFALL
                        56.28
                                 56.28
                                             56.282
                (mm) =
   RUNOFF COEFFICIENT =
                         .96
                                   .47
                                              .717
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 64.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

*# External catchment containing a portion of Cedar Creek Road, a portion of
*# industrial area, and a grassed area near Hwy 401 off-ramp,

*# draining south into site and flowing south / east.

*#-----|

```
DESIGN STANDHYD
                     Area (ha)= 14.55
| 06:101 DT= 1.00 |
                     Total Imp(\%) = 60.00 Dir. Conn.(\%) = 48.00
                           IMPERVIOUS
                                        PERVIOUS (i)
    Surface Area (ha)=
                              8.73
                                           5.82
    Dep. Storage
                   (mm)=
                                           1.50
                               .80
                          2.30
311.45
.013
                   (%)=
    Average Slope
                                           2.30
    Length
                     (m) =
                                          40.00
    Mannings n
                              .013
                                           .250
    Max.eff.Inten.(mm/hr)=
                            169.55
                                          29.79
              over (min) 3.00 14.00 eff. (min)= 3.19 (ii) 14.17 (ii) Tpeak (min)= 3.00 14.00 08
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
    Unit Hyd. peak (cms)=
                               .36
                                          .08
                                                       *TOTALS*
    PEAK FLOW
                   (cms)=
                              2.71
                                           .29
                                                         2.782 (iii)
                             1.02
    TIME TO PEAK
                   (hrs)=
                                          1.28
                                                        1.017
                          55.48
                                         12.13
    RUNOFF VOLUME
                    (mm) =
                                                       32.940
    TOTAL RAINFALL
                    (mm) =
                             56.28
                                         56.28
                                                       56.282
    RUNOFF COEFFICIENT =
                              .99
                                           .22
                                                         .585
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
010:0009-----
*# External catchment west of site, containing exisiting industrial
*# property draining into private SWM feature and then onto site flowing east
*#-----|
______
DESIGN STANDHYD
              Area (ha) = 12.64
IMPERVIOUS
                          PERVIOUS (i)
                .80
3.10
290.20
   Surface Area
                 10.11
                            2.53
             (ha)=
   Dep. Storage
             (mm) =
                            1.50
   Average Slope
            (%)=
                            3.10
   Length
              (m) =
                            40.00
                            .250
   Mannings n
                   .013
   Max.eff.Inten.(mm/hr)=
                 169.55
                           112.10
```

```
over (min)
                             3.00
                                           9.00
Storage Coeff. (min)=
                                           8.70 (ii)
                             2.79 (ii)
Unit Hyd. Tpeak (min)=
                             3.00
                                           9.00
Unit Hyd. peak (cms)=
                              .39
                                            .13
                                                       *TOTALS*
PEAK FLOW
                (cms) =
                             2.53
                                            .52
                                                         2.765 (iii)
TIME TO PEAK
                (hrs)=
                             1.02
                                          1.17
                                                         1.017
RUNOFF VOLUME
                 (mm) =
                            55.48
                                          19.71
                                                        37.598
                 (mm) =
TOTAL RAINFALL
                            56.28
                                          56.28
                                                        56.282
RUNOFF COEFFICIENT =
                              .99
                                            .35
                                                          .668
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 010:0010 *# *# *# *# *#	Infilt	ration in	External :	SWM Featur	e		
ROUTE RESERVOIF IN>07:(102) OUT<08:(xSWinf))) ====: OUTF (cr	ested rout ==== OUT LOW STO ms) (ha 200 .0000 218 .4380	LFOW STORARAGE .m.) E+00	AGE TABLE OUTFLOW (cms)	====== STORAGE (ha.m.) .3759E+00		
	JLTS						
INFLOW >07:	(102) (xSWinf) (OVF-xI)	12.64 10.45	2.765 .018	1.017 .883	37.598 37.596		
	TOTAL NUMB CUMULATIVE PERCENTAGE	TIME OF O	VERFLOWS	(hours)=	1.57		
	PEAK FLOI TIME SHIFT MAXIMUM S	OF PEAK F	LOW		-8.00		

```
010:0011-----
*#
*#
             Total existing area draining to the east
*#
*#------|
| ADD HYD (ToEast ) | ID: NHYD AREA
                            OPEAK
                                 TPEAK R.V.
                                          DWF
_____
                       (ha)
                            (cms) (hrs) (mm)
                                          (cms)
                       55.94 7.366 1.27 40.36
           ID1 02:100
                                          .000
           +ID2 03:IntEst 7.79 .399 1.42 18.88 .000
           +ID3 06:101 14.55 2.782 1.02 32.94 .000
           +ID4 09:0VF-xI 2.19 .422 1.60 37.60
                                          .000
            ______
            SUM 05:ToEast
                     80.47 8.840 1.22 36.86
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
______
010:0012-----
*#------
*# External catchment west of the site, containing a portion of existing
*# industrial property, draining east into the site and flowing south.
*#-----|
DESIGN STANDHYD | Area (ha)= 4.52
| 01:103 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00
______
                IMPERVIOUS PERVIOUS (i)
  Surface Area (ha)= 3.62

Dep. Storage (mm)= .80

Average Slope (%)= 5.30

Length (m)= 173.59
                          .90
                          1.50
                          5.30
                         40.00
  Mannings n
                          .250
                  .013
```

Unit Hyd. peak	(cms)=	.61	.17	
•				*TOTALS*
PEAK FLOW	(cms)=	1.01	.21	1.112 (iii)
TIME TO PEAK	(hrs)=	1.00	1.12	1.000
RUNOFF VOLUME	(mm)=	55.48	19.71	37.598
TOTAL RAINFALL	(mm) =	56.28	56.28	56.282
RUNOFF COEFFICI	ENT =	.99	.35	.668

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*# *# *#	Total Flo	ows to the	south			
ADD HYD (TSouth		AREA (ha)		TPEAK (hrs)	R.V. (mm)	DWF (cms)
	+ID2 01:103	4.52	1.112	1.00	37.60	.000
	SUM 02:TSouth		1.133		====== 23.95	 000.

*# Total Flows from site (eventually to Cedar Creek) *#-----| | ADD HYD (TotalF) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) (cms) 8.840 80.47 1.22 36.86 ID1 05:ToEast .000 +ID2 02:TSouth 15.52 1.133 1.00 23.95 .000

SUM 03:TotalF 95.99 9.434 1.22 34.78 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 010:0015-----010:0002-----010:0002-----** END OF RUN : 24 *********************************** Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\ START Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\ TZERO = .00 hrs onMETOUT= 2 (output = METRIC) NRUN = 025 NSTORM= # 1=Kit25yr.3hr 025:0002-----*#******************************** *# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214] *# Date : 01-25-2024 : [Amy Kyle, Water Resources Specialist] *# Modeller Company : Stantec Consulting Ltd. (Waterloo)

```
*#
 License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
 The storm events modelled are:
*#
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*#*********************************
025:0002-----
| READ STORM |
               Filename: 25-yr, 3hr Chicago Storm - Kitchener IDF
              Comments: 25-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 68.26 mm|
         TIME
             RAIN
                    TIME
                        RAIN
                               TIME
                                    RAIN |
                                          TIME
                                                RAIN
                    hrs
                        mm/hr |
         hrs
            mm/hr
                               hrs
                                   mm/hr
                                           hrs
                                               mm/hr
          .08
             3.567
                    .83 38.324
                               1.58 16.257
                                          2.33
                                               5.336
             4.072
                    .92 87.426
          .17
                               1.67 13.647
                                         2.42
                                               4.912
          .25
             4.719
                    1.00 191.557
                               1.75 11.668
                                         2.50
                                               4.544
                               1.83 10.127
          .33
             5.571
                    1.08 109.318
                                          2.58
                                               4.222
          .42
             6.733 | 1.17 65.637 |
                              1.92 8.900
                                         2.67
                                              3.938
             8.387 | 1.25 44.391 |
                              2.00 7.906
                                         2.75
          .50
                                              3.686
          .58 10.876
                    1.33 32.362
                              2.08 7.088 | 2.83
                                               3.461
          .67 14.925
                    1.42 24.846
                               2.17 6.405
                                          2.92
                                               3.260
          .75 22.291
                    1.50 19.811
                               2.25 5.829
                                          3.00
                                               3.079
025:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#-----|
*#
*#
             Existing internal area draining to the east
*#------|
DESIGN NASHYD
                Area
                     (ha) = 7.06 Curve Number (CN) = 71.00
                Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
| 01:105 DT= 1.00 |
----- U.H. Tp(hrs)=
                         .330
   Unit Hyd Qpeak (cms)=
                     .817
   PEAK FLOW
              (cms) =
                    .498 (i)
   TIME TO PEAK
             (hrs)=
                   1.450
   RUNOFF VOLUME
              (mm) =
                   26.137
```

```
RUNOFF COEFFICIENT = .383
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0004-----
*#
   Small external area entering site from east and draining south / east
*#
*#------
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)= .068 (i)
              1.250
  TIME TO PEAK
          (hrs)=
              25.376
  RUNOFF VOLUME
           (mm) =
  TOTAL RAINFALL (mm)= 68.256
  RUNOFF COEFFICIENT = .372
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0005-----
*#------
*#
           Total existing area draining to the east
*#-----|
______
| ADD HYD (Intest ) | ID: NHYD AREA QPEAK TPEAK R.V.
                                       DWF
                     (ha)
                     (ha) (cms) (hrs) (mm) (cms)
7.06 .498 1.45 26.14 .000
-----
           ID1 01:105
                  .73 .068 1.25 25.38 .000
          +ID2 02:104
           ______
```

SUM 03:IntEst 7.79 .553 1.42 26.07 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

TOTAL RAINFALL (mm)= 68.256

```
025:0006-----
*#
*#
           Existing internal area draining to the south
*#
*#------|
----- U.H. Tp(hrs)= .540
  Unit Hyd Qpeak (cms)= .778
  PEAK FLOW (cms)= .544 (i)
  TIME TO PEAK (hrs)= 1.717
  RUNOFF VOLUME
            (mm) =
                25.376
  TOTAL RAINFALL (mm)= 68.256
  RUNOFF COEFFICIENT =
                 .372
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
______
025:0007-----
*# Total Pre-Development Drainage Area (Including Large External Catchments)
*#------|
*# External industrial catchment and part of Hwy 401, draining south into the
*#
              site and flowing south / east.
*#
*#------
| CALIB STANDHYD | Area (ha)= 55.94
| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00
                 IMPERVIOUS PERVIOUS (i)
  Surface Area (ha)= 44.75

Dep. Storage (mm)= 2.00

Average Slope (%)= 1.60

Length (m)= 1500.00
                          11.19
                          5.00
                           2.00
                          30.00
  Mannings n
                  .020
                          .250
              =
  Max.eff.Inten.(mm/hr)= 135.90 155.96
over (min) 13.00 18.00
Storage Coeff. (min)= 12.90 (ii) 17.88 (ii)
```

```
Unit Hyd. Tpeak (min)= 13.00
                                 18.00
Unit Hyd. peak (cms)=
                      .09
                                  .06
                                            *TOTALS*
PEAK FLOW
           (cms)=
                      7.08
                                 2.96
                                             9.560 (iii)
TIME TO PEAK (hrs)=
                     1.20
                                 1.35
                                             1.250
                   66.25
                               35.57
RUNOFF VOLUME
            (mm) =
                                            50.915
TOTAL RAINFALL
             (mm) =
                     68.26
                                68.26
                                           68.256
RUNOFF COEFFICIENT =
                      .97
                                              .746
                                  .52
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

______ 025:0008-----*#*%-------|----|------| *# External catchment containing a portion of Cedar Creek Road, a portion of industrial area, and a grassed area near Hwy 401 off-ramp, *# draining south into site and flowing south / east. *#-----| DESIGN STANDHYD | Area (ha)= 14.55 \mid 06:101 DT= 1.00 \mid Total Imp(%)= 60.00 Dir. Conn.(%)= 48.00 IMPERVIOUS PERVIOUS (i) Surface Area (ha)= 8.73
Dep. Storage (mm)= .80
Average Slope (%)= 2.30 5.82 8.73 1.50 2.30 Length (m) = 311.4540.00 .250 Mannings n .013 Max.eff.Inten.(mm/hr)= 191.56 42.07 3.00 Unit Hyd. Tpeak (min)= 3.03 (ii) 12.60 (ii) 13.00 13.00 13.00 Unit Hyd. peak (cms)= .37 over (min) 13.00 *TOTALS* .44 PEAK FLOW (cms)= 3.14 3.259 (iii) 1.27 TIME TO PEAK (hrs)= 1.02 1.017 67.46 68.26 RUNOFF VOLUME 17.15 41.299 (mm) =TOTAL RAINFALL (mm)= 68.26 68.256 RUNOFF COEFFICIENT = .99 .25 .605

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

```
CN* = 50.0 Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
```

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0009-----*# *# External catchment west of site, containing exisiting industrial *# property draining into private SWM feature and then onto site flowing east *#-----| _____ | DESIGN STANDHYD | Area (ha) = 12.64| 07:102 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00 IMPERVIOUS PERVIOUS (i) Surface Area (ha)= 10.11 2.53 (mm) =Dep. Storage .80 1.50 Average Slope 3.10 (%)= 3.10 (%)= 3.10 (m)= 290.29 Length 40.00 .013 Mannings n .250 191.56 Max.eff.Inten.(mm/hr)= 150.65 over (min) 3.00 8.00 2.66 (ii) 7.91 (ii) 3.00 8.00 Storage Coeff. (min)= Unit Hyd. Tpeak (min)= .41 Unit Hyd. peak (cms)= .14 *TOTALS* PEAK FLOW (cms)= 2.92 .73 3.301 (iii) ./3 1.17 27.04 1.02 TIME TO PEAK (hrs)=1.017 67.46 RUNOFF VOLUME (mm) = 47.250 TOTAL RAINFALL (mm) =68.26 68.26 68.256 RUNOFF COEFFICIENT = .99 .40 .692 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT. (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY. ______

025:0010-----

*#------

Infiltration in External SWM Feature

*#

*#

```
*#
*#------|
ROUTE RESERVOIR
               Requested routing time step = 1.0 min.
| IN>07:(102 ) |
OUT<08:(xSWinf) | ======= OUTLFOW STORAGE TABLE =======
               OUTFLOW STORAGE | OUTFLOW STORAGE
                             (cms)
                 (cms)
                      (ha.m.)
                                     (ha.m.)
                  .000 .0000E+00 | .018 .3759E+00
.018 .4380E-01 | .000 .0000E+00
                 .000 .0000E+00
  TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                       4
            CUMULATIVE TIME OF OVERFLOWS (hours) = 1.87
PERCENTAGE OF TIME OVERFLOWING (%) = 1.37
                     REDUCTION [Qout/Qin](%)=
            PEAK FLOW
                                      .545
            TIME SHIFT OF PEAK FLOW (min)= -10.00
            MAXIMUM STORAGE USED
                             (ha.m.)=.3759E+00
*#
*#
              Total existing area draining to the east
*#-----|
7.79 .553 1.42 26.07
            +ID2 03:IntEst
                                               .000
            +ID3 06:101 14.55 3.259 1.02 41.30 .000
            +ID4 09:0VF-xI 4.32 1.421 1.28 47.25
                                                .000
             _______
             SUM 05:ToEast 82.60 12.689 1.28 46.69 .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
025:0012-----
*#-----|
*# External catchment west of the site, containing a portion of existing
*# industrial property, draining east into the site and flowing south.
*#
*#-----|
| DESIGN STANDHYD |
                 Area (ha) = 4.52
IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)=
Dep. Storage (mm)=
Average Slope (%)=
                      3.62
                                 .90
                   .80
5.30
173.59
                       .80
                                1.50
                                5.30
   Length
               (m)=
                              40.00
                      .013
   Mannings n
                                .250
   Max.eff.Inten.(mm/hr)=
                   191.56
                              159.27
           over (min)
                       2.00
                                6.00
   Storage Coeff. (min)=
                       1.66 (ii) 6.04 (ii)
   Unit Hyd. Tpeak (min)=
                      2.00
                               6.00
   Unit Hyd. peak (cms)=
                       .63
                                .19
                                         *TOTALS*
                     1.15
1.00
   PEAK FLOW
              (cms)=
                                . 29
                                          1.319 (iii)
                               1.12
   TIME TO PEAK
              (hrs)=
                                          1.000
                   67.46
68.26
   RUNOFF VOLUME
               (mm) =
                               27.04
                                         47.250
   TOTAL RAINFALL (mm)=
                      68.26
                               68.26
                                         68.256
   RUNOFF COEFFICIENT =
                                .40
                      .99
                                           .692
    (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
       CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
       THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0013----
*#-----|
*#
*#
                    Total Flows to the south
```

*#-----|

ADD HYD (TSouth) ID: NHYD ID1 04:106	AREA (ha) 11.00	QPEAK (cms) .544	TPEAK (hrs) 1.72	R.V. (mm) 25.38	DWF (cms) .000
	+ID2 01:103		1.319			
	SUM 02:TSouth	15.52			31.75	
NOTE: PEAK FLOW	S DO NOT INCLUDE BASEF	LOWS IF	ANY.			
*#	Total Flows from site		-		•	
ADD HYD (TotalF) ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
		(ha)	(cms) 12.689	(hrs)	(mm)	(cms)
	ID1 05:ToEast	82.60	12.689	1.28	46.69	.000
	+ID2 02:TSouth	15.52	1.350	1.00	31.75	.000
	SUM 03:TotalF				44.32	.000
NOTE: PEAK FLOW	S DO NOT INCLUDE BASEF	LOWS IF	ANY.			
 025:0015						
025:0002						
025:0002						
025:0002						

```
025:0002-----
 ** END OF RUN: 49
**********************************
l START
              Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
TZERO = .00 hrs on
        2 (output = METRIC)
  METOUT=
  NRUN = 050
  NSTORM=
       # 1=Kit50yr.3hr
050:0002-----
*#**********************************
*# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
*# Date
      : 01-25-2024
*# Modeller
           : [Amy Kyle, Water Resources Specialist]
*# Company : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*#
  for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*±**********************************
050:0002-----
READ STORM
                Filename: 50-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 77.24 mm|
                Comments: 50-yr, 3hr Chicago Storm - Kitchener IDF
              RAIN
                     TIME
                           RAIN
                                 TIME
                                       RAIN
         TIME
                                             TIME
                                                   RAIN
          hrs
              mm/hr |
                      hrs
                          mm/hr |
                                 hrs mm/hr
                                             hrs
                                                  mm/hr
                      .83 44.095
              3.816 |
                                 1.58 18.483
                                                  5.829
          .08
                                             2.33
                      .92 99.987
          .17
              4.387
                                 1.67 15.446
                                             2.42
                                                  5.344
```

```
.42 7.433 | 1.17 75.450 |
                        1.92 9.934 | 2.67 4.235
        .50 9.341 | 1.25 51.107 | 2.00 8.785 | 2.75 3.950
        .58 12.226 | 1.33 37.204 |
.67 16.932 | 1.42 28.478 |
                        2.08 7.841 | 2.83 3.697
                        2.17 7.055 2.92 3.470
        .75 25.505 | 1.50 22.619 | 2.25 6.393 | 3.00 3.267
050:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#------|
*#
*#
           Existing internal area draining to the east
*#-----|
| DESIGN NASHYD | Area (ha)= 7.06 Curve Number (CN)=71.00
| 01:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .330
  Unit Hyd Qpeak (cms)= .817
  PEAK FLOW (cms) = .616 (i)
  TIME TO PEAK (hrs)=
              1.450
  RUNOFF VOLUME
          (mm) =
               31.959
  TOTAL RAINFALL
              77.237
           (mm) =
  RUNOFF COEFFICIENT =
                .414
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0004-----
*#
*#
   Small external area entering site from east and draining south / east
*#-----|
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
```

.25 5.123 | 1.00 214.691 | 1.75 13.144 | 2.50 4.924

1.83 11.355 | 2.58 4.558

.33 6.098 | 1.08 124.641 |

```
RUNOFF COEFFICIENT = .402
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0005-----
*#-----|
*#
*#
           Total existing area draining to the east
*#-----|
______
                      (ha) (cms) (hrs) (mm)
7.06 .616 1 45 37 65
| ADD HYD (IntEst ) | ID: NHYD
                                        DWF
                                       (cms)
           ID1 01:105
                                       .000
                   .73 .084 1.25 31.07
          +ID2 02:104
                                       .000
           ______
                      7.79 .684 1.42 31.88
           SUM 03:IntEst
                                        .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
050:0006-----
*#
*#
          Existing internal area draining to the south
*#------
----- U.H. Tp(hrs)= .540
  Unit Hyd Qpeak (cms)= .778
  PEAK FLOW
           (cms) = .673 (i)
               1.717
  TIME TO PEAK
           (hrs)=
  RUNOFF VOLUME
           (mm)=
               31.074
  TOTAL RAINFALL
           (mm) = 77.237
  RUNOFF COEFFICIENT =
                .402
```

PEAK FLOW (cms)= .084 (i) TIME TO PEAK (hrs)= 1.250

(mm) =

(mm) =

31.074

77.237

RUNOFF VOLUME

TOTAL RAINFALL

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY. *# Total Pre-Development Drainage Area (Including Large External Catchments) *#-----| *# External industrial catchment and part of Hwy 401, draining south into the *# site and flowing south / east. *# *#------| | CALIB STANDHYD | Area (ha) = 55.94| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00 Surface Area (ha)= 44.75
Dep. Storage (mm)= 2.00
Average Slope (%)= 1.60
(m)= 1500.00 IMPERVIOUS PERVIOUS (i) 11.19 5.00 2.00 30.00 Mannings n .020 .250 158.05 Max.eff.Inten.(mm/hr)= 194.43 12.00 over (min) 17.00 Storage Coeff. (min)= 12.00 17.00 .09 12.15 (ii) 16.70 (ii) Unit Hyd. Tpeak (min)= Unit Hyd. peak (cms)= *TOTALS* 8.29 3.74 PEAK FLOW (cms) =11.442 (iii) (hrs)= TIME TO PEAK 1.18 1.32 1.233 75.23 77.24 .97 RUNOFF VOLUME (mm) =42.76 58.997 TOTAL RAINFALL (mm)= 77.24 77.237 .97 RUNOFF COEFFICIENT = .55 .764 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 64.0$ Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT. (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0008-----

```
*#
*# External catchment containing a portion of Cedar Creek Road, a portion of
*#
        industrial area, and a grassed area near Hwy 401 off-ramp,
           draining south into site and flowing south / east.
*#
*#-----|
______
                   Area (ha) = 14.55
| DESIGN STANDHYD |
| 06:101 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)=
                       IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)= 8.73

Dep. Storage (mm)= .80

Average Slope (%)= 2.30

Length (m)= 311.45
                                    5.82
                                     1.50
                                    2.30
                                  40.00
                         .013
                                    .250
   Mannings n
   Max.eff.Inten.(mm/hr)=
                      214.69
                                   54.05
                          3.00
                                   12.00
            over (min)
                         2.90 (ii) 11.55 (ii)
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                          3.00 12.00
   Unit Hyd. peak (cms)=
                                     .10
                           .38
                                               *TOTALS*
                                   .57
1.25
                        3.56
1.02
   PEAK FLOW
               (cms)=
                                                 3.739 (iii)
   TIME TO PEAK (hrs)=
                                                1.017
   RUNOFF COEFFICIENT = 99
   RUNOFF VOLUME
                (mm) =
                         76.44
                                   21.32
                                               47.778
                                    77.24
                                               77.237
                         .99
                                     .28
                                                 .619
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0009----
*#
*# External catchment west of site, containing exisiting industrial
*# property draining into private SWM feature and then onto site flowing east
*#
*#-----|
-----
DESIGN STANDHYD
                  Area (ha) = 12.64
                  Total Imp(\%) = 80.00 Dir. Conn.(\%) = 50.00
07:102 DT= 1.00
                       IMPERVIOUS PERVIOUS (i)
```

2.53

Surface Area (ha)= 10.11

```
Dep. Storage (mm)=
                       .80
3.10
                                     1.50
Average Slope
               (%)=
                                    3.10
                        290.29
                                    40.00
Length
                (m)=
Mannings n
                        .013
                                     .250
                =
Max.eff.Inten.(mm/hr)=
                    214.69
                                   188.85
                       3.00
                                    7.00
         over (min)
Storage Coeff. (min)=
                        2.54 (ii) 7.34 (ii)
Unit Hyd. Tpeak (min)=
                         3.00
                                    7.00
Unit Hyd. peak (cms)=
                         .42
                                     .16
                                                *TOTALS*
                                     .93
PEAK FLOW
                        3.30
             (cms)=
                                                  3.858 (iii)
TIME TO PEAK
             (hrs)=
                        1.02
                                    1.13
                                                  1.017
                    76.44
77.24
RUNOFF VOLUME
               (mm) =
                                   32.95
                                                 54.694
                                   77.24
TOTAL RAINFALL
               (mm) =
                                                77.237
RUNOFF COEFFICIENT =
                        .99
                                    .43
                                                 .708
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0010-----*#-----| *# *# Infiltration in External SWM Feature *#-----| ROUTE RESERVOIR Requested routing time step = 1.0 min. IN>07:(102) | OUT<08:(xSWinf) | ====== OUTLFOW STORAGE TABLE ====== STORAGE | OUTFLOW STORAGE OUTFLOW (cms) (ha.m.) (cms) (ha.m.) .000 .0000E+00 .018 .3759E+00 .000 .0000E+00 .018 .4380E-01 AREA ROUTING RESULTS QPEAK TPEAK R.V. (ha) (cms) (hrs) -----(mm) INFLOW >07: (102) 12.64 1.017 3.858 54.694 OUTFLOW<08: (xSWinf) 7.19 .817 .018 54.693 OVERFLOW<08: (XSW1n+)
OVERFLOW<09: (OVF-xI) 5.45 1.200 54.694 2.263 TOTAL NUMBER OF SIMULATED OVERFLOWS = 2

CUMULATIVE TIME OF OVERFLOWS (hours)=

PERCENTAGE OF TIME OVERFLOWING (%)=

1.97

1.44

```
050:0011-----
*#
*#
             Total existing area draining to the east
*#-----|
| ADD HYD (ToEast
           ) | ID: NHYD AREA
                             QPEAK TPEAK R.V.
                                            DWF
_____
                        (ha)
                             (cms) (hrs) (mm)
                                            (cms)
            ID1 02:100
                        55.94
                             11.442 1.23 59.00
                                            .000
           +ID2 03:IntEst 7.79 .684 1.42 31.88
                                           .000
           +ID3 06:101
                        14.55 3.739 1.02 47.78
                                            .000
           +ID4 09:0VF-xI 5.45 2.263 1.20 54.69
                                            .000
            ______
            SUM 05:ToEast 83.73
                             16.169 1.20 54.24
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
*#-----|
*# External catchment west of the site, containing a portion of existing
*# industrial property, draining east into the site and flowing south.
*#------|
| DESIGN STANDHYD |
                   (ha) = 4.52
              Area
IMPERVIOUS
                          PERVIOUS (i)
  Surface Area (ha)=
                            .90
                    3.62
            (mm) =
  Dep. Storage
                   .80
                           1.50
  Average Slope
            (%)=
                   5.30
                           5.30
  Length
             (m) =
                  173.59
                           40.00
```

REDUCTION [Qout/Qin](%)=

TIME SHIFT OF PEAK FLOW (min)= -12.00

.467

(ha.m.)=.3759E+00

PEAK FLOW

MAXIMUM STORAGE USED

Mannings n	=	.013	.250		
Max.eff.Inten.(r	nm/hr)=	214.69	195.13		
over	(min)	2.00	6.00		
Storage Coeff.	(min)=	1.59	(ii) 5.62	(ii)	
Unit Hyd. Tpeak	(min)=	2.00	6.00		
Unit Hyd. peak	(cms)=	.64	.20		
				TOTALS	
PEAK FLOW	(cms)=	1.30	.36	1.513	(iii)
TIME TO PEAK	(hrs)=	1.00	1.10	1.000	
RUNOFF VOLUME	(mm) =	76.44	32.95	54.694	
TOTAL RAINFALL	(mm) =	77.24	77.24	77.237	
RUNOFF COEFFICIE	ENT =	.99	.43	.708	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*# *#

	-					
# # #	Total F1	ows to the				
ADD HYD (TSouth) ID: NHYD		(CMS)		R.V. (mm)	
	ID1 04:106		.673			
	+ID2 01:103	4.52	1.513	1.00	54.69	.000
	==========	:=======	======		======	
	SUM 02:TSouth	15.52	1.554	1.00	37.95	.000
	SUM 02:TSOUTH	15.52	1.554	1.00	37.95	.00

Total Flows from site (eventually to Cedar Creek)

ADD HYD (TotalF	ID1 05:ToEast	83.73	QPEAK (cms) 16.169	1.20	(mm) 54.24	(cms) .000
	+ID2 02:TSouth	15.52	1.554	1.00	37.95	.000
	SUM 03:TotalF	99.25	17.136		51.70	.000
NOTE: PEAK FLO	WS DO NOT INCLUDE BAS	SEFLOWS IF	ANY.			
** END OF RUN :	99					
*******	********	*******	******	*****	*****	*****
START	 Project dir.: C:	:\SWMHYMO\(CEDARC~1\2	202401~4	.\	
	Rainfall dir.: C:	:\SWMHYMO\(CEDARC~1\2	202401~4	.\	

```
TZERO =
         .00 hrs on
  METOUT=
         2 (output = METRIC)
  NRUN = 100
  NSTORM=
       # 1=Kit100yr.3hr
100:0002-----
*#********************************
  Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
*#
*#
          : 01-25-2024
*#
          : [Amy Kyle, Water Resources Specialist]
  Modeller
*#
  Company
          : Stantec Consulting Ltd. (Waterloo)
*#
  License #
          : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*#
  for the 2509 Cedar Creek Road SWM Facility
  The storm events modelled are:
*#
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*#**********************
______
100:0002-----
READ STORM
                Filename: 100-yr, 3hr Chicago Storm - Kitchener ID
                Comments: 100-yr, 3hr Chicago Storm - Kitchener ID
| Ptotal= 87.07 mm|
              RAIN |
                          RAIN |
         TIME
                     TIME
                                TIME
                                      RAIN |
                                            TIME
                                                 RAIN
                         mm/hr |
          hrs
              mm/hr
                     hrs
                                 hrs
                                     mm/hr
                                            hrs
                                                mm/hr
          .08
              4.087
                     .83 50.502
                                1.58 20.973
                                            2.33
                                                6.373
          .17
              4.733 |
                     .92 113.675
                                1.67 17.458
                                            2.42
                                                5.820
              5.569
                     1.00 239.354
                                1.75 14.796
                                                5.342
          . 25
                                           2.50
          .33
              6.681
                     1.08 141.249
                                1.83 12.729
                                            2.58
                                                4.926
                                1.92 11.089
          .42
              8.210
                     1.17 86.233
                                           2.67
                                                4.561
          .50 10.405
                     1.25 58.548
                                2.00
                                           2.75
                                                4.239
                                    9.765
                     1.33 42.595
                                2.08
                                            2.83
                                                3.953
          .58 13.734
                                     8.679
                     1.42 32.533
                                2.17
                                     7.777
                                            2.92
                                                3.698
          .67
             19.179
          .75 29.096
                     1.50 25.760
                                2.25
                                     7.018
                                            3.00
                                                3.469
100:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#-----|
```

```
*#
*#
               Existing internal area draining to the east
*#-----|
DESIGN NASHYD
                Area (ha)= 7.06 Curve Number (CN)=71.00
Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 01:105 DT= 1.00 |
----- U.H. Tp(hrs) = .330
   Unit Hyd Qpeak (cms)= .817
   PEAK FLOW (cms) = .752 (i)
   TIME TO PEAK (hrs)=
                    1.433
               (mm) =
   RUNOFF VOLUME
                    38.675
   TOTAL RAINFALL (mm)=
                    87.067
   RUNOFF COEFFICIENT = .444
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#
*#
    Small external area entering site from east and draining south / east
*#-----|
                 Area (ha)= .73 Curve Number (CN)=70.00
DESIGN NASHYD
| 02:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .190
   Unit Hyd Qpeak (cms)= .147
   PEAK FLOW (cms)= .103 (i)
   TIME TO PEAK
              (hrs)=
                    1.250
   RUNOFF VOLUME
               (mm) =
                    37.658
              (mm)=
                    87.067
   TOTAL RAINFALL
   RUNOFF COEFFICIENT = .433
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#------
*#
                Total existing area draining to the east
*#
```

```
*#------
_____
         ) | ID: NHYD AREA QPEAK TPEAK R.V.
----- (ha) (cms) (hrs) (mm)
| ADD HYD (IntEst
                                     DWF
-----
                        (cms) (hrs) (mm)
                                    (cms)
                    7.06 .752 1.43 38.68
          ID1 01:105
                                    .000
                  .73 .103 1.25 37.66
         +ID2 02:104
                                    .000
          ______
          SUM 03:IntEst 7.79 .836 1.42 38.58 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0006-----
*#
*#
         Existing internal area draining to the south
*#-----|
-----
----- U.H. Tp(hrs)= .540
  Unit Hyd Qpeak (cms)= .778
  PEAK FLOW (cms)= .823 (i)
  TIME TO PEAK (hrs)=
              1.700
  RUNOFF VOLUME
          (mm) =
             37.659
  TOTAL RAINFALL (mm)= 87.067
  RUNOFF COEFFICIENT = .433
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0007-----
*# Total Pre-Development Drainage Area (Including Large External Catchments)
*#-----|
*# External industrial catchment and part of Hwy 401, draining south into the
           site and flowing south / east.
*#
*#-----|
```

```
(ha) = 55.94
CALIB STANDHYD
                       Area
| 02:100 DT= 1.00 |
                      Total Imp(%)= 80.00 Dir. Conn.(%)=
                                                               50.00
                            IMPERVIOUS
                                          PERVIOUS (i)
    Surface Area
                    (ha)=
                               44.75
                                            11.19
    Dep. Storage
                                            5.00
                    (mm) =
                               2.00
    Average Slope
                     (%)=
                                1.60
                                            2.00
    Length
                      (m) =
                             1500.00
                                            30.00
    Mannings n
                                .020
                                             .250
                       =
    Max.eff.Inten.(mm/hr)=
                             177.53
                                          239.93
               over (min)
                              12.00
                                           16.00
                           11.60 (ii) 15.78 (ii)
12.00 16.00
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
    Unit Hyd. peak (cms)=
                               .10
                                            .07
                                                        *TOTALS*
    PEAK FLOW
                    (cms) =
                               9.52
                                            4.63
                                                         13.580 (iii)
                    (hrs)=
    TIME TO PEAK
                               1.18
                                            1.30
                                                          1.217
    RUNOFF VOLUME
                     (mm) =
                               85.06
                                           50.88
                                                         67.975
    TOTAL RAINFALL
                    (mm) =
                               87.07
                                          87.07
                                                         87.067
    RUNOFF COEFFICIENT =
                               .98
                                            .58
                                                           .781
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
100:0008-----
*# External catchment containing a portion of Cedar Creek Road, a portion of
       industrial area, and a grassed area near Hwy 401 off-ramp,
*#
         draining south into site and flowing south / east.
*#
*#------
| DESIGN STANDHYD |
               Area (ha)= 14.55
              Total Imp(%)=
| 06:101 DT= 1.00 |
                          60.00 Dir. Conn.(%)=
______
                   IMPERVIOUS
                            PERVIOUS (i)
   Surface Area
              (ha)=
                      8.73
                              5.82
   Dep. Storage
              (mm) =
                              1.50
                      .80
                    2.30
   Average Slope
             (%)=
                              2.30
                    311.45
                             40.00
   Length
               (m) =
   Mannings n
                      .013
                              .250
```

```
Max.eff.Inten.(mm/hr) = 239.35 68.89
                          3.00
          over (min)
                                       11.00
Storage Coeff. (min)= 2.77 (ii) 10.63 (ii)
Unit Hyd. Tpeak (min)= 3.00 11.00
Unit Hyd. peak (cms)= .39 .11
Unit Hyd. peak (cms)=
                           .39
                                        .11
                                                     *TOTALS*
                                         .73
PEAK FLOW
               (cms)=
                           4.01
                                                       4.274 (iii)
               (hrs)=
TIME TO PEAK
                           1.02
                                        1.23
                                                      1.017
                      86.27
87.07
                                      26.24
               (mm) =
RUNOFF VOLUME
                                                     55.053
TOTAL RAINFALL
               ( mm ) =
                                       87.07
                                                     87.067
RUNOFF COEFFICIENT =
                           .99
                                        .30
                                                       .632
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0009------ -*# *# External catchment west of site, containing exisiting industrial *# property draining into private SWM feature and then onto site flowing east *#-----| _____ DESIGN STANDHYD | Area (ha)= 12.64 | 07:102 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00 IMPERVIOUS PERVIOUS (i) Surface Area (ha)= 10.11 (mm) = .80 (%) = 3.10 (m) = .290.29 = .20.11 2.53 Dep. Storage 1.50 Average Slope 3.10 Length 40.00 Mannings n .250 239.35 2.00 Max.eff.Inten.(mm/hr)= 228.73 over (min) 7.00 2.43 (ii) 6.88 (ii) 2.00 7.00 Storage Coeff. (min)= Unit Hyd. Tpeak (min)= .49 Unit Hyd. peak (cms)= .16 *TOTALS* PEAK FLOW (cms)= 3.81 1.15 4.403 (iii) 1.00 TIME TO PEAK (hrs)= 1.13 1.017 86.27 RUNOFF VOLUME (mm) =39.75 63.011 TOTAL RAINFALL (mm) =87.07 87.07 87.067 RUNOFF COEFFICIENT = .99 .46 .724

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
______
100:0010-----
*#-----|
*#
               Infiltration in External SWM Feature
*#-----|
                 Requested routing time step = 1.0 min.
ROUTE RESERVOIR
 IN>07:(102 )
OUT<08:(xSWinf) | ======= OUTLFOW STORAGE TABLE =======
                 OUTFLOW STORAGE | OUTFLOW STORAGE

    (cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    .018
    .3759E+00

    .018
    .4380E-01
    .000
    .0000E+00

                  (cms) (ha.m.)
                   .000 .0000E+00
   OVERFLOW<09: (OVF-xI)
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                           2
             CUMULATIVE TIME OF OVERFLOWS (hours)= 2.02
PERCENTAGE OF TIME OVERFLOWING (%)= 1.48
             PEAK FLOW REDUCTION [Qout/Qin](%)=
             TIME SHIFT OF PEAK FLOW (min)= -14.00
             MAXIMUM STORAGE USED
                             (ha.m.)=.3759E+00
*#
*#
               Total existing area draining to the east
*#-----|
| ADD HYD (ToEast ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
```

ID1	02:100	(ha) 55.94	(cms) 13.580	(hrs) 1.22	(mm) 67.98	(cms) .000
+ID2	03:IntEst	7.79	.836	1.42	38.58	.000
+ID3	06:101	14.55	4.274	1.02	55.05	.000
+ID4	09:0VF-xI	6.40	3.189	1.13	63.01	.000
===:		======		=====		======
SUM	05:ToEast	84.68	19.260	1.18	62.68	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0012					
*#					
*# [\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	a+ a£	+ba a + + a		· mantian of ove	:atima
<pre>*# External catchment *# industrial propert</pre>		-	•	•	•
*#	Ly, uraini	ing east i	into the site	and riowing soc	acii.
*# -					
					!
DESIGN STANDHYD	Area	(ha)=	4.52		
01:103 DT= 1.00	Total	L Imp(%)=	80.00 Dir	c. Conn.(%)= !	50.00
	<i>(</i> 1. \)		JS PERVIOUS	5 (i)	
Surface Area					
Dep. Storage					
Average Slope	(%)=	5.30	5.30		
Length			40.00		
Mannings n	=	.013	.250		
Max.eff.Inten.(r	nm /hn_	220 25	247 00		
			5.00		
Storage Coeff.				/ii\	
Unit Hyd. Tpeak		2.00		(11)	
Unit Hyd. peak	` '	.66			
onic nyu. peak	(CIIIS)-	.00	. 22	*TOTALS	*
PEAK FLOW	(cms)=	1.46	.46		
TIME TO PEAK	` '				(111)
RUNOFF VOLUME	(mm)=	86.27	39.75	63.011	
TOTAL RAINFALL			87.07		
RUNOFF COEFFICIE			.46		

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-	 -					
# # #	Total Fl	ows to the				
ADD HYD (TSouth) ID: NHYD	AREA		TPEAK	R.V.	DWF
	ID1 04:106		.823			
	+ID2 01:103	4.52	1.767	1.00	63.01	.000
	======== SUM 02:TSouth					
-						
- # #	Total Flows from si	te (eventua	ally to Ce	edar Cre	ek)	
- # # # #	Total Flows from si	te (eventua	ally to Co	edar Cre	ek) 	
- # # # #	Total Flows from si	te (eventua	ally to Ce	edar Cre	ek) R.V.	DWF
- # # # #	Total Flows from si	te (eventua AREA (ha)	ally to Co	edar Cre TPEAK (hrs)	ek) R.V. (mm)	DWF
- # # # #	Total Flows from si -) ID: NHYD	te (eventua AREA (ha) 84.68	ally to Ce QPEAK (cms)	edar Cre TPEAK (hrs) 1.18	ek) R.V. (mm) 62.68	DWF (cms) .000
- # # # #	Total Flows from si -) ID: NHYD ID1 05:ToEast	AREA (ha) 84.68	QPEAK (cms) 19.260 1.819	TPEAK (hrs) 1.18	ek) R.V. (mm) 62.68 45.04	DWF (cms) .000
- # # # ADD HYD (Totalf	Total Flows from si -) ID: NHYD ID1 05:ToEast +ID2 02:TSouth ====================================	AREA (ha) 84.68 15.52 100.20	QPEAK (cms) 19.260 1.819	TPEAK (hrs) 1.18	ek) R.V. (mm) 62.68 45.04	DWF (cms) .000
- ## ## #ADD HYD (TotalF	Total Flows from si -) ID: NHYD ID1 05:ToEast +ID2 02:TSouth	AREA (ha) 84.68 15.52 100.20	QPEAK (cms) 19.260 1.819 20.460	TPEAK (hrs) 1.18 1.00	ek) R.V. (mm) 62.68 45.04 ======	DWF (cms) .000 .000

```
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
** END OF RUN: 499
************************************
START
          Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
          Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
 TZERO = .00 hrs on
 METOUT= 2 (output = METRIC)
 NRUN = 500
 NSTORM=
    # 1=hurhaz48.stm
500:0002-----
*#********************************
*# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project # : [161414214]
      : 01-25-2024
```

```
*# Modeller : [Amy Kyle, Water Resources Specialist]
*# Company : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
```

*#

*# This hydrologic analysis prepared to provide pond sizing

*# for the 2509 Cedar Creek Road SWM Facility

*# The storm events modelled are:

25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF) *#

*# and the Regional Event

500:0002-----

| READ STORM | Filename: REGIONAL STORM | Ptotal= 285.00 mm | Comments: REGIONAL STORM

	-						
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	2.000	12.25	2.000	24.25	2.000	36.25	6.000
.50	2.000	12.50	2.000	24.50	2.000	36.50	6.000
.75	2.000	12.75	2.000	24.75	2.000	36.75	6.000
1.00	2.000	13.00	2.000	25.00	2.000	37.00	6.000
1.25	2.000	13.25	2.000	25.25	2.000	37.25	4.000
1.50	2.000	13.50	2.000	25.50	2.000	37.50	4.000
1.75	2.000	13.75	2.000	25.75	2.000	37.75	4.000
2.00	2.000	14.00	2.000	26.00	2.000	38.00	4.000
2.25	2.000	14.25	2.000	26.25	2.000	38.25	6.000
2.50	2.000	14.50	2.000	26.50	2.000	38.50	6.000
2.75	2.000	14.75	2.000	26.75	2.000	38.75	6.000
3.00	2.000	15.00	2.000	27.00	2.000	39.00	6.000
3.25	2.000	15.25	2.000	27.25	2.000	39.25	13.000
3.50	2.000	15.50	2.000	27.50	2.000	39.50	13.000
3.75	2.000	15.75	2.000	27.75	2.000	39.75	13.000
4.00	2.000	16.00	2.000	28.00	2.000	40.00	13.000
4.25	2.000	16.25	2.000	28.25	2.000	40.25	17.000
4.50	2.000	16.50	2.000	28.50	2.000	40.50	17.000
4.75	2.000	16.75	2.000	28.75	2.000	40.75	17.000
5.00	2.000	17.00	2.000	29.00	2.000	41.00	17.000
5.25	2.000	17.25	2.000	29.25	2.000	41.25	13.000
5.50	2.000	17.50	2.000	29.50	2.000	41.50	13.000
5.75	2.000	17.75	2.000	29.75	2.000	41.75	13.000
6.00	2.000	18.00	2.000	30.00	2.000	42.00	13.000
6.25	2.000	18.25	2.000	30.25	2.000	42.25	23.000
6.50	2.000	18.50	2.000	30.50	2.000	42.50	23.000
6.75	2.000	18.75	2.000	30.75	2.000	42.75	23.000
7.00	2.000	19.00	2.000	31.00	2.000	43.00	23.000
7.25	2.000	19.25	2.000	31.25	2.000	43.25	13.000
7.50	2.000	19.50	2.000	31.50	2.000	43.50	13.000

```
7.75
     2.000
            19.75
                 2.000 | 31.75 2.000 | 43.75 13.000
     2.000 | 20.00 | 2.000 | 32.00 | 2.000 | 44.00 | 13.000
8.00
            20.25
                  8.25
     2.000
     2.000
                 2.000 | 32.50 2.000 | 44.50 13.000
8.50
            20.50
                 2.000 | 32.75 2.000 | 44.75 13.000
8.75
     2.000
            20.75
                  2.000 | 33.00 2.000 | 45.00 13.000
9.00
     2.000 | 21.00
9.25
     2.000 | 21.25
                 2.000 | 33.25 2.000 | 45.25 53.000
                 2.000 | 33.50 2.000 | 45.50 53.000
9.50
     2.000
           21.50
9.75
     2.000 | 21.75
                 2.000 | 33.75 2.000 | 45.75 53.000
                 2.000 | 34.00 2.000 | 46.00 53.000
10.00
     2.000
           22.00
                               2.000 | 46.25 38.000
     2.000
           22.25
                  2.000 | 34.25
10.25
                 2.000 | 34.50 2.000 | 46.50 38.000
10.50
     2.000
           22.50
           22.75
                 2.000 | 34.75 2.000 | 46.75 38.000
10.75
     2.000
11.00 2.000 | 23.00 2.000 | 35.00 2.000 | 47.00 38.000
           23.25 2.000 | 35.25 3.000 | 47.25 13.000
     2.000
11.25
11.50 2.000 | 23.50 2.000 | 35.50 3.000 | 47.50 13.000
     11.75
     12.00
```

```
500:0003-----
*# Pre-Development Drainage Area (Internal Catchments)
*#------
*#
*#
          Existing internal area draining to the east
*#
*#------
-----
           Area (ha)= 7.06 Curve Number (CN)=71.00
DESIGN NASHYD
| 01:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .330
  Unit Hyd Qpeak (cms)= .817
       (cms) = .895 (i)
  PEAK FLOW
  TIME TO PEAK (hrs)= 46.083
  RUNOFF VOLUME
          (mm) = 207.548
  TOTAL RAINFALL (mm)= 285.000
  RUNOFF COEFFICIENT =
             .728
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

--500:0004-----

- -

```
*#
*#
   Small external area entering site from east and draining south / east
*#-----|
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)= .095 (i)
  TIME TO PEAK (hrs)=
               46.017
           (mm) = 204.845
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)= 285.000
  RUNOFF COEFFICIENT = .719
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0005-----
*#------
*#
*#
           Total existing area draining to the east
*#------
| ADD HYD (IntEst
          ) | ID: NHYD
                     AREA
                          QPEAK TPEAK R.V.
                                        DWF
                     (ha) (cms) (hrs) (mm)
7.06 .895 46.08 207.55
-----
                                       (cms)
           ID1 01:105
                                       .000
                   .73 .095 46.02 204.85 .000
          +ID2 02:104
           ______
           SUM 03:IntEst 7.79 .989 46.07 207.29
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
500:0006-----
*#
*#
          Existing internal area draining to the south
*#------|
```

```
DESIGN NASHYD
                Area (ha)= 11.00 Curve Number (CN)=70.00
04:106 DT= 1.00
                 Ia
                      (mm) = 1.500 # of Linear Res.(N) = 3.00
                U.H. Tp(hrs) = .540
-----
   Unit Hyd Qpeak (cms)= .778
   PEAK FLOW
              (cms) = 1.242 (i)
              (hrs)= 46.367
   TIME TO PEAK
              (mm) = 204.845
   RUNOFF VOLUME
             (mm) = 285.000
   TOTAL RAINFALL
   RUNOFF COEFFICIENT = .719
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0007-----
*# Total Pre-Development Drainage Area (Including Large External Catchments)
*#-----|
*# External industrial catchment and part of Hwy 401, draining south into the
*#
                site and flowing south / east.
*#-----|
| CALIB STANDHYD |
                Area (ha)= 55.94
| 02:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
                    IMPERVIOUS
                              PERVIOUS (i)
   Surface Area
              (ha)=
                     44.75
                               11.19
                     2.00
   Dep. Storage
              (mm)=
                                5.00
   Average Slope
               (%)=
                                2.00
                      1.60
                               30.00
   Length
               (m) =
                     1500.00
   Mannings n
                      .020
                               .250
   Max.eff.Inten.(mm/hr)=
                     53.00 126.91
           over (min)
                      19.00
                               24.00
                     24.00
18.81 (ii) 24.21 (ii)
19.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                      .06
                                .05
                                         *TOTALS*
   PEAK FLOW
                      3.91
                               3.57
             (cms)=
                                          7.465 (iii)
   TIME TO PEAK
              (hrs)=
                   46.07
282.91
285.00
                     46.07
                               46.17
                                         46.100
   RUNOFF VOLUME
              (mm) =
                              235.37
                                         259.226
   TOTAL RAINFALL
              (mm) =
                               285.00
                                        285.000
   RUNOFF COEFFICIENT =
                      .99
                               .83
                                         .910
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

500:0008-----*# External catchment containing a portion of Cedar Creek Road, a portion of industrial area, and a grassed area near Hwy 401 off-ramp, *# draining south into site and flowing south / east. *#------______ DESIGN STANDHYD Area (ha) = 14.5560.00 Dir. Conn.(%)= 48.00 IMPERVIOUS PERVIOUS (i) Surface Area (ha)= 8.73 5.82 Dep. Storage (mm) =1.50 .80 2.30 Average Slope (%)= 2.30 Length (m)=311.45 40.00 Mannings n .013 .250 Max.eff.Inten.(mm/hr)= 53.00 54.13 over (min) 5.00 14.00 Storage Coeff. (min)= 5.07 (ii) 13.72 (ii) Unit Hyd. Tpeak (min)= 5.00 14.00 Unit Hyd. peak (cms)= .22 .08 *TOTALS* .85 PEAK FLOW (cms)= 1.03 1.875 (iii) 46.00 284.19 TIME TO PEAK (hrs)= 46.03 46.000 RUNOFF VOLUME (mm) =168.10 223.839 285.00 285.000 TOTAL RAINFALL (mm) =RUNOFF COEFFICIENT = 1.00 .59 .785 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT. (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

--500:0009-----

```
*#
*# External catchment west of site, containing exisiting industrial
*# property draining into private SWM feature and then onto site flowing east
*#-----|
DESIGN STANDHYD
                          (ha) = 12.64
                  Area
| 07:102 DT= 1.00 |
                  Total Imp(%)= 80.00 Dir. Conn.(%)=
                                                    50.00
                        IMPERVIOUS
                                   PERVIOUS (i)
   Surface Area
                          10.11
                                     2.53
                (ha)=
                (mm) =
                          .80
   Dep. Storage
                                    1.50
                  (\%) = 3.10
(m) = 290.29
   Average Slope
                (%)=
                                     3.10
   Length
                                    40.00
                         .013
   Mannings n
                                     .250
                                  119.98
   Max.eff.Inten.(mm/hr)=
                        53.00
            over (min)
                         4.00
                                    10.00
                      4.45 (ii) 10.20 (ii)
4.00 10.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                          .26
                                    .11
                                               *TOTALS*
                                    .83
   PEAK FLOW
                (cms)=
                          .93
                                                1.765 (iii)
                      46.00
284.17
   TIME TO PEAK
                (hrs)=
                                   46.00
                                                46.000
   RUNOFF VOLUME
                                   209.52
                                               246.871
                (mm) =
   TOTAL RAINFALL
                 (mm) =
                         285.00
                                    285.00
                                               285.000
   RUNOFF COEFFICIENT =
                         1.00
                                     .74
                                                 .866
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
                  Infiltration in External SWM Feature
*#-----|
ROUTE RESERVOIR
                    Requested routing time step = 1.0 min.
 IN>07:(102 )
```

====== OUTLFOW STORAGE TABLE =======

(cms)

| .018 .3759E+00

STORAGE

(ha.m.)

OUTFLOW STORAGE | OUTFLOW (cms) (ha.m.) | (cms)

.000 .0000E+00

OUT<08:(xSWinf)

```
.018 .4380E-01 | .000 .0000E+00
                     AREA
(ha)
12.64
   ROUTING RESULTS
                                    TPEAK
                             QPEAK
                                             R.V.
   -----
                             (cms)
                                    (hrs)
                                              (mm)
                                    46.000 246.871
4.833 246.884
   INFLOW >07: (102 )
                             1.765
   OUTFLOW<08: (xSWinf)
                      2.73
                             .018
  OVERFLOW<09: (OVF-xI)
                      9.91
                             1.746
                                    46.000
                                           246.871
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                              2
             CUMULATIVE TIME OF OVERFLOWS (hours)=
                                            15.28
             PERCENTAGE OF TIME OVERFLOWING (%)=
                                           8.41
             PEAK FLOW REDUCTION [Qout/Qin](%)= 1.020
             TIME SHIFT OF PEAK FLOW (min)= -2470.00
             MAXIMUM STORAGE USED
                                  (ha.m.)=.3759E+00
*#
*#
                Total existing area draining to the east
*#------
| ADD HYD (ToEast ) | ID: NHYD
                              AREA
                                     QPEAK
                                          TPEAK R.V.
                                                      DWF
                              (ha) (cms) (hrs) (mm)
55.94 7.465 46.10 259.23
                                          (hrs) (mm)
                                                      (cms)
               ID1 02:100
                                    .989 46.07 207.29
              +ID2 03:IntEst
                             7.79
                                                      .000
              +ID3 06:101
                         14.55 1.875 46.00 223.84
                                                      .000
              +ID4 09:0VF-xI 9.91 1.746 46.00 246.87
                                                      .000
               ______
               SUM 05:ToEast 88.19
                                    11.995 46.02 247.41 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
500:0012-----
*#-----|
*# External catchment west of the site, containing a portion of existing
```

*# industrial property, draining east into the site and flowing south.

```
*#
*#------|
DESIGN STANDHYD
                   Area (ha) = 4.52
| 01:103 DT= 1.00 |
                  Total Imp(%)= 80.00 Dir. Conn.(%)=
                                                     50.00
------
                       IMPERVIOUS
                                   PERVIOUS (i)
   Surface Area
                (ha)=
                        3.62
                                      .90
                      .80
5.30
173.59
   Dep. Storage
                 (mm) =
                                     1.50
                (%)=
   Average Slope
                                     5.30
   Length
                  (m) =
                                    40.00
   Mannings n
                          .013
                                     .250
                      53.00
   Max.eff.Inten.(mm/hr)=
                                   120.05
                         3.00
                                    8.00
            over (min)
                         2.78 (ii) 7.68 (ii)
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                          3.00
                                    8.00
   Unit Hyd. peak (cms)=
                          .39
                                     .15
                                               *TOTALS*
                                   .30
   PEAK FLOW
               (cms)=
                         .33
                                                  .633 (iii)
                      45.73
284.18
285.00
               (hrs)=
   TIME TO PEAK
                                   46.00
                                                46.000
   RUNOFF VOLUME
                (mm) =
                                    209.52
                                               246.871
   TOTAL RAINFALL (mm)=
                                    285.00
                                               285.000
   RUNOFF COEFFICIENT =
                                    .74
                                                .866
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
500:0013-----
*#-----|
*#
              Total Flows to the south
*#
*#------
| ADD HYD (TSouth ) | ID: NHYD
                    AREA
                         QPEAK
                            TPEAK
                                 R.V.
                    (ha) (cms) (hrs) (mm)
11.00 1.242 46.37 204.85
-----
                                    (cms)
          ID1 04:106
                                    .000
         +ID2 01:103
                    4.52 .633 46.00 246.87
                                     .000
          ______
          SUM 02:TSouth 15.52 1.755 46.02 217.08 .000
```

NOTE:	PEAK FLO	WS DO N	OT INCLUDE	BASEF						
 *# *# *#		Total	Flows from	site	(eventu	ally to Co	edar Cro	 eek)		
ADD HYD	(TotalF	ID1 (ID: NHYD 05:ToEast 02:TSouth		(ha) 88.19 15.52	QPEAK (cms) 11.995 1.755	(hrs) 46.02 46.02	(mm) 247.41 217.08	(cms) .000	
		SUM (03:TotalF OT INCLUDE	BASEF	103.71 LOWS IF	13.750 ANY.	46.02	242.87	.000	
 500:0002-										
 500:0002										

 FINISH	

WARNINGS / ERRORS / NOTES	
Simulation ended on 2024-01-25	at 15:08:57

```
______
                               000
                                      999
 SSSSS
              М
                Н
                  Н
                    Υ
                       Y M
                            М
                                           999
         W
                                                =======
      WWW
           MM MM
                Н
                  Н
                     YY
                         MM MM
                                 0
                                      9
                                        9
                                          9
                                             9
                              0
 SSSSS
      WWW
           M M M
                HHHHH
                      Υ
                         M M M
                              0
                                 0
                                   ##
                                                Ver 4.05
                Н
                         Μ
                            Μ
                                 0
                                      9999
                                           9999
                                                Sept 2011
       W W
           Μ
              Μ
                  Н
                      Υ
 SSSSS
                                        9
       W W
              Μ
                Н
                               000
                                             9
                                                =======
                                        9
                                             9
                                                # 4730904
     StormWater Management HYdrologic Model
                                      999
                                           999
***********************************
******
        A single event and continuous hydrologic simulation model
******
          based on the principles of HYMO and its successors
                  OTTHYMO-83 and OTTHYMO-89.
**********************************
****** Distributed by:
                  J.F. Sabourin and Associates Inc.
******
                  Ottawa, Ontario: (613) 836-3884
*****
                  Gatineau, Quebec: (819) 243-6858
******
                   E-Mail: swmhymo@ifsa.Com
***********************************
++++++ Licensed user: Stantec Consulting Ltd. (Kitchener)
++++++++
                 Kitchener
                                SERIAL#:4730904
                                                ++++++++
***********************************
              +++++ PROGRAM ARRAY DIMENSIONS ++++++
*****
              Maximum value for ID numbers :
              Max. number of rainfall points: 105408
******
              Max. number of flow points
                                  : 105408
*************************************
********
                 DETAILED OUTPUT
***********************************
                                  RUN COUNTER: 000240
       DATE: 2024-01-25
                     TIME: 15:14:59
************************************
* Input filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPost.dat
* Output filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPost.out
                                                     *
* Summary filename: C:\SWMHYMO\CEDARC~1\202401~4\CCrPost.sum
* User comments:
* 1:
 2:
```

_ -

```
001:0001-----
*#*********************************
   Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
   Date
         : 01/25/2024
*# Modeller
            : [Amy Kyle, Water Resources Specialist]
            : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
   25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
   and the Regional Event
*#*********************************
START
                 Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
                 Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
   TZERO =
           .00 hrs on
   METOUT=
           2 (output = METRIC)
   NRUN = 001
   NSTORM=
        # 1=Kit25mm.4hr
001:0002-----
______
READ STORM
                   Filename: 25 mm, 4hr Chicago Storm - Kitchener IDF
| Ptotal= 25.00 mm|
                   Comments: 25 mm, 4hr Chicago Storm - Kitchener IDF
           TIME
                 RAIN |
                        TIME
                              RAIN |
                                      TIME
                                             RAIN |
                                                    TIME
                                                          RAIN
            hrs
                mm/hr |
                         hrs
                              mm/hr
                                      hrs
                                            mm/hr
                                                    hrs
                                                         mm/hr
                                      2.08
                                            5.764
            .08
                1.465
                        1.08
                              4.024
                                                    3.08
                                                         2.074
            .17
                1.540
                        1.17
                              4.814
                                      2.17
                                                    3.17
                                                         1.977
                                           4.969
            .25
                        1.25
                              6.025
                                      2.25
                                            4.374
                                                   3.25
                1.625
                                                         1.889
            .33
                1.720
                        1.33
                              8.114
                                      2.33
                                           3.913
                                                   3.33
                                                         1.810
            .42
                1.829
                        1.42 12.526
                                      2.42 3.545
                                                    3.42
                                                         1.737
            .50
                1.955
                        1.50 27.198
                                      2.50 3.245
                                                    3.50
                                                         1.671
            .58
                2.101
                        1.58 74.855
                                      2.58 2.994
                                                   3.58
                                                         1.610
                                      2.67
            .67
                2.274
                        1.67
                             31.410 |
                                            2.782
                                                   3.67
                                                         1.553
            .75
                2.482
                        1.75
                             16.819
                                      2.75 2.601
                                                   3.75
                                                         1.501
                                      2.83
            .83
                2.736
                         1.83 11.357
                                            2.443
                                                   3.83
                                                         1.453
            .92
                3.055
                        1.92
                             8.563
                                      2.92
                                            2.305
                                                  3.92
                                                         1.408
                3.468
                        2.00
                             6.882 | 3.00
                                            2.183 | 4.00
           1.00
                                                         1.366
```

- -

```
001:0003-----
*#-----|
*# Proposed Drainage Conditions (Internal Areas)
*#-----|
*#
   Small portion of West Road Ditch draining offsite to the east through
*#
                 By-Pass Storm Sewer(BPSS)
*#------|
----- U.H. Tp(hrs)= .260
  Unit Hyd Qpeak (cms)= .021
  PEAK FLOW (cms)= .001 (i)
TIME TO PEAK (hrs)= 1.917
RUNOFF VOLUME (mm)= 1.986
  TOTAL RAINFALL (mm)= 25.000
  RUNOFF COEFFICIENT = .079
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0004-----
*#------|
*# Proposed developed catchment draining offsite to the east through BPSS
*#-----|
| DESIGN STANDHYD | Area (ha)= .64
| 02:201 \quad DT= 1.00 | Total Imp(%)= 90.00 \quad Dir. Conn.(%)= 50.00
  Surface Area (ha)= .58

Dep. Storage (mm)= .80

(%)= 2.00
                 IMPERVIOUS PERVIOUS (i)
                  .58
                           .06
                           1.50
  Average Slope (%)= 2.00

Length (m)= 65.32

Mannings n = .013
                          2.00
                          40.00
                          .250
  Max.eff.Inten.(mm/hr)= 74.85 90.91
over (min) 2.00 9.00
Storage Coeff. (min)= 1.80 (ii) 9.14 (ii)
```

```
Unit Hyd. Tpeak (min)=
                    2.00
                                   9.00
Unit Hyd. peak (cms)=
                         .60
                                     .12
                                               *TOTALS*
                                    .01
PEAK FLOW
            (cms)=
                         .06
                                                 .067 (iii)
TIME TO PEAK
                        1.58
             (hrs)=
                                   1.72
                                                 1.583
                      24.20
RUNOFF VOLUME
             (mm) =
                                    8.08
                                                16.141
TOTAL RAINFALL
               (mm) =
                       25.00
                                   25.00
                                               25.000
RUNOFF COEFFICIENT =
                         .97
                                     .32
                                                 . 646
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
001:0005-----
*#------
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#-----|
             Area (ha)= .55 Curve Number (CN)=50.00
DESIGN NASHYD
| 03:203 DT= 1.00 |
                 (mm) = 1.500 \# of Linear Res.(N) = 3.00
              Ia
 ----- U.H. Tp(hrs)=
                      .080
  Unit Hyd Qpeak (cms)= .263
  PEAK FLOW (cms)=
                 .005 (i)
  TIME TO PEAK (hrs)=
                1.667
                1.990
           (mm) =
  RUNOFF VOLUME
  TOTAL RAINFALL
            (mm) =
                 25.000
  RUNOFF COEFFICIENT =
                 .080
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#------
*#
      Total internal area draining onto agricultural area to the east
*#-----|
ADD HYD (Intuce ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
```

ID1	01:200	(ha) .14	(cms) .001	(hrs) 1.92	` '	(cms) .000
+ID2	02:201	.64	.067	1.58	16.14	.000
+ID3	03:203	.55	.005	1.67	1.99	.000
===:			:======		======	======
SUM	05:IntUcE	1.33	.071	1.58	8.80	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

--001:0007------* *# *# Proposed industrial lots draining to Rear Lot Ditch *# *#-----|

Surface Area Dep. Storage Average Slope Length	(ha)= (mm)= (%)= (m)=	IMPERVIOUS 7.94 .80 2.00 242.49	PERVIOUS (i) .88 1.50 2.00 40.00	
Mannings n	=	.013	.250	
Max.eff.Inten.(mm/hr)=	74.85	10.94	
over	(min)	4.00	21.00	
Storage Coeff.	(min)=	3.96 (ii)	21.07 (ii)	
Unit Hyd. Tpeak	(min)=	4.00	21.00	
Unit Hyd. peak	(cms)=	.28	.05	
•				*TOTALS*
PEAK FLOW	(cms)=	1.08	.02	1.085 (iii)
TIME TO PEAK	(hrs)=	1.62	1.97	1.617
RUNOFF VOLUME	(mm)=	24.20	3.89	20.138
TOTAL RAINFALL	(mm) =	25.00	25.00	25.000
RUNOFF COEFFICI	ENT =	.97	.16	.806

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
001:0008-----
*#------|
*#
   External agricultural area draining onsite and entering Rear Lot Ditch
*#
*#-----|
             Area (ha)= .73 Curve Number (CN)=70.00
DESIGN NASHYD
| 07:104 DT= 1.00 |
            Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)=
          (cms)=
  PEAK FLOW
                .010 (i)
  TIME TO PEAK (hrs)=
                1.817
           (mm) =
               4.172
  RUNOFF VOLUME
  TOTAL RAINFALL
           (mm) =
                25.000
  RUNOFF COEFFICIENT =
                 .167
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0009-----
*#------
*#
*#
    Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#-----|
ADD HYD (RLswl
           ) | ID: NHYD
                       AREA
                            QPEAK TPEAK R.V.
                                         DWF
-----
                       (ha)
                           (cms) (hrs)
                                    (mm)
                                        (cms)
                       8.82 1.085 1.62 20.14
           ID1 06:202
                                        .000
           +ID2 07:104
                   .73 .010 1.82 4.17 .000
           -----
           SUM 08:RLswl
                      9.55 1.089 1.62 18.92 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0010-----
```

```
*#
*#
    Proposed industrial lots draining to East Road Ditch within catchment,
*#
                        and new internal roadway
*#
*#------|
DESIGN STANDHYD
                     Area
                             (ha) = 4.92
| 01:204 DT= 1.00 |
                    Total Imp(%)= 90.00 Dir. Conn.(%)=
                                                          80.00
                          IMPERVIOUS
                                      PERVIOUS (i)
    Surface Area
                   (ha)=
                              4.43
                                          .49
    Dep. Storage
                  (mm) =
                              .80
                                         1.50
    Average Slope
                  (%)=
                              2.00
                                         2.00
    Length
                    (m)=
                            181.11
                                        40.00
    Mannings n
                            .013
                                         .250
    Max.eff.Inten.(mm/hr)=
                           74.85
                                        11.23
              over (min)
                                        20.00
                             3.00
                           3.33 (ii) 20.25 (ii)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                            3.00
                                        20.00
    Unit Hyd. peak (cms)=
                             .35
                                         .06
                                                    *TOTALS*
    PEAK FLOW
                  (cms) =
                             .65
                                         .01
                                                       .654 (iii)
    TIME TO PEAK
                  (hrs)=
                            1.60
                                        1.95
                                                     1.600
    RUNOFF VOLUME
                   (mm) =
                             24.20
                                        3.89
                                                     20.138
    TOTAL RAINFALL
                   (mm) =
                             25.00
                                        25.00
                                                     25.000
    RUNOFF COEFFICIENT =
                              .97
                                         .16
                                                       .806
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
         CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
         THAN THE STORAGE COEFFICIENT.
```

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

	oftop in volume	nfiltration from an ass	lumped togethoumed 0.15ha ro	er and si	ized for rea per	25mm lot (7]	 lots)
ADD HYD (Roof		ID: NHYD 01:204	AREA (ha) 4.92	QPEAK (cms) .654		R.V. (mm) 20.14	DWF (cms) .000
	+ID2	06:202	8.82	1.085	1.62	20.14	.000

SUM 02:Roof 13.74 1.729 1.60 20.14 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
001:0012-----
ROUTE RESERVOIR
               Requested routing time step = 1.0 min.
| IN>02:(Roof )
           | ====== OUTLFOW STORAGE TABLE =======
OUT<04:(R-inf)
               OUTFLOW STORAGE | OUTFLOW STORAGE
                (cms) (ha.m.)
                            (cms)
                                   (ha.m.)
                 .000 .0000E+00
                               .000 .2625E-01
  TOTAL NUMBER OF SIMULATED OVERFLOWS =
           CUMULATIVE TIME OF OVERFLOWS (hours)= 4.85
           PERCENTAGE OF TIME OVERFLOWING (%)=
                                     . 28
           PEAK FLOW REDUCTION [Qout/Qin](%)=
                                     .001
           TIME SHIFT OF PEAK FLOW (min)= -18.00
           MAXIMUM STORAGE USED (ha.m.)=.2625E-01
   *** WARNING: Outflow volume is less than inflow volume.
001:0013-----
*#-----|
*#
         Proposed SWM facility catchment (infiltration basin)
*#-----|
DESIGN NASHYD
              Area (ha)= 1.63 Curve Number (CN)=57.00
              Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
09:205 DT= 1.00
```

Unit Hyd Qpeak (cms)= .178

----- U.H. Tp(hrs)= .350

```
(mm) =
   TOTAL RAINFALL
                     25.000
   RUNOFF COEFFICIENT =
                    .103
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0014-----
*#-----|
*#
*#
                  All flows entering SWM facility
*#
*#------|
| ADD HYD (ToSWM ) | ID: NHYD
                              AREA QPEAK
                                          TPEAK R.V.
                                                      DWF
                              (ha) (cms) (hrs) (mm) (cms)
12.44 1.719 1.62 20.14 .000
-----
              ID1 10:inf0
              +ID2 07:104
                         .73 .010 1.82 4.17 .000
                         1.63 .009 2.03 2.57 .000
              +ID3 09:205
               ______
                              14.80 1.725 1.62 17.41
               SUM 06:ToSWM
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
*#
*#
                Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR
                  Requested routing time step = 1.0 min.
IN>06:(ToSWM )
| OUT<07:(SWMinf) |
                 ====== OUTLFOW STORAGE TABLE ======
______
                  OUTFLOW STORAGE | OUTFLOW STORAGE

    (cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    .044
    .7033E+00

    .044
    .6530E-01
    .000
    .0000E+00
```

PEAK FLOW (cms) = .009 (i)

(mm) =

TIME TO PEAK (hrs)=

RUNOFF VOLUME

2.033 2.567

```
R.V.
                                                   (mm)
                                                  17.414
                                                  17.414
                                                   .000
               TOTAL NUMBER OF SIMULATED OVERFLOWS =
               CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                    .00
               PERCENTAGE OF TIME OVERFLOWING (%)=
                                                  .00
               PEAK FLOW REDUCTION [Qout/Qin](%)= 2.551
               TIME SHIFT OF PEAK FLOW (min)= .00
               MAXIMUM STORAGE USED (ha.m.)=.2158E+00
001:0016-----
*#------
*#
*#
                 Active Storage Portion of SWM facility
*#------|
______
ROUTE RESERVOIR
                    Requested routing time step = 1.0 min.
 IN>08:(OVF-I )
OUT<01:(SWMout) ======= OUTLFOW STORAGE TABLE =======
                    OUTFLOW STORAGE | OUTFLOW STORAGE (cms) (ha.m.) | (cms) (ha.m.)

    (cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    1.479
    .2400E+00

    .202
    .7850E-01
    4.101
    .4070E+00

    .689
    .1586E+00
    .000
    .0000E+00

     *** WARNING: Inflow hydrograph is dry.
                        AREA QPEAK
(ha) (cms)
.00 .000
.00 .000
                                        TPEAK
    ROUTING RESULTS
                                                   R.V.
                                        (hrs)
                                                   (mm)
                                         .000
    INFLOW >08: (OVF-I )
                                                   .000
    OUTFLOW<01: (SWMout)
                                          .000
                                                   .000
   OVERFLOW<02: (OVF )
                        13.74
                                  .000
                                          .000
                                                   .000
               TOTAL NUMBER OF SIMULATED OVERFLOWS =
               CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                    .00
               PERCENTAGE OF TIME OVERFLOWING (%)=
                                                   .00
*** WARNING: Inflow and ouflow hydrographs are dry.
```

- -

```
001:0017-----
*#------
*#
   West Road Ditch, conveying external drainage from the west around the
*#
          proposed SWM facility to Outlet Channel
*#
*#------|
----- U.H. Tp(hrs)= .810
  Unit Hyd Qpeak (cms)= .058
          (cms) = .003 (i)
  PEAK FLOW
          (hrs)=
              2.650
1.989
  TIME TO PEAK
  RUNOFF VOLUME
          (mm) =
  TOTAL RAINFALL (mm)=
               25.000
  RUNOFF COEFFICIENT =
               .080
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0018-----
*#-----|
*#
     Grassed area south of SWM facility draining offsite to the south
*#------|
| DESIGN NASHYD | Area (ha)= .14 Curve Number (CN)=50.00
.
----- U.H. Tp(hrs)= .070
  Unit Hyd Qpeak (cms)= .076
  PEAK FLOW (cms)=
               .001 (i)
  TIME TO PEAK (hrs)=
                1.650
              1.989
  RUNOFF VOLUME
          (mm)=
          (mm) =
  TOTAL RAINFALL
               25.000
  RUNOFF COEFFICIENT =
               .080
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0019-----
```

```
*#------|
*#
*#
          Total Flows to the east from internal catchments
*#------
______
           ) | ID: NHYD AREA
| ADD HYD (IntE
                            QPEAK TPEAK R.V.
                                           DWF
-----
                            (cms) (hrs)
                        (ha)
                                      (mm)
                                          (cms)
                       1.33
                            .071 1.58 8.80
           ID1 05:IntUcE
                                          .000
                        .00 .000 .00 .00
           +ID2 01:SWMout
                                          .000
**DRY**
                     1.22 .003 2.65 1.99
           +ID3 02:206
                                           .000
            ______
            SUM 07:IntE 2.55 .071 1.58 5.54
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0020-----
*#-----|
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
*#------|
*# External industrial catchment and part of Hwy 401, draining south across
            Cedar Creek Road and entering BPSS
*#
*#------
CALIB STANDHYD | Area (ha)= 55.94
| 03:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00
______
                IMPERVIOUS
                         PERVIOUS (i)
  Surface Area
           (ha)=
                 44.75
                         11.19
                2.00
1.60
  Dep. Storage
            (mm) =
                          5.00
                          2.00
  Average Slope
           (%)=
             (m) = 1500.00
  Length
                         30.00
                  .020
  Mannings n
                          .250
                       17.90
  Max.eff.Inten.(mm/hr)= 35.29 17.90
over (min) 22.00 34.00
Storage Coeff. (min)= 22.13 (ii) 33.94 (ii)
Unit Hyd. Tpeak (min)= 22.00 34.00
```

Unit Hyd. peak	(cms)=	.05	.03	
•				*TOTALS*
PEAK FLOW	(cms)=	1.75	.32	1.952 (iii)
TIME TO PEAK	(hrs)=	1.92	2.20	1.933
RUNOFF VOLUME	(mm) =	23.00	6.60	14.800
TOTAL RAINFALL	(mm) =	25.00	25.00	25.000
RUNOFF COEFFICI	ENT =	.92	.26	.592

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*#-----| *# *# External catchment containing a portion of Cedar Creek Road, a portion *# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS *#------DESIGN STANDHYD (ha) = 14.55Area | 07:101 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 48.00 IMPERVIOUS PERVIOUS (i) 5.82 Surface Area 8.73 (ha)= 1.50 Dep. Storage (mm) =.80 2.30 Average Slope (%)= 2.30 Length (m) =311.45 40.00 Mannings n .013 .250 Max.eff.Inten.(mm/hr)= 74.85 3.89 over (min) 4.00 29.00 Storage Coeff. (min)= 4.42 (ii) 29.21 (ii) Unit Hyd. Tpeak (min)= 4.00 29.00 Unit Hyd. peak (cms)= .26 .04 *TOTALS* PEAK FLOW (cms) =1.04 1.041 (iii) . 04 1.62 TIME TO PEAK (hrs)= 2.12 1.617 RUNOFF VOLUME (mm) =24.20 2.59 12.965 TOTAL RAINFALL (mm) =25.00 25.00 25.000 RUNOFF COEFFICIENT = .97 .10 .519

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT. (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0022 *# *#							
*# Total area (*# *#	_			_			
ADD HYD (UCtoE	• •	HYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)		DWF (cms)
	ID1 05:In	tUcE	1.33	.071	1.58	8.80	.000
	+ID2 03:10	0	55.94	1.952	1.93	14.80	.000
	+ID3 07:10	1	14.55	1.041	1.62	12.96	.000
	====== SUM 09:UC	======= toE		2.222			
	catchment orivate SWM faci	west of sifeature ar	ite containd then in	ning induto West I	ustrial Road Dit	property	 /, ting
	catchment orivate SWM faci	west of sifeature ar	ite containd then incentering O	ning induto West I	ustrial Road Dit	property	 /, ting

```
over (min)
                             4.00
                                         16.00
                             3.87 (ii)
Storage Coeff. (min)=
                                         15.77 (ii)
Unit Hyd. Tpeak (min)=
                             4.00
                                         16.00
Unit Hyd. peak (cms)=
                              .29
                                           .07
                                                       *TOTALS*
PEAK FLOW
                (cms) =
                              .97
                                           .08
                                                         1.002 (iii)
TIME TO PEAK
                (hrs)=
                             1.62
                                          1.87
                                                         1.617
RUNOFF VOLUME
                 (mm) =
                            24.20
                                          4.72
                                                        14.463
                 (mm) =
                                                        25.000
TOTAL RAINFALL
                            25.00
                                         25.00
RUNOFF COEFFICIENT =
                              .97
                                           .19
                                                          .579
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

01:0024						
‡	-					
!						
:	Infil [.]	tration in	External	SWM Featur	'e	
#	1					
‡	-					
ROUTE RESERVOIR	l Reg	uested roud	ting time	sten = 1	0 min	
IN>04:(102)		acseca roa	cing cinc	зеер – 1.	0 111111	
OUT<05:(xSWinf)	===:	===== OU ⁻	TLFOW STOR	RAGE TABLE	=======	
		cms) (ha				
		.000 .000				
		.018 .4380	0E-01	.000	.0000E+00	
ROUTING RESUL	TC	ADEA	ODEAK	TDEAK	P \/	
INFLOW >04: (102)	12.64	1.002	1.617	14.463	
OUTFLOW<05: (
OVERFLOW<06: (
		BER OF SIMU				
		E TIME OF (,		
	PERCENTAG	E OF TIME (JAEKLTOMIL	=(%) bi	.00	
	PEAK FL	OW REDUC	ΓΙΟΝ [Qout	:/Qin](%)=	1.797	
	TIME SHIF	T OF PEAK I	ELOW	(min)=	-2.00	

(ha.m.)=.1636E+00

MAXIMUM STORAGE USED

```
001:0025-----
*#-----|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
                SWM facility and entering Outlet Channel
*#
*#-----|
| DESIGN STANDHYD |
                 Area (ha) = 4.52
| 07:103 DT= 1.00 |
                Total Imp(%)= 80.00 Dir. Conn.(%)=
                    IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)=
Dep. Storage (mm)=
Average Slope (%)=
                      3.62
                                 .90
                       .80
                                1.50
                   .80
5.30
173.59
                                5.30
   Length
               (m)=
                               40.00
                      .013
   Mannings n
                                .250
   Max.eff.Inten.(mm/hr)=
                      74.85
                               22.59
           over (min)
                       2.00
                                12.00
   Storage Coeff. (min)=
                       2.42 (ii) 11.97 (ii)
   Unit Hyd. Tpeak (min)=
                       2.00
                               12.00
   Unit Hyd. peak (cms)=
                       .49
                                 .09
                                         *TOTALS*
                      1.58
                       .42
   PEAK FLOW
              (cms)=
                                .04
                                           .430 (iii)
              (hrs)=
                                1.78
   TIME TO PEAK
                                           1.583
   RUNOFF VOLUME
               (mm) =
                       24.20
                                4.73
                                          14.463
   TOTAL RAINFALL (mm)=
                       25.00
                                25.00
                                          25.000
   RUNOFF COEFFICIENT =
                       .97
                                 .19
                                           .579
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
       CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
       THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
______
001:0026----
*#-----|
*#
*#
             Total Flows through West Road Ditch
```

*#-----|

```
| ADD HYD (WRswl ) | ID: NHYD
                     AREA
                              OPEAK
                                   TPEAK R.V.
                                             DWF
                              (cms) (hrs) (mm)
                         (ha)
                                             (cms)
            ID1 06:0VF-xI
                               .000
                                        .00
                          .00
                                    .00
                                             .000
**DRY**
                         4.52 .430 1.58 14.46
            +ID2 07:103
                                             .000
            +ID3 02:206
                     1.22 .003 2.65 1.99
                                             .000
            ______
            SUM 08:WRswl
                          5.74 .430 1.58 11.81
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0027-----
*#-----|
DESIGN NASHYD
               Area
                    (ha) = 1.13 Curve Number (CN) = 50.00
| 05:208 DT= 1.00 |
                   (mm)= 1.500 # of Linear Res.(N)= 3.00
               Ia
----- U.H. Tp(hrs)= .850
  Unit Hyd Qpeak (cms)= .051
  PEAK FLOW
           (cms)=
                  .003 (i)
                 2.700
   TIME TO PEAK (hrs)=
                 1.989
            (mm) =
   RUNOFF VOLUME
   TOTAL RAINFALL
             (mm) =
                  25.000
  RUNOFF COEFFICIENT =
                  .080
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
001:0028-----
*#-----|
*#
           Total Flows through Outlet Channel
*#------
______
| ADD HYD (OutChan ) | ID: NHYD
                               QPEAK
                                   TPEAK
                                        R.V.
                         AREA
                                             DWF
                         (ha)
                              (cms)
                                    (hrs)
                                        (mm)
                                             (cms)
            ID1 01:SWMout
                         .00
                               .000
                                   .00 .00
                                             .000
**DRY**
                        5.74 .430 1.58 11.81 .000
            +ID2 08:WRswl
```

+ID3 05:208	1.13	.003	2.70	1.99	.000
============	========	======	======	======	=======
SUM 03:OutChan	6.87	.430	1.58	10.20	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

- 01:0029							
-							
#							
# #	Totol		and (avent		Codon C	ma alc)	
# #	IOCAL	Flows to the	east (event	ually to	Cedar C	reek)	
#							
ADD HYD (TotE		TD: NHYD	AREA	QPEAK	TPEAK	R.V.	DWE
	, , 	ID. WIIID		(cms)			
	ID1	01:SWMout		.000			
*DRY**	LTDO	A9+UDcu1	E 7/	.430	1 50	11 01	000
	+102	08:WRswl	5./4	.430	1.00	11.01	.000
	+ID3	09:UCtoE	71.82	2.222	1.92	14.32	.000
				======		======	======
	SUM	04:TotE	77.56	2.311	1.92	14.13	.000
NOTE: PEAK FI	OWS DO 1	NOT INCLUDE BA	ASFFLOWS TF	ANY.			
- 01:0030							
	 	Total Flow	ws from the	 Site			
001:0030	 	Total Flo	ws from the	 Site			
	 	Total Flow	ws from the	Site	TPEAK	R.V.	
	 	Total Flo	ws from the	 Site	TPEAK	R.V. (mm)	
		Total Flow	ws from the AREA (ha)	Site QPEAK (cms)	TPEAK	R.V. (mm)	 DWF (cms)

```
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
001:0031-----
 ** END OF RUN :
***********************************
             | Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
START
TZERO = .00 hrs on
  METOUT= 2 (output = METRIC)
  NRUN = 002
  NSTORM=
      # 1=Kit2yr.3hr
*#********************************
*# Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
*# Date
      : 01/25/2024
*# Modeller : [Amy Kyle, Water Resources Specialist]
*# Company
          : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
*# 25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
*# and the Regional Event
*#*********************************
002:0002-----
READ STORM | Filename: 2-yr, 3hr Chicago Storm - Kitchener IDF
                Comments: 2-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 34.27 mm|
```

```
RAIN
                  TIME RAIN
                            TIME RAIN
                                     TIME
        TIME
                                           RAIN
        hrs mm/hr
                  hrs mm/hr
                            hrs mm/hr
                                      hrs
                                          mm/hr
                            1.58 7.979
        .08 2.837
                  .83 15.850
                                      2.33
                                          3.697
        .17 3.094
                  .92 36.885
                            1.67 7.027
                                     2.42
                                          3.501
                            1.75 6.286 2.50
            3.409
                  1.00 109.401
                                          3.326
        . 25
                            1.83 5.694
        .33 3.803 l
                1.08 47.437
                                     2.58
                                          3.169
        .42 4.314 |
                            1.92 5.211 | 2.67
                  1.17 26.381
                                          3.028
        .50 5.002 | 1.25 18.051 | 2.00 4.807 | 2.75 2.899
        .58 5.982 | 1.33 13.687 |
                            2.08 4.466
                                     2.83
                                          2.783
           7.493
                  1.42 11.030
                            2.17 4.173 | 2.92
        .67
                                          2.676
        .75 10.127
                  1.50 9.251
                            2.25 3.920 3.00
                                          2.578
______
002:0003-----
*#-----|
*# Proposed Drainage Conditions (Internal Areas)
*#
*#
   Small portion of West Road Ditch draining offsite to the east through
*#
                 By-Pass Storm Sewer(BPSS)
*#-----|
                  (ha)= .14 Curve Number (CN)=50.00
DESIGN NASHYD
              Area
| 01:200 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .260
  Unit Hyd Qpeak (cms)=
                .021
                 .001 (i)
  PEAK FLOW
           (cms)=
  TIME TO PEAK
           (hrs)=
                  1.350
  RUNOFF VOLUME
             (mm) =
                3.741
            (mm) =
  TOTAL RAINFALL
                 34.271
  RUNOFF COEFFICIENT =
                  .109
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0004-----
*#-----|
*#
*# Proposed developed catchment draining offsite to the east through BPSS
```

```
*#------|
-----
                 Area (ha)= .64
| DESIGN STANDHYD
| 02:201 DT= 1.00 | Total Imp(%)= 90.00
                                    Dir. Conn.(%)=
                                                  50.00
                      IMPERVIOUS
                                 PERVIOUS (i)
                       .58
   Surface Area (ha)=
                                    .06
   Dep. Storage (mm)=
                         .80
                                   1.50
   Average Slope (%)=
                        2.00
                                   2.00
                         65.32
   Length
                 (m) =
                                  40.00
   Mannings n
                        .013
                                  .250
   Max.eff.Inten.(mm/hr)=
                     109.40
                                 168.34
            over (min)
                         2.00
                                   7.00
                        1.55 (ii) 7.28 (ii)
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                        2.00
                                  7.00
   Unit Hyd. peak (cms)=
                         .65
                                   .16
                                             *TOTALS*
                                   .02
   PEAK FLOW
               (cms)=
                         .09
                                               .103 (iii)
                                 1.10
13.61
                       1.00
   TIME TO PEAK (hrs)=
                                              1.000
   RUNOFF VOLUME
               (mm) =
                        33.47
                                             23.542
   TOTAL RAINFALL (mm)=
                       34.27
                                  34.27
                                             34.271
   RUNOFF COEFFICIENT =
                        .98
                                   .40
                                               .687
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0005-----
```

```
*#-----|
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#------
              Area (ha)= .55 Curve Number (CN)=50.00
DESIGN NASHYD
| 03:203 DT= 1.00 |
              Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)=
                        .080
   Unit Hyd Qpeak (cms)=
                   .263
   PEAK FLOW
            (cms)=
                  .010 (i)
                  1.083
   TIME TO PEAK
            (hrs)=
   RUNOFF VOLUME
             (mm) =
                  3.745
                 34.271
   TOTAL RAINFALL
            ( mm ) =
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
______
002:0006-----
*#------|
*#
       Total internal area draining onto agricultural area to the east
*#
*#-----|
| ADD HYD (IntUcE ) | ID: NHYD
                          AREA
                               QPEAK
                                     TPEAK R.V.
                                               DWF
-----
                               (cms) (hrs) (mm)
                          (ha)
                                               (cms)
                           .14
             ID1 01:200
                                .001 1.35 3.74
                                               .000
            +ID2 02:201
                      .64 .103 1.00 23.54 .000
                      .55 .010 1.08 3.74 .000
            +ID3 03:203
             ______
             SUM 05:IntUcE 1.33 .109 1.00 13.27 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0007-----
*#
*#
         Proposed industrial lots draining to Rear Lot Ditch
*#-----|
| DESIGN STANDHYD | Area (ha)= 8.82
| 06:202 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 80.00
                  IMPERVIOUS PERVIOUS (i)
  Surface Area (ha)= 7.94

Dep. Storage (mm)= .80

Average Slope (%)= 2.00

Length (m)= 242.49

Mannings n = .013
                              .88
                             1.50
                             2.00
                            40.00
                            .250
   Max.eff.Inten.(mm/hr)= 109.40 23.44
over (min) 3.00 16.00
Storage Coeff. (min)= 3.41 (ii) 16.02 (ii)
```

```
3.00
Unit Hyd. Tpeak (min)=
                                   16.00
Unit Hyd. peak (cms)=
                        .34
                                    .07
                                              *TOTALS*
                                    .03
PEAK FLOW
            (cms)=
                        1.69
                                                1.695 (iii)
TIME TO PEAK (hrs)=
                       1.02
                                   1.30
                                                1.017
                     33.47
RUNOFF VOLUME
             (mm) =
                                   7.00
                                               28.177
TOTAL RAINFALL
              (mm) =
                       34.27
                                  34.27
                                              34.271
RUNOFF COEFFICIENT =
                         .98
                                                 .822
                                    .20
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
______
002:0008-----
*#------|
*#
*#
   External agricultural area draining onsite and entering Rear Lot Ditch
*#------|
           Area (ha)= .73 Curve Number (CN)=70.00
DESIGN NASHYD
| 07:104 DT= 1.00 |
               (mm) = 1.500 # of Linear Res.(N) = 3.00
            Ia
 ----- U.H. Tp(hrs)=
                    .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)=
               .018 (i)
  TIME TO PEAK (hrs)=
              1.250
               7.583
          (mm) =
  RUNOFF VOLUME
  TOTAL RAINFALL
           (mm) =
              34.271
  RUNOFF COEFFICIENT =
               .221
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0009-----
*#------
*#
    Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#-----|
ADD HYD (RLswl ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
```

```
(ha) (cms) (hrs) (mm) (cms)
8.82 1.695 1.02 28.18 .000
                   ID1 06:202
                                        .73
                                                                      .000
                  +ID2 07:104
                                               .018 1.25 7.58
                   ______
                                  9.55 1.700 1.02 26.60
                   SUM 08:RLswl
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0010-----
*#
    Proposed industrial lots draining to East Road Ditch within catchment,
*#
                          and new internal roadway
*#------|
| DESIGN STANDHYD |
                     Area (ha) = 4.92
01:204 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 80.00
                            IMPERVIOUS PERVIOUS (i)

      Surface Area
      (ha)=
      4.43

      Dep. Storage
      (mm)=
      .80

      Average Slope
      (%)=
      2.00

      Length
      (m)=
      181.11

                                            .49
                                            1.50
                                           2.00
                                           40.00
                              .013
    Mannings n
                                           .250
    Max.eff.Inten.(mm/hr) = 109.40
                                          24.32
                             3.00 15.00
2.86 (ii) 15.28 (ii)
               over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                              3.00
                                          15.00
                                            .07
    Unit Hyd. peak (cms)=
                               .39
                                                       *TOTALS*
    PEAK FLOW (cms)=
TIME TO PEAK (hrs)=
                             .99
1.02
                                           .02
                                                          .990 (iii)
                                          1.28
                                                         1.017
    TOTAL RAINFALL (mm)= 34.27
RUNOFF COEFFICIENT = .98
                                           7.00
                                                        28.177
                                          34.27
                                                       34.271
                                            .20
                                                         .822
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
002:0011-----
*#-----|
*#
          Rooftop infiltration lumped together and sized for 25mm
       runoff volume from an assumed 0.15ha rooftop area per lot (7 lots)
*#
*#-----|
ADD HYD (Roof ) | ID: NHYD
                            AREA
                                   QPEAK TPEAK R.V.
                                                     DWF
----
                                   (cms) (hrs) (mm)
                             (ha)
                                                    (cms)
              ID1 01:204
                             4.92
                                    .990 1.02 28.18
                                                    .000
                         8.82 1.695 1.02 28.18 .000
              +ID2 06:202
               ______
              SUM 02:Roof
                         13.74 2.685 1.02 28.18 .000
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0012-----
ROUTE RESERVOIR | Requested routing time step = 1.0 min.
 IN>02:(Roof )
OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======
                 OUTFLOW
                         STORAGE | OUTFLOW STORAGE
                                (cms)
                   (cms)
                        (ha.m.)
                                         (ha.m.)
                    .000 .0000E+00
                                   .000 .2625E-01
                     AREA
                                  TPEAK
   ROUTING RESULTS
                            OPEAK
                                           R.V.
                     (ha) (cms) (hrs)
13.74 2.685 1.017
                                            (mm)
  INFLOW >02: (Roof ) 13.74

OUTFLOW<04: (R-inf ) .93

OVERFLOW<10: (infO ) 12.81
                                   1.017
.767
                                           28.177
                            .000
                                           6.031
                             2.653 1.017
                                           28.177
             TOTAL NUMBER OF SIMULATED OVERFLOWS = CUMULATIVE TIME OF OVERFLOWS (hours)=
                                            5
                                          4.08
             PERCENTAGE OF TIME OVERFLOWING (%)=
                                           .23
                       REDUCTION [Qout/Qin](%)=
                  FLOW
                                           .000
             TIME SHIFT OF PEAK FLOW
                                  (min) = -15.00
             MAXIMUM STORAGE USED
                                  (ha.m.)=.2625E-01
```

^{***} WARNING: Outflow volume is less than inflow volume.

```
002:0013-----
*#------|
*#
         Proposed SWM facility catchment (infiltration basin)
*#-----|
DESIGN NASHYD
             Area (ha)= 1.63 Curve Number (CN)=57.00 Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 09:205 DT= 1.00 |
----- U.H. Tp(hrs)= .350
  Unit Hyd Qpeak (cms)= .178
           (cms)=
  PEAK FLOW
                 .018 (i)
  TIME TO PEAK (hrs)=
                1.467
            (mm) =
                4.786
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)=
                34.271
  RUNOFF COEFFICIENT =
                 .140
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0014-----
*#-----|
*#
*#
               All flows entering SWM facility
*#-----|
ADD HYD (ToSWM
           ) | ID: NHYD
                        AREA
                            QPEAK
                                 TPEAK R.V.
                                           DWF
------
                        (ha)
                             (cms) (hrs)
                                      (mm)
                                          (cms)
           ID1 10:inf0 12.81 2.653 1.02 28.18
                                          .000
           +ID2 07:104
                    .73 .018 1.25 7.58 .000
           +ID3 09:205
                        1.63 .018 1.47 4.79
                                           .000
            ______
            SUM 06:ToSWM
                        15.17 2.661 1.02 24.67
                                          .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
```

- -

```
*#
                                                    Infiltration Portion of SWM facility
*#
*#-----|
ROUTE RESERVOIR
                                                        Requested routing time step = 1.0 min.
     IN>06:(ToSWM )
OUT<07:(SWMinf) | ======= OUTLFOW STORAGE TABLE ========
----- OUTFLOW STORAGE | OUTFLOW STORAGE
                                                               (na.m.) | (cms) (ha.m.)
.000 .0000E+00 | .044 .7033E+00
.044 .6530E-01 | .000 .0000E+00
                                                        OUTFLOW STORAGE | OUTFLOW STORAGE
                                                             (cms) (ha.m.)
       | COLE | QPEAK | TPEAK | TPEAK | (ha) (cms) (hrs) | INFLOW > 06: (ToSWM) | 15.17 | 2.661 | 1.017 | OUTFLOW < 07: (SWMinf) | 15.17 | .044 | 1.000 | OVERFLOW < 08: (OVF-I) | .00 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |
                                                                    AREA
                                                                                          QPEAK TPEAK
                                                                                                                                                R.V.
                                                                                                                                               (mm)
                                                                                                                                           24.672
                                                                                                                                           24.672
                                                                                                                                             .000
                                           TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                           CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                                                                                                                .00
                                           PERCENTAGE OF TIME OVERFLOWING (%)=
                                                                                                                                                .00
                                           PEAK FLOW REDUCTION [Qout/Qin](%)=
                                                                                                                                           1.653
                                           TIME SHIFT OF PEAK FLOW (min)= -1.00
                                                                                                          (ha.m.)=.3378E+00
                                           MAXIMUM STORAGE USED
002:0016-----
*#------
*#
*#
                                                 Active Storage Portion of SWM facility
*#------|
ROUTE RESERVOIR
                                                        Requested routing time step = 1.0 min.
| IN>08:(OVF-I ) |
OUT<01:(SWMout) ======= OUTLFOW STORAGE TABLE =======
                                                        OUTFLOW STORAGE OUTFLOW STORAGE
                                                               cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | 1.479 .2400E+00
.202 .7850E-01 | 4.101 .4070E+00
                                                             (cms)
                                                                .689 .1586E+00
                                                                                                                  .000 .0000E+00
             *** WARNING: Inflow hydrograph is dry.
```

```
AREA QPEAK
                        (cms)
   ______
                   (ha)
                               (hrs)
                                       (mm)
                   .00
                         .000
                               .000
   INFLOW >08: (OVF-I )
                                       .000
  OUTFLOW<01: (SWMout)
                                .000
                          .000
                    .00
                                       .000
             )
                   13.74
  OVERFLOW<02: (OVF
                          .000
                                .000
                                       .000
           TOTAL NUMBER OF SIMULATED OVERFLOWS =
           CUMULATIVE TIME OF OVERFLOWS (hours)=
                                       .00
           PERCENTAGE OF TIME OVERFLOWING
                               (%)=
                                      .00
*** WARNING: Inflow and ouflow hydrographs are dry.
______
002:0017-----
*#------|
   West Road Ditch, conveying external drainage from the west around the
*#
            proposed SWM facility to Outlet Channel
*#
*#------|
| DESIGN NASHYD |
               Area (ha)= 1.22 Curve Number (CN)=50.00
| 02:206 DT= 1.00 |
              Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)= .810
   Unit Hyd Qpeak (cms)= .058
   PEAK FLOW
            (cms) = .006 (i)
            (hrs)=
                 2.117
   TIME TO PEAK
                 3.744
   RUNOFF VOLUME
             (mm) =
   TOTAL RAINFALL
            (mm) =
                  34.271
   RUNOFF COEFFICIENT =
                    .109
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0018-----
*#-----|
*#
*#
     Grassed area south of SWM facility draining offsite to the south
*#-----|
DESIGN NASHYD | Area (ha)= .14 Curve Number (CN)=50.00
| 10:207 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
```

TPEAK

R.V.

ROUTING RESULTS

```
----- U.H. Tp(hrs)=
                   .070
  Unit Hyd Qpeak (cms)=
               .076
  PEAK FLOW (cms)= .003 (i)
TIME TO PEAK (hrs)= 1.083
  RUNOFF VOLUME
          (mm) =
              3.744
  TOTAL RAINFALL
          (mm) =
              34.271
  RUNOFF COEFFICIENT =
               .109
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0019-----
*#------
*#
*#
        Total Flows to the east from internal catchments
*#------|
OPEAK TPEAK R.V.
                                     DWF
                    (ha) (cms) (hrs) (mm)
1.33 .109 1.00 13 27
                                     (cms)
          ID1 05:IntUcE
                                     .000
         +ID2 01:SWMout
                     .00 .000 .00 .00 .000
**DRY**
                 1.22 .006 2.12 3.74 .000
         +ID3 02:206
          ______
                    2.55 .109 1.00 8.71
          SUM 07:IntE
                                     .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0020-----
*#------
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
*#-----|
*# External industrial catchment and part of Hwy 401, draining south across
          Cedar Creek Road and entering BPSS
*#
*#------
```

```
| CALIB STANDHYD |
                     Area (ha)= 55.94
| 03:100 DT= 1.00 |
                     Total Imp(\%) = 80.00 Dir. Conn.(\%) = 50.00
                           IMPERVIOUS
                                        PERVIOUS (i)
    Surface Area
                 (ha)=
                             44.75
                                          11.19
    Dep. Storage
                                          5.00
                   (mm) =
                              2.00
                          1500.00
920
    Average Slope
                   (%)=
                                          2.00
    Length
                     (m) =
                                          30.00
    Mannings n
                                           .250
                      =
    Max.eff.Inten.(mm/hr)=
                            58.21
                                          37.61
                         18.00 27.00
18.11 (ii) 26.90 (ii)
18.00 27.00
              over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
    Unit Hyd. peak (cms)=
                              .06
                                          .04
                                                      *TOTALS*
    PEAK FLOW
                   (cms) =
                              2.84
                                           .68
                                                        3.293 (iii)
                   (hrs)=
                             1.27
    TIME TO PEAK
                                          1.50
                                                        1.300
                          32.27
    RUNOFF VOLUME
                    (mm) =
                                                       21.959
                                         11.65
    TOTAL RAINFALL
                    (mm) =
                            34.27
                                         34.27
                                                      34.271
    RUNOFF COEFFICIENT =
                              .94
                                          .34
                                                         .641
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
002:0021-----
*#------
*# External catchment containing a portion of Cedar Creek Road, a portion
*# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
*#
*#------
                Area (ha)= 14.55
DESIGN STANDHYD
| 07:101 DT= 1.00 |
               Total Imp(%)= 60.00 Dir. Conn.(%)=
                   IMPERVIOUS
                             PERVIOUS (i)
   Surface Area (ha)=
                    8.73
                               5.82
   Dep. Storage (mm)=
Average Slope (%)=
              (mm) =
                              1.50
              (%)= .80
(%)= 2.30
(m)= 311.45
                      .80
                              2.30
   Length
                             40.00
   Mannings n
                    .013
                              .250
                =
```

```
Max.eff.Inten.(mm/hr)=
                            109.40
                                           8.66
           over (min)
                                           22.00
                              4.00
Storage Coeff. (min)=
                              3.80 (ii)
                                           21.80 (ii)
Unit Hyd. Tpeak (min)=
                              4.00
                                          22.00
Unit Hyd. peak (cms)=
                               .29
                                             .05
                                                        *TOTALS*
PEAK FLOW
                (cms) =
                              1.57
                                             .08
                                                          1.587 (iii)
TIME TO PEAK
                (hrs)=
                              1.03
                                            1.42
                                                          1.033
RUNOFF VOLUME
                  (mm) =
                             33.47
                                            4.80
                                                         18.562
TOTAL RAINFALL
                  (mm) =
                             34.27
                                           34.27
                                                         34.271
RUNOFF COEFFICIENT
                               .98
                                             .14
                                                           .542
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*# *# Total area *#	 draining offsite to 	east onto a	gricultu	ral area	to the	east
ADD HYD (UCtoE) ID: NHYD ID1 05:IntUcE	AREA (ha) 1.33	(cms)			DWF (cms) .000
	+ID2 03:100	55.94	3.293		21.96	.000
	+ID3 07:101	14.55	1.587	1.03	18.56	.000
	SUM 09:UCtoE	71.82	3.823	1.27	21.11	.000
NOTE: PEAK FLO	SUM 09:UCtoE OWS DO NOT INCLUDE BA			1.27	21.11	.000

^{*#} Large external catchment west of site containing industrial property,

[#] draining into private SWM feature and then into West Road Ditch, routing

```
*#
             around SWM facility and entering Outlet Channel
*#
*#-----|
DESIGN STANDHYD
                     Area (ha)= 12.64
| 04:102 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
   Surface Area (ha)= 10.11

Dep. Storage (mm)= .80

Average Slope (%)= 3.10

(m)= 290.29

013
                         IMPERVIOUS PERVIOUS (i)
                                         2.53
                                        1.50
                                        3.10
                                       40.00
    Mannings n
                            .013
                                        .250
    Max.eff.Inten.(mm/hr)= 109.40 40.60
                        3.00 12.00
3.33 (ii) 12.20 (ii)
3.00 12.00
.35 .09
             over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                                       .09
    Unit Hyd. peak (cms)=
                                                    *TOTALS*
                                       .17
                           1.52
    PEAK FLOW
                  (cms)=
                                                     1.577 (iii)
    TIME TO PEAK (hrs)= 1.02
RUNOFF VOLUME (mm)= 33.47
TOTAL RAINFALL (mm)= 34.27
                                        1.22
                                                     1.017
                                        8.38
                                                    20.926
                                       34.27
                                                    34.271
    RUNOFF COEFFICIENT =
                            .98
                                        .24
                                                     .611
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
         CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
         THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
002:0024----
*#-----|
*#
*#
                    Infiltration in External SWM Feature
*#------
ROUTE RESERVOIR
                     Requested routing time step = 1.0 min.
| IN>04:(102 )
| OUT<05:(xSWinf) |
                     ====== OUTLFOW STORAGE TABLE =======
______
                      OUTFLOW STORAGE | OUTFLOW STORAGE

    (cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    .018
    .3759E+00

    .018
    .4380E-01
    .000
    .0000E+00
```

```
ROUTING RESULTS AREA QPEAK TPEAK
------ (ha) (cms) (hrs)
INFLOW >04: (102 ) 12.64 1.577 1.017
OUTFLOW<05: (xSWinf) 12.64 .018 .967
OVERFLOW<06: (OVF-xI) .00 .000 .000
                                                           R.V.
                                                             (mm)
                                                           20.926
                                                           20.926
                                                            .000
                  TOTAL NUMBER OF SIMULATED OVERFLOWS =
                  CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                              .00
                  PERCENTAGE OF TIME OVERFLOWING (%)=
                                                            .00
                  PEAK
                         FLOW REDUCTION [Qout/Qin](%)=
                                                           1.141
                  TIME SHIFT OF PEAK FLOW (min)= -3.00
                  MAXIMUM STORAGE USED (ha.m.)=.2478E+00
______
002:0025-----
*#------|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
                      SWM facility and entering Outlet Channel
*#
*#-----|
DESIGN STANDHYD | Area (ha)= 4.52
| 07:103 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
                            IMPERVIOUS PERVIOUS (i)

      Surface Area
      (ha)=
      3.62

      Dep. Storage
      (mm)=
      .80

      Average Slope
      (%)=
      5.30

      (**)
      173.50

                             3.62
                                             .90
                                            1.50
                                             5.30
    Length
                    (m)= 173.59
                                           40.00
                               .013
    Mannings n
                                            .250
    Max.eff.Inten.(mm/hr)= 109.40 45.49 over (min) 2.00 9.00 Storage Coeff. (min)= 2.08 (ii) 9.30 (ii) Unit Hyd. Tpeak (min)= 2.00 9.00 Unit Hyd. peak (cms)= .54 .12
                                                          *TOTALS*
                                           .07
                               .63
    PEAK FLOW
                    (cms)=
                                                           .655 (iii)
                   (hrs)=
                                            1.17
    TIME TO PEAK
                                1.00
                                                           1.000
                           33.47
34.27
    RUNOFF VOLUME
                    (mm) =
                                             8.38
                                                          20.926
    TOTAL RAINFALL (mm)=
                                            34.27
                                                         34.271
    RUNOFF COEFFICIENT =
                                            .24
                               .98
                                                           .611
```

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

```
CN* = 50.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
```

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
002:0026-----
*#------|
*#
*#
          Total Flows through West Road Ditch
*#------
           ) | ID: NHYD AREA
ADD HYD (WRswl
                           QPEAK TPEAK R.V.
                                          DWF
-----
                           (cms) (hrs) (mm)
                       (ha)
                                         (cms)
           ID1 06:0VF-xI
                        .00
                            .000 .00 .00
                                         .000
**DRY**
                       4.52 .655 1.00 20.93 .000
           +ID2 07:103
                       1.22 .006 2.12 3.74
           +ID3 02:206
           ______
           SUM 08:WRswl
                    5.74 .655
                                 1.00 17.27
                                          .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0027-----
*#-----|
DESIGN NASHYD | Area (ha)= 1.13 Curve Number (CN)=50.00
| 05:208 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)=
                      .850
  Unit Hyd Qpeak (cms)= .051
  PEAK FLOW
          (cms)=
                 .005 (i)
  TIME TO PEAK (hrs)=
                 2.167
           (mm)=
  RUNOFF VOLUME
                3.744
  TOTAL RAINFALL (mm)=
               34.271
  RUNOFF COEFFICIENT = .109
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

'# '# '# '# '#	Total	Flows through	Outlet Cha	nnel			·
ADD HYD (OutChan)	ID: NHYD	AREA	-	TPEAK		
DRY	ID1	01:SWMout		(cms) .000			
DRY	+ID2	08:WRswl	5.74	.655	1.00	17.27	.000
	+ID3	05:208	1.13	.005	2.17	3.74	.000
		======== 03:OutChan				15.05	.000
 002:0029 *#	 						
· ·- 002:0029 ·- ·# ·# ·#	 - Total	Flows to the		ually to	Cedar C	reek)	
	Total	Flows to the ID: NHYD	east (event	ually to	Cedar C	reek)	 DWF
	Total	Flows to the	east (event	ually to QPEAK (cms)	Cedar C TPEAK (hrs)	reek)	 DWF
	Total) ID1	Flows to the ID: NHYD	east (event AREA	Ually to QPEAK (cms) .000	Cedar C TPEAK (hrs)	reek) R.V. (mm)	DWF (cms)
	Total) ID1 +ID2	Flows to the ID: NHYD 01:SWMout	east (eventAREA (ha) .00	Ually to QPEAK (cms) .000	TPEAK (hrs) .00	R.V. (mm)	DWF (cms)
	Total	Flows to the ID: NHYD 01:SWMout 08:WRswl	east (event AREA (ha) .00 5.74 71.82	Ually to QPEAK (cms) .000 .655 3.823	TPEAK (hrs) .00 1.00 1.27	R.V. (mm) .00 17.27	DWF (cms) .000 .000

```
*#-----|
*#
*#
           Total Flows from the Site
*#-----|
.14 .003 1.08 3.74
        +ID2 10:207
                               .000
        ______
        SUM 06:AllFlo 77.70 4.002 1.27 20.80
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0002-----
** END OF RUN:
| Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
------ Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
 TZERO = .00 hrs on
 METOUT= 2 (output = METRIC)
 NRUN = 005
 NSTORM= 1
   # 1=Kit5yr.3hr
005:0002-----
*#*********************************
```

```
Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
           : 01/25/2024
*#
  Date
*# Modeller
           : [Amy Kyle, Water Resources Specialist]
*#
           : Stantec Consulting Ltd. (Waterloo)
  Company
*#
  License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
 The storm events modelled are:
*#
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*#**********************
005:0002-----
                Filename: 5-yr, 3hr Chicago Storm - Kitchener IDF
READ STORM
| Ptotal= 47.26 mm|
                Comments: 5-yr, 3hr Chicago Storm - Kitchener IDF
         TIME
              RAIN
                     TIME
                          RAIN
                                 TIME
                                      RAIN |
                                             TIME
                                                  RAIN
          hrs
              mm/hr
                      hrs
                          mm/hr l
                                 hrs
                                      mm/hr
                                             hrs
                                                  mm/hr
          .08
              3.031
                      .83 24.598
                                 1.58 11.053
                                             2.33
                                                 4.231
          .17
              3.380
                      .92 57.395
                                 1.67 9.458
                                             2.42
                                                  3.949
          .25
                     1.00 139.288
                                1.75 8.241
              3.819
                                            2.50
                                                  3.701
          .33
              4.385
                     1.08 72.741
                                 1.83 7.286
                                             2.58
                                                 3.483
          .42
              5.141
                     1.17 42.120
                                 1.92 6.519
                                             2.67
                                                 3.288
          .50
              6.195
                     1.25 28.378
                                2.00 5.892
                                            2.75
                                                3.114
                                 2.08
          .58
              7.751
                     1.33 20.884
                                      5.370
                                            2.83
                                                  2.957
          .67 10.239
                     1.42 16.280
                                 2.17 4.930 | 2.92
                                                  2.815
                     1.50 13.216
                                 2.25 4.554 | 3.00
          .75 14.725
                                                  2.687
005:0003-----
*#------
*# Proposed Drainage Conditions (Internal Areas)
*#-----|
*#
*#
    Small portion of West Road Ditch draining offsite to the east through
*#
                    By-Pass Storm Sewer(BPSS)
*#
*#------
DESIGN NASHYD
                 Area
                      (ha)=
                            .14 Curve Number
                                            (CN) = 50.00
| 01:200 DT= 1.00 |
                            1.500 # of Linear Res.(N)= 3.00
                Ia
                      (mm) =
                U.H. Tp(hrs)=
                           .260
```

*#

```
(cms)=
    PEAK FLOW
                           .003 (i)
    TIME TO PEAK (hrs)=
                         1.367
6.981
    RUNOFF VOLUME (mm)=
                   (mm) =
    TOTAL RAINFALL
                           47.258
    RUNOFF COEFFICIENT =
                            .148
    (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0004-----
*#------|
*# Proposed developed catchment draining offsite to the east through BPSS
*#-----|
                     Area (ha)= .64
| DESIGN STANDHYD |
02:201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 50.00
                           IMPERVIOUS PERVIOUS (i)

      Surface Area
      (ha)=
      .58

      Dep. Storage
      (mm)=
      .80

      Average Slope
      (%)=
      2.00

      Length
      (m)=
      65.32

                           .58
                                           .06
                                           1.50
                                          2.00
                                          40.00
    Mannings n
                                           .250
                             .013
    Max.eff.Inten.(mm/hr) = 139.29
                                        286.71
                            1.00 6.00
1.41 (ii) 6.04 (ii)
              over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                             1.00
                                         6.00
    Unit Hyd. peak (cms)=
                              .86
                                           .19
                                                      *TOTALS*
    PEAK FLOW (cms)=
TIME TO PEAK (hrs)=
                            .12
1.00
                                        1.08
                                          .04
                                                        .143 (iii)
                                                       1.000
    TOTAL RAINFALL (mm)= 46.46
RUNOFF COEFFICIENT = .98
                                         22.56
                                                      34.507
                                        47.26
                                                     47.258
                                          .48
                                                        .730
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
          CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
          THAN THE STORAGE COEFFICIENT.
```

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Unit Hyd Qpeak (cms)= .021

```
005:0005-----
*#-----|
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#------|
             Area (ha)= .55 Curve Number (CN)=50.00
Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
DESIGN NASHYD
03:203 DT= 1.00
             U.H. Tp(hrs) = .080
-----
  Unit Hyd Qpeak (cms)= .263
           (cms) = .019 (i)
  PEAK FLOW
           (hrs)=
                1.100
6.985
  TIME TO PEAK
  RUNOFF VOLUME
            (mm) =
  TOTAL RAINFALL (mm)=
                47.258
  RUNOFF COEFFICIENT =
                 .148
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0006-----
*#-----|
      Total internal area draining onto agricultural area to the east
*#
*#------|
| ADD HYD (IntUcE ) | ID: NHYD
                       AREA
                            QPEAK TPEAK R.V.
                                          DWF
                            (cms) (hrs) (mm)
-----
                       (ha)
                                          (cms)
                             .003 1.37 6.98
           ID1 01:200
                        . 14
                                          .000
                        .64 .143 1.00 34.51 .000
           +ID2 02:201
           +ID3 03:203
                        .55 .019 1.10 6.98
                                          .000
            ______
            SUM 05:IntUcE 1.33 .155
                                  1.00 20.23
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
005:0007-----
```

```
*#
*#
           Proposed industrial lots draining to Rear Lot Ditch
*#
*#-----|
DESIGN STANDHYD
                  Area (ha) = 8.82
                 Total Imp(%)= 90.00 Dir. Conn.(%)=
| 06:202 DT= 1.00 |
                                                  80.00
                      IMPERVIOUS
                                 PERVIOUS (i)
   Surface Area
                        7.94
               (ha)=
                                    .88
               (mm) =
   Dep. Storage
                                    1.50
                         .80
   Average Slope
               (%)=
                        2.00
                                   2.00
                        242.49
   Length
                 (m) =
                                  40.00
   Mannings n
                        .013
                                   .250
   Max.eff.Inten.(mm/hr)=
                       139.29
                                  47.27
            over (min)
                        3.00
                                  13.00
                     3.09 (ii) 12.62 (ii)
3.00 13.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                         .37
   Unit Hyd. peak (cms)=
                                   .09
                                             *TOTALS*
                                   .07
   PEAK FLOW
               (cms)=
                        2.26
                                              2.283 (iii)
                        1.02
                                  1.25
   TIME TO PEAK
                (hrs)=
                                              1.017
   RUNOFF VOLUME
                                             39.660
               (mm) =
                       46.46
                                  12.47
   TOTAL RAINFALL
                (mm) =
                       47.26
                                  47.26
                                            47.258
   RUNOFF COEFFICIENT =
                         .98
                                   .26
                                              .839
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
    External agricultural area draining onsite and entering Rear Lot Ditch
*#-----|
```

.190

Unit Hyd Qpeak (cms)= .147

----- U.H. Tp(hrs)=

```
RUNOFF COEFFICIENT = .287
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0009-----
*#------|
*#
*#
     Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#------
______
| ADD HYD (RLswl ) | ID: NHYD
                                QPEAK
                          AREA
                                     TPEAK
                                          R.V.
                                                DWF
_____
                          (ha) (cms) (hrs) (mm)
                                               (cms)
                          8.82 2.283 1.02 39.66
             ID1 06:202
                                               .000
            +ID2 07:104
                           .73
                               .035 1.25 13.54
                                                .000
             ______
             SUM 08:RLswl
                          9.55
                               2.294 1.02 37.66
                                               .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
005:0010-----
*#
*#
   Proposed industrial lots draining to East Road Ditch within catchment,
                 and new internal roadway
*#
*#
*#-----|
DESIGN STANDHYD
               Area (ha) = 4.92
| 01:204 DT= 1.00 |
              Total Imp(%)= 90.00 Dir. Conn.(%)=
                   IMPERVIOUS
                            PERVIOUS (i)
  Surface Area (ha)= 4.43

Dep. Storage (mm)= .80

Average Slope (%)= 2.00

Length (m)= 181.11
                              .49
                             1.50
                             2.00
                            40.00
                   .013
   Mannings n
                             .250
              =
```

PEAK FLOW (cms)= .035 (i) TIME TO PEAK (hrs)= 1.250

(mm) =

(mm) =

13.542

47.258

RUNOFF VOLUME

TOTAL RAINFALL

```
Max.eff.Inten.(mm/hr)= 139.29
over (min) 3.00
                                   48.75
                                   12.00
Storage Coeff. (min)=
                        2.60 (ii) 12.00 (ii)
Unit Hyd. Tpeak (min)=
                        3.00
                                    12.00
Unit Hyd. peak (cms)=
                         .41
                                     .09
                                                *TOTALS*
                                    .04
PEAK FLOW
            (cms)=
                        1.31
                                                  1.323 (iii)
             (hrs)=
TIME TO PEAK
                         1.02
                                    1.23
                                                  1.017
                    46.46
47.26
RUNOFF VOLUME
               (mm) =
                                   12.47
                                                39.660
             (mm) =
                                   47.26
TOTAL RAINFALL
                                                47.258
RUNOFF COEFFICIENT =
                        .98
                                     .26
                                                 .839
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0011-----*#------| *# Rooftop infiltration lumped together and sized for 25mm runoff volume from an assumed 0.15ha rooftop area per lot (7 lots) *#-----| | ADD HYD (Roof) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (cms) (hrs) (mm) -----(ha) (cms) 4.92 1.323 1.02 39.66 ID1 01:204 .000 8.82 2.283 1.02 39.66 .000 +ID2 06:202 ______ SUM 02:Roof 13.74 3.606 1.02 39.66 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 005:0012-----______ ROUTE RESERVOIR Requested routing time step = 1.0 min. | IN>02:(Roof) OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======

OUTFLOW STORAGE | OUTFLOW STORAGE

```
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .000 .2625E-01
  R.V.
                                    (mm)
                                    39,660
                                   8.488
                             1.017 39.660
           TOTAL NUMBER OF SIMULATED OVERFLOWS = 5
CUMULATIVE TIME OF OVERFLOWS (hours)= 3.80
           PERCENTAGE OF TIME OVERFLOWING (%)=
                                    .22
           PEAK FLOW REDUCTION [Qout/Qin](%)= .000
           TIME SHIFT OF PEAK FLOW (min)= -19.00
           MAXIMUM STORAGE USED
                             (ha.m.)=.2625E-01
   *** WARNING: Outflow volume is less than inflow volume.
*#------|
         Proposed SWM facility catchment (infiltration basin)
*#
*#-----|
Unit Hyd Qpeak (cms)= .178
           (cms) = .035 (i)
  PEAK FLOW
  TIME TO PEAK (hrs)= 1.483
            (mm) =
                8.820
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)=
                 47.258
  RUNOFF COEFFICIENT =
                  .187
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0014-----
*#-----|
*#
               All flows entering SWM facility
*#
```

```
*#
*#-----|
| ADD HYD (ToSWM ) | ID: NHYD
                            AREA
                                   QPEAK TPEAK R.V.
                                                   DWF
              (ha) (cms) (hrs) (mm)
ID1 10:inf0 13.08 3.571 1.02 39.66
                                                   (cms)
                                                  .000
                             .73 .035 1.25 13.54
             +ID2 07:104
                                                   .000
             +ID3 09:205
                        1.63 .035 1.48 8.82 .000
              ______
              SUM 06:ToSWM
                         15.44 3.587 1.02 35.17
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
*#
*#
               Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR
                 Requested routing time step = 1.0 min.
IN>06:(ToSWM)
            ======= OUTLFOW STORAGE TABLE ======
OUT<07:(SWMinf)
                 OUTFLOW STORAGE | OUTFLOW STORAGE
                       (ha.m.)
                                (cms)
                  (cms)
                                        (ha.m.)
                   .000 .0000E+00 | .044 .7033E+00
.044 .6530E-01 | .000 .0000E+00
  .00
.00
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                            0
             CUMULATIVE TIME OF OVERFLOWS (hours)=
             PERCENTAGE OF TIME OVERFLOWING (%)=
             PEAK FLOW REDUCTION [Qout/Qin](%)=
                                         1.227
             TIME SHIFT OF PEAK FLOW (min)=
             MAXIMUM STORAGE USED
                               (ha.m.)=.5054E+00
```

```
005:0016-----
*#-----|
*#
               Active Storage Portion of SWM facility
*#
*#------|
                 Requested routing time step = 1.0 min.
 ROUTE RESERVOIR
 IN>08:(OVF-I )
OUT<01:(SWMout) | ====== OUTLFOW STORAGE TABLE ======
                 OUTFLOW STORAGE | OUTFLOW STORAGE
                               (cms) (ha.m.)
1.479 .2400E+00
4.101 .4070E+00
                  (cms) (ha.m.)
                   .000 .0000E+00
                   .202 .7850E-01
                                   .000 .0000E+00
                   .689 .1586E+00
    *** WARNING: Inflow hydrograph is dry.
                    AREA
   ROUTING RESULTS
                            OPEAK
                                  TPEAK
                                           R.V.
                     (ha)
                                  (hrs)
   -----
                           (cms)
                                           (mm)
                     .00
                                   .000
   INFLOW >08: (OVF-I )
                            .000
                                           .000
   OUTFLOW<01: (SWMout)
                     .00
                            .000
                                   .000
                                           .000
  OVERFLOW<02: (OVF )
                     13.74
                            .000
                                   .000
                                           .000
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                           0
             CUMULATIVE TIME OF OVERFLOWS (hours)=
                                           .00
             PERCENTAGE OF TIME OVERFLOWING
                                  (%)=
                                           .00
*** WARNING: Inflow and ouflow hydrographs are dry.
005:0017-----
*#-----|
*#
    West Road Ditch, conveying external drainage from the west around the
             proposed SWM facility to Outlet Channel
*#
*#-----|
| DESIGN NASHYD
                      (ha) = 1.22 Curve Number (CN) = 50.00
               Area
| 02:206 DT= 1.00 |
                     (mm) = 1.500 \# of Linear Res.(N) = 3.00
                 Ia
                 U.H. Tp(hrs) = .810
   Unit Hyd Qpeak (cms)= .058
              (cms) = .012 (i)
   PEAK FLOW
```

```
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
______
005:0018-----
*#------
     Grassed area south of SWM facility draining offsite to the south
*#
*#------
             Area (ha)= .14 Curve Number (CN)=50.00
DESIGN NASHYD
             Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 10:207 DT= 1.00 |
Unit Hyd Qpeak (cms)= .076
  PEAK FLOW (cms)= .005 (i)
TIME TO PEAK (hrs)= 1.083
           (mm) =
  RUNOFF VOLUME
                6.984
  TOTAL RAINFALL (mm)= 47.258
  RUNOFF COEFFICIENT = .148
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
*#
          Total Flows to the east from internal catchments
*#------|
| ADD HYD (IntE ) | ID: NHYD
                        AREA
                            QPEAK TPEAK R.V.
                                          DWF
                       (ha) (cms) (hrs) (mm)
1.33 .155 1.00 20.23
-----
                                          (cms)
           ID1 05:IntUcE
                                          .000
                        .00 .000 .00 .00 .000
           +ID2 01:SWMout
**DRY**
                       1.22 .012 2.08 6.98
           +ID3 02:206
                                           .000
```

TIME TO PEAK (hrs)= 2.083 RUNOFF VOLUME (mm)= 6.984

RUNOFF COEFFICIENT =

(mm) = 47.258

.148

TOTAL RAINFALL

SUM 07:IntE 2.55 .155 1.00 13.89 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0020-----*#------*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches) *#------*# External industrial catchment and part of Hwy 401, draining south across Cedar Creek Road and entering BPSS *#-----| CALIB STANDHYD | Area (ha)= 55.94 | 03:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)= ______ IMPERVIOUS PERVIOUS (i) 44.75 Surface Area (ha)= 11.19

 Dep. Storage
 (mm)=
 2.00

 Average Slope
 (%)=
 1.60

 Length
 (m)=
 1500.00

 Mannings n
 (m)=
 1500.00

 5.00 2.00 30.00 .020 Mannings n .250 77.05 22.00 89.81 Max.eff.Inten.(mm/hr)= over (min) 15.00 15.23 (ii) 21.82 (ii) 15.00 22.00 Storage Coeff. (min)= Unit Hyd. Tpeak (min)= Unit Hyd. peak (cms)= .05 .07 *TOTALS* 1.42 PEAK FLOW (cms)= 4.46 5.512 (iii) TIME TO PEAK (hrs)= 1.23 1.42 1.283 20.00 45.26 RUNOFF VOLUME (mm) =32.629 TOTAL RAINFALL (mm) =47.26 47.26 47.258 RUNOFF COEFFICIENT = .42 .96 .690 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 64.0$ Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

```
005:0021-----
*#------|
*# External catchment containing a portion of Cedar Creek Road, a portion
*# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
*#
*#-----|
DESIGN STANDHYD
                Area (ha)= 14.55
| 07:101 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 48.00
                     IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)=
Dep. Storage (mm)=
Average Slope (%)=
                      8.73
                                5.82
                       .80
                                1.50
                      2.30
                                2.30
   Length
               (m)=
                    311.45
                               40.00
   Mannings n
                                .250
                       .013
   Max.eff.Inten.(mm/hr)= 139.29 19.01
                   3.00 17.00
3.45 (ii) 16.59 (ii)
3.00 17.00
.34 .07
           over (min)
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                                         *TOTALS*
                      2.18
                               .19
1.33
   PEAK FLOW
              (cms)=
                                           2.214 (iii)
                   1.02
46.46
47.26
   TIME TO PEAK
              (hrs)=
                                           1.017
              (mm) =
   RUNOFF VOLUME
                                8.80
                                         26.877
   TOTAL RAINFALL (mm)=
                                47.26
                                         47.258
   RUNOFF COEFFICIENT =
                                .19
                       .98
                                           .569
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
       CN* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
       THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
005:0022----
*#------
     Total area draining offsite to east onto agricultural area to the east
*#
*#-----|
```

AREA QPEAK TPEAK

(ha)

R.V.

(cms) (hrs) (mm) (cms)

1.33 .155 1.00 20.23 .000

DWF

| ADD HYD (UCtoE) | ID: NHYD

ID1 05:IntUcE

+ID2	03:100	55.94	5.512	1.28	32.63	.000
+ID3	07:101	14.55	2.214	1.02	26.88	.000
====		=======		-=====		
>UM	09:UCtoF	/I.X/	b. 44 l	1.73	31.23	. 11111

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0023					
*# -					
*#					
*# Large external o				•	
*# draining into pri					n, routing
	l SWM fac	ility and	entering Outl	et Channel	
*#					
*# -					
DESIGN STANDHYD	l Anna	(ha)-	12 64		
04:102 DT= 1.00				. (onn (%)=	50.00
104.102	-	1 1 mp (70) –	00.00 DI	. com: (70)=	70.00
		IMPERVIOL	JS PERVIOUS	5 (i)	
Surface Area	(ha)=	10.11	2.53	• •	
Dep. Storage	(mm) =	.80	1.50		
Average Slope					
•	(m)=		40.00		
Mannings n	=	.013	.250		
	<i>(</i> 1	420.00	=0.00		
Max.eff.Inten.(m	•				
	•		10.00	(::)	
Storage Coeff. Unit Hyd. Tpeak		3.00	•	(11)	
Unit Hyd. peak		.37	.11		
onie nyu: peak	(CIII3)-	• 37	• + +	*TOTALS	k
PEAK FLOW	(cms)=	2.04	.35		
TIME TO PEAK	• •	1.02			· -/
RUNOFF VOLUME		46.46	14.68	30.571	
	• •	47.26	47.26	47.258	
RUNOFF COEFFICIE	NT =	.98	.31	.647	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
005:0024-----
*#------|
*#
*#
               Infiltration in External SWM Feature
*#
*#-----|
| ROUTE RESERVOIR |
                 Requested routing time step = 1.0 min.
 IN>04:(102 )
OUT<05:(xSWinf) ======= OUTLFOW STORAGE TABLE =======
                OUTFLOW
                        STORAGE | OUTFLOW
                                        STORAGE
                               (cms)
                  (cms)
                       (ha.m.)
                                        (ha.m.)
                                  .018 .3759E+00
                   .000 .0000E+00
                   .018 .4380E-01
                                  .000 .0000E+00
                    AREA
   ROUTING RESULTS
                           OPEAK
                                 TPEAK
                                          R.V.
   ------
                     (ha)
                           (cms)
                                  (hrs)
                                          (mm)
  OUTFLOW<05: (xSWinf)
OVERFLOW<06: (OVF-xI)
                                  1.017
                     12.64
                           2.179
                                         30.571
                                  .917
                     12.64
                           .018
                                         30.570
                                .000
                    .00
                            .000
                                          .000
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                           0
             CUMULATIVE TIME OF OVERFLOWS (hours)=
                                           .00
             PERCENTAGE OF TIME OVERFLOWING
                                   (%)=
                                           .00
                      REDUCTION [Qout/Qin](%)=
                 FLOW
                                          .826
             TIME SHIFT OF PEAK FLOW
                                  (min)=
                                         -6.00
            MAXIMUM STORAGE USED
                               (ha.m.)=.3695E+00
*#------|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
*#
               SWM facility and entering Outlet Channel
*#------
80.00
                                 Dir. Conn.(%)=
                                             50.00
                    IMPERVIOUS
                             PERVIOUS (i)
```

Surface Area	(ha)=	3.62	.90		
Dep. Storage	(mm)=	.80	1.50		
Average Slope	(%)=	5.30	5.30		
Length	(m)=	173.59	40.00		
Mannings n	=	.013	.250		
May off Inton (n	mm /b n \ _	120 20	01 20		
Max.eff.Inten.(•	139.29			
over	(min)	2.00	8.00		
Storage Coeff.	(min)=	1.89	(ii) 7.61	(ii)	
Unit Hyd. Tpeak	(min)=	2.00	8.00		
Unit Hyd. peak	(cms) =	.58	.15		
				*TOTALS	*
PEAK FLOW	(cms) =	.82	.14	.881	(iii)
TIME TO PEAK	(hrs)=	1.00	1.15	1.000	
RUNOFF VOLUME	(mm)=	46.46	14.68	30.571	
TOTAL RAINFALL	(mm) =	47.26	47.26	47.258	
RUNOFF COEFFICIE	ENT =	.98	.31	.647	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0026----*#-----| *# *# Total Flows through West Road Ditch *#-----| ADD HYD (WRswl) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) (cms) 00. 00. 000. 00. ID1 06:0VF-xI .000 **DRY** +ID2 07:103 4.52 .881 1.00 30.57 .000 +ID3 02:206 1.22 .012 2.08 6.98 .000 ______ 5.74 .881 1.00 25.56 .000 SUM 08:WRswl

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

- -

```
005:0027-----
*#------
DESIGN NASHYD
                  (ha) = 1.13 Curve Number (CN) = 50.00
              Area
              Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 05:208 DT= 1.00 |
              U.H. Tp(hrs)=
                      .850
  Unit Hyd Qpeak (cms)= .051
           (cms) = .011 (i)
  PEAK FLOW
           (hrs)=
  TIME TO PEAK
                2.133
                6.984
  RUNOFF VOLUME
            (mm) =
  TOTAL RAINFALL (mm)=
                 47.258
  RUNOFF COEFFICIENT =
                 .148
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
*#
          Total Flows through Outlet Channel
*#-----|
ADD HYD (OutChan ) | ID: NHYD AREA
                            QPEAK TPEAK R.V.
                                          DWF
                            (cms) (hrs) (mm)
                       (ha)
                                          (cms)
                        .00
           ID1 01:SWMout
                             .000
                                  .00 .00
                                          .000
**DRY**
           +ID2 08:WRswl 5.74 .881 1.00 25.56 .000
           +ID3 05:208
                       1.13 .011 2.13 6.98
                                          .000
            ______
            SUM 03:OutChan 6.87 .881 1.00 22.50
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
005:0029-----
*#------
*#
          Total Flows to the east (eventually to Cedar Creek)
*#
```

ADD HYD (TotE) ID: NHYD	AREA	-		R.V.	
*DRY**	ID1 01:SWMout		(cms) .000			(cms) .000
**************************************	+ID2 08:WRswl	5.74	.881	1.00	25.56	.000
	+ID3 09:UCtoE	71.82	6.441	1.23	31.23	.000
	SUM 04:TotE		6.766	1.23	30.81	.000
NOTE: PEAK FLO	OWS DO NOT INCLUDE BA	SEFLOWS IF	ANY.			
005:0030						
{# {#						
<pre> </pre> <pre> <pre> </pre> <pre> <pre> </pre> <pre> <pre> </pre> <pre> <pre> </pre> <pre> <pre> </pre> <pre> </pre> <pre> <pre> </pre> <pre> </pre> <pre> </pre> <pre> </pre> <pre> </pre> <pre> </pre> <pre> <td>Total Flow</td><td>s from the</td><td></td><td></td><td></td><td></td></pre></pre></pre></pre></pre></pre></pre>	Total Flow	s from the				
ADD HYD (AllFlo			QPEAK		R.V.	
	ID1 04:TotE		(cms) 6.766			
	+ID2 10:207	.14	.005	1.08	6.98	.000
	SUM 06:AllFlo	 77.70	6.769	1.23	30.77	 000.
NOTE: PEAK FLO	OWS DO NOT INCLUDE BA	SEFLOWS IF	ANY.			
· · -						
ΩΓ.ΩΩ31						
005:0031 						
005:0031 						
·- ·						

```
** END OF RUN: 9
```

.42

5.623

```
Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
START
                 Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
   TZERO =
           .00 hrs on
   METOUT=
           2 (output = METRIC)
   NRUN = 010
   NSTORM=
        # 1=Kit10yr.3hr
010:0002-----
*#*********************************
   Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
*#
   Date
            : 01/25/2024
*# Modeller
            : [Amy Kyle, Water Resources Specialist]
*#
   Company
            : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
*# The storm events modelled are:
   25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
*#
   and the Regional Event
010:0002-----
READ STORM
                   Filename: 10-yr, 3hr Chicago Storm - Kitchener IDF
                   Comments: 10-yr, 3hr Chicago Storm - Kitchener IDF
| Ptotal= 56.28 mm|
                 RAIN
           TIME
                        TIME
                               RAIN
                                      TIME
                                            RAIN |
                                                   TIME
                                                          RAIN
                mm/hr
           hrs
                         hrs
                              mm/hr
                                      hrs
                                           mm/hr
                                                    hrs
                                                         mm/hr
            .08
                         .83 29.808
                                      1.58 12.832
                                                   2.33
                                                         4.548
                3.160
            .17
                3.560
                         .92
                            70.748
                                      1.67 10.862
                                                   2.42
                                                         4.218
            . 25
                4.067
                        1.00 169.551
                                      1.75
                                          9.368
                                                   2.50
                                                         3.931
                4.729 |
            .33
                        1.08 89.762 l
                                      1.83
                                           8.203 l
                                                   2.58
                                                         3.678
```

1.17 51.823

1.92

7.274

2.67

3.454

```
.58 8.770 | 1.33 25.132 |
                         2.08 5.895 2.83
                                       3.076
        .67 11.826
               1.42 19.351
                         2.17 5.372
                                  2.92
                                       2.915
        .75 17.407
                1.50 15.520
                          2.25 4.928 | 3.00
                                       2.770
010:0003-----
*#------|
*# Proposed Drainage Conditions (Internal Areas)
*#------
*#
*#
   Small portion of West Road Ditch draining offsite to the east through
*#
                By-Pass Storm Sewer(BPSS)
*#------|
DESIGN NASHYD | Area (ha)= .14 Curve Number (CN)=50.00
| 01:200 DT= 1.00 |
             Ia (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)= .260
  Unit Hyd Qpeak (cms)= .021
  PEAK FLOW
          (cms)=
                .004 (i)
  TIME TO PEAK (hrs)=
               1.367
               9.715
  RUNOFF VOLUME
           (mm) =
  TOTAL RAINFALL
            (mm) =
                56.282
  RUNOFF COEFFICIENT =
                 .173
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
010:0004-----
*#------|
*# Proposed developed catchment draining offsite to the east through BPSS
*#-----|
| DESIGN STANDHYD |
            Area (ha)=
                      .64
02:201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 50.00
                IMPERVIOUS
                        PERVIOUS (i)
                 .58
  Surface Area
            (ha)=
                          .06
               .80
  Dep. Storage
            (mm) =
                         1.50
```

.50

6.884 | 1.25 34.566 |

2.00 6.519 | 2.75

3.255

```
Average Slope (%)= 2.00 2.00

Length (m)= 65.32 40.00

Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 169.55 414.94
                            1.00
           over (min)
                                            5.00
                             1.30 (ii) 5.30 (ii)
1.00 5.00
Storage Coeff. (min)=
                         1.00
.91
Unit Hyd. Tpeak (min)=
Unit Hyd. peak (cms)=
                                            .22
                                                          *TOTALS*
                (cms)= .15
(hrs)= 1.00
                                            .05
                                          ده.
1.07
PEAK FLOW
                                                            .184 (iii)
               (hrs)=
TIME TO PEAK
                                                           1.000
RUNOFF VOLUME (mm)= 55.48

TOTAL RAINFALL (mm)= 56.28

RUNOFF COEFFICIENT = .99
                                         29.35
                                                         42.416
                                          56.28
                                                         56.282
                                            .52
                                                           .754
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0006-----

- -

```
*#------|
*#
*#
        Total internal area draining onto agricultural area to the east
*#------|
| ADD HYD (IntUcE
             ) | ID: NHYD
                            AREA
                                  OPEAK
                                       TPEAK R.V.
                                                   DWF
_____
                            (ha)
                                  (cms) (hrs) (mm)
                                                  (cms)
                             .14 .004 1.37 9.72 .000
              ID1 01:200
                        .64 .184 1.00 42.42 .000
             +ID2 02:201
             +ID3 03:203
                             .55 .028 1.10 9.72
                                                  .000
              ______
                         1.33 .202 1.00 25.45 .000
              SUM 05:IntUcE
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
010:0007-----
*#
*#
          Proposed industrial lots draining to Rear Lot Ditch
*#-----|
DESIGN STANDHYD | Area (ha)= 8.82
| 06:202 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 80.00
                    IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)= 7.94
                                .88
             (mm)= .80

(%)= 2.00

(m)= 242.49

= .013
   Dep. Storage
                               1.50
   Average Slope
                                2.00
   Length
                               40.00
                     .013
   Mannings n
                               .250
                              71.63
   Max.eff.Inten.(mm/hr)= 169.55
                     3.00
          over (min)
                              11.00
                   2.86 (ii) 10.92 (ii)
3.00 11.00
   Storage Coeff. (min)=
                           11.00
   Unit Hyd. Tpeak (min)=
   Unit Hyd. peak (cms)=
                      .39
                               .10
                                        *TOTALS*
   PEAK FLOW
             (cms)=
                      2.81
                               .11
                                         2.846 (iii)
                    1.02
   TIME TO PEAK (hrs)=
                               1.22
                                         1.017
                   55.48
   RUNOFF VOLUME
              (mm)=
                              16.89
                                        47.765
   TOTAL RAINFALL (mm)= 56.28
RUNOFF COEFFICIENT = .99
                              56.28
                                        56.282
                               .30
                                         .849
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0008						
*#						
*#						
*# External agri	cultural area drain	ing onsite	and enter	ing Rea	r Lot Di	itch
*#						
*#						
DESIGN NASHYD	Area (ha)=	.73	Curve Nun	ıber (CN) = 70.6	90
DESIGN NASHYD 07:104	0 Ia (mm)=	1.500	# of Line	ear Res.	(N) = 3.6	90
	U.H. Tp(hrs)=	.190			` '	
Unit Hvd Oneak	(cms)= .147					
	(=::)					
PEAK FLOW	(cms)= .050 (i)				
TIME TO DEAK	(hrs) = 1.250	-)				
DUNCE VOLUME	(hrs)= 1.250 $(mm)=$ 18.339					
TOTAL DATALLALL	(IIIII) = 10.339					
	(mm)= 56.282					
RUNOFF CUEFFIC	IENT = .326					
(:) DEAK ELOU	DOES NOT THELLIDE DA		N.N.Y			
(1) PEAK FLOW	DOES NOT INCLUDE BA	SEFLOW IF A	ANY.			
010:0009						
*#						
*#						
*# Total area	entering Rear Lot D	itch and er	ntering SV	MF at E	ast inle	et
*#						
*#						
						•
ADD HYD (RLswl) ID: NHYD	AREA	OPEAK	TPEAK	R.V.	DWF
			(cms)			
	ID1 06:202	8.82	2.846		47.76	.000
	151 00.202	0.02	2.0.0	1.02	.,.,	.000
	+ID2 07:104	.73	.050	1.25	18.34	.000
	1102 0/.104	• / 3	.00	1.23	10.04	.000
		0 55	======= 2 062	1 02	======= //E E2	=====
	SUM 08:RLswl	9.55	2.862	1.02	45.52	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

*#

*# *#	Proposed indust	an	d new int	ernal r	oadway	y			
	SIGN STANDHYD 204 DT= 1.00					r. Coni	n.(%)=	80.00	
			IMPERVIOL	IS DE	RVTOLIS	5 (i)			
	Surface Area					3 (1)			
	Den. Storage	(mm)=	. 80		1.50				
	Average Slope	(%)=	2.00		2.00				
	Average Slope Length	(m)=	181.11		40.00				
	Mannings n	=	.013		.250				
	Max.eff.Inten.(
		(min)							
	Storage Coeff.	(min)=	2.40	(ii)	10.33	(ii)			
	Unit Hyd. Tpeak								
	Unit Hyd. peak	(cms)=	.49		.11				
	DEAL 51 011	, ,	4 4=				*TOTA		
	PEAK FLOW	•						90 (iii))
	TIME TO PEAK								
	RUNOFF VOLUME								
	TOTAL RAINFALL RUNOFF COEFFICI	(mm)=					56.2		
	KUNUFF CUEFFICI	ENI =	.99		.30		.8	49	
	(i) CN PROCED	URE SELECT	ED FOR PE	RVIOUS	LOSSES	5:			
	CN* = 50	.0 Ia =	Dep. Sto	orage (Above))			
	(ii) TIME STEP	(DT) SHOU	LD BE SMA	ALLER OR	EQUAI	L			
		STORAGE CO							
	(iii) PEAK FLOW	DOES NOT	INCLUDE E	BASEFLOW	IF AN	WY.			
		·							
10:0	0011								
-	_								
' #	_					_			
'#		op infiltr							.
*#	runott vo	lume from	an assume	ea 0.15h	a root	rtop a	rea per	Tot (7	iots)

```
*#------
8.82 2.846 1.02 47.76
             +ID2 06:202
                                                    .000
              ______
              SUM 02:Roof 13.74 4.482 1.00 47.76 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
010:0012-----
ROUTE RESERVOIR
                 Requested routing time step = 1.0 min.
IN>02:(Roof )
OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======
                 OUTFLOW STORAGE | OUTFLOW STORAGE
                  (cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .000 .2625E-01
   ROUTING RESULTS AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) INFLOW >02: (Roof ) 13.74 4.482 1.000 47.765 OUTFLOW<04: (R-inf ) .55 .000 .667 10.223
                            .000
  OVERFLOW<10: (inf0 ) 13.19
                                  1.017 47.765
                           4.479
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
             CUMULATIVE TIME OF OVERFLOWS (hours)= 3.65
             PERCENTAGE OF TIME OVERFLOWING (%)=
                                           .21
             PEAK FLOW REDUCTION [Qout/Qin](%)=
                                          .000
             TIME SHIFT OF PEAK FLOW (min)= -20.00
             MAXIMUM STORAGE USED
                                 (ha.m.)=.2625E-01
    *** WARNING: Outflow volume is less than inflow volume.
*#------
*#
           Proposed SWM facility catchment (infiltration basin)
*#
```

```
*#------
DESIGN NASHYD | Area (ha)= 1.63 Curve Number (CN)=57.00 09:205 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 09:205 DT= 1.00 |
 ----- U.H. Tp(hrs)=
                        .350
  Unit Hyd Qpeak (cms)= .178
                 .050 (i)
1.483
  PEAK FLOW (cms)=
  TIME TO PEAK (hrs)=
            (mm) =
  RUNOFF VOLUME
                  12.180
             (mm) =
                  56.282
  TOTAL RAINFALL
  RUNOFF COEFFICIENT =
                  .216
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
010:0014-----
*#------
*#
                All flows entering SWM facility
*#------|
| ADD HYD (ToSWM ) | ID: NHYD
                          AREA
                               QPEAK
                                    TPEAK R.V.
                                              DWF
                          (ha) (cms) (hrs) (mm)
13.19 4.479 1.02 47.76
                                              (cms)
            ID1 10:inf0
                                              .000
                          .73 .050 1.25 18.34
            +ID2 07:104
                                              .000
                     1.63 .050 1.48 12.18
            +ID3 09:205
                                              .000
             ______
             SUM 06:ToSWM
                      15.55 4.502 1.02 42.65 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
010:0015-----
*#
*#
              Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR | Requested routing time step = 1.0 min.
```

```
IN>06:(ToSWM )
| OUT<07:(SWMinf) |
                     ====== OUTLFOW STORAGE TABLE =======
                      OUTFLOW STORAGE | OUTFLOW STORAGE
                                           (cms)
                         (cms)
                                                      (ha.m.)
                                (ha.m.)
                                          | .044 .7033E+00
| .000 .0000E+00
                         .000 .0000E+00
                          .044 .6530E-01
                       AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) 15.55 4.502 1.017 42.653 15.55 .044 .917 42.653
    ROUTING RESULTS
    INFLOW >06: (ToSWM )
    OUTFLOW<07: (SWMinf)
   OVERFLOW<08: (OVF-I )
                           .00
                                      .000
                                               .000
                                                         .000
                 TOTAL NUMBER OF SIMULATED OVERFLOWS =
                 CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                          .00
                 PERCENTAGE OF TIME OVERFLOWING (%)=
                                                         .00
                 PEAK FLOW REDUCTION [Qout/Qin](%)=
                                                        .977
                 TIME SHIFT OF PEAK FLOW (min)= -6.00
                 MAXIMUM STORAGE USED
                                            (ha.m.)=.6250E+00
*#-----|
*#
                    Active Storage Portion of SWM facility
*#------|
ROUTE RESERVOIR
                       Requested routing time step = 1.0 min.
 IN>08:(OVF-I )
OUT<01:(SWMout) ======= OUTLFOW STORAGE TABLE =======
                       OUTFLOW STORAGE | OUTFLOW STORAGE

    cms)
    (ha.m.)
    (cms)
    (ha.m.)

    .000
    .0000E+00
    1.479
    .2400E+00

    .202
    .7850E-01
    4.101
    .4070E+00

                         (cms) (ha.m.)
                          .689 .1586E+00
                                               .000 .0000E+00
     *** WARNING: Inflow hydrograph is dry.
    ROUTING RESULTS
                           AREA QPEAK
                                              TPEAK
                                                          R.V.
                                    (cms)
                            (ha)
                                              (hrs)
                                                          (mm)
                            .00
                                     .000
                                               .000
    INFLOW >08: (OVF-I )
                                                          .000
   OUTFLOW<01: (SWMout)
OVERFLOW<02: (OVF )
                                     .000
                                               .000
                                                          .000
                            13.74 .000
                                               .000
                                                          .000
                 TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                                          0
                 CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                          .00
```

```
*** WARNING: Inflow and ouflow hydrographs are dry.
______
010:0017-----
*#------|
*#
*#
   West Road Ditch, conveying external drainage from the west around the
*#
           proposed SWM facility to Outlet Channel
*#
*#------|
----- U.H. Tp(hrs)= .810
  Unit Hyd Qpeak (cms)= .058
  PEAK FLOW (cms) = .017 (i)
               2.067
9.719
  TIME TO PEAK (hrs)=
  RUNOFF VOLUME
           (mm) =
  TOTAL RAINFALL
            (mm) =
                56.282
  RUNOFF COEFFICIENT =
                 .173
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
010:0018-----
*#------
*#
     Grassed area south of SWM facility draining offsite to the south
*#
*#------|
DESIGN NASHYD | Area (ha)= .14 Curve Number (CN)=50.00
| 10:207 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)=
                     .070
  Unit Hyd Qpeak (cms)= .076
  PEAK FLOW (cms)= .007 (i)
TIME TO PEAK (hrs)= 1.083
  RUNOFF VOLUME
           (mm) = 9.718
           (mm) = 56.282
  TOTAL RAINFALL
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
______
010:0019-----
*#------|
*#
*#
        Total Flows to the east from internal catchments
*#
*#------
                   (na) (cms) (hrs) (mm)
1.33 .202 1 00
ADD HYD (Inte ) | ID: NHYD AREA
                                  DWF
-----
                   (ha)
                                 (cms)
         ID1 05:IntUcE
                                  .000
         +ID2 01:SWMout .00 .000 .00 .00 .000
**DRY**
                1.22 .017 2.07 9.72 .000
         +ID3 02:206
         ______
         SUM 07:IntE 2.55 .202 1.00 17.92 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
______
010:0020-----
*#-----|
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
*#------
*# External industrial catchment and part of Hwy 401, draining south across
         Cedar Creek Road and entering BPSS
*#------|
CALIB STANDHYD | Area (ha)= 55.94
| 03:100 DT= 1.00 | Total Imp(%)= 80.00 Dir. Conn.(%)=
             IMPERVIOUS PERVIOUS (i)
  Surface Area (ha)= 44.75
                   11.19
  Dep. Storage (mm)= 2.00
Average Slope (%)= 1.60
                    5.00
                     2.00
```

```
Length
                         1500.00
                                        30.00
                 (m)=
Mannings n
                           .020
                                        . 250
Max.eff.Inten.(mm/hr)= 112.83
                                      111.58
          over (min) 14.00 20.00
eff. (min)= 13.90 (ii) 19.59 (ii)
Tpeak (min)= 14.00 20.00
Storage Coeff. (min)=
Unit Hyd. Tpeak (min)=
Unit Hyd. peak (cms)=
                            .08
                                         .06
                                                     *TOTALS*
                                    2.08
                         5.73
1.22
PEAK FLOW
               (cms)=
                                                       7.366 (iii)
TIME TO PEAK
              (hrs)=
                                        1.38
                                                       1.267
RUNOFF VOLUME
                      54.28
56.28
06
               (mm) =
                          54.28
                                       26.44
                                                      40.362
TOTAL RAINFALL (mm)=
                                       56.28
                                                     56.282
RUNOFF COEFFICIENT =
                                         .47
                                                       .717
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

#------# External catchment containing a portion of Cedar Creek Road, a portion *# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS *# *#-----| _____ DESIGN STANDHYD | Area (ha)= 14.55 $| 07:101 \quad DT= 1.00 \quad Total Imp(%)= 60.00 \quad Dir. Conn.(%)= 48.00$ IMPERVIOUS PERVIOUS (i) Surface Area (ha)=
Dep. Storage (mm)= 8.73 5.82 1.50 .80 2.30 Average Slope (%)= 2.30 311.45 Length (m) =40.00 Mannings n .013 .250 Max.eff.Inten.(mm/hr) = 169.55 29.79 3.00 over (min) 14.00 3.19 (ii) 14.17 (ii) 3.00 14.00 .36 .08 Storage Coeff. (min)= Unit Hyd. Tpeak (min)= Unit Hyd. peak (cms)= *TOTALS* 2.71 1.02 .29 PEAK FLOW 2.782 (iii) (cms)= TIME TO PEAK (hrs)= 1.28 1.017

```
RUNOFF VOLUME (mm)= 55.48 12.13 32.940

TOTAL RAINFALL (mm)= 56.28 56.28 56.282

RUNOFF COEFFICIENT = .99 .22 .585

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN* = 50.0 Ia = Dep. Storage (Above)
```

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

0:0022						
	-					
: :	draining offsite to					
ADD HYD (UCtoE) TD. NHAD	AREA	QPEAK	TPEAK	R.V.	DWF
(00002			(cms)			
	ID1 05:IntUcE	1.33			25.45	
	+ID2 03:100	55.94	7.366	1.27	40.36	.000
	+ID3 07:101	14.55	2.782	1.02	32.94	.000
	SUM 09:UCtoE		8.624			
		CEELOUG TE	ANY.			
NOTE: PEAK FLO	WS DO NOT INCLUDE BA	SEFLOWS IF	, ·			
	WS DO NOT INCLUDE BA					
		site contai	ning indu	ustrial	 property	

IMPERVIOUS PERVIOUS (i)

Total Imp(%)= 80.00 Dir. Conn.(%)= 50.00

Area (ha)= 12.64

| DESIGN STANDHYD |

| 04:102 DT= 1.00 |

Surface Area	(ha)=	10.11	2.53	
Dep. Storage	(mm) =	.80	1.50	
Average Slope	(%)=	3.10	3.10	
Length	(m)=	290.29	40.00	
Mannings n	=	.013	.250	
Max.eff.Inten.(mm/hr)=	169.55	112.10	
over	(min)	3.00	9.00	
Storage Coeff.	(min)=	2.79	(ii) 8.70	(ii)
Unit Hyd. Tpeak	(min)=	3.00	9.00	
Unit Hyd. peak	(cms)=	.39	.13	
				TOTALS
PEAK FLOW	(cms)=	2.53	.52	2.765 (iii)
TIME TO PEAK	(hrs)=	1.02	1.17	1.017
RUNOFF VOLUME	(mm) =	55.48	19.71	37.598
TOTAL RAINFALL	(mm) =	56.28	56.28	56.282
RUNOFF COEFFICI	ENT =	.99	.35	.668

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

#------# Infiltration in External SWM Feature *# *#-----| ROUTE RESERVOIR Requested routing time step = 1.0 min. IN>04:(102) OUT<05:(xSWinf) ====== OUTLFOW STORAGE TABLE ====== OUTFLOW OUTFLOW STORAGE STORAGE (cms) (cms) (ha.m.) (ha.m.) .018 .3759E+00 .000 .0000E+00 .018 .4380E-01 .000 .0000E+00 AREA ROUTING RESULTS QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) INFLOW >04: (102) 12.64 2.765 1.017 37.598 OUTFLOW<05: (xSWinf) 10.45 .018 .883 37.596 OVERFLOW<06: (OVF-xI) 2.19 .422 1.600 37.598

TOTAL NUMBER OF SIMULATED OVERFLOWS =

CUMULATIVE TIME OF OVERFLOWS (hours)=

2

1.57

```
PERCENTAGE OF TIME OVERFLOWING (%)= 1.15
```

PEAK FLOW REDUCTION [Qout/Qin](%)= .651
TIME SHIFT OF PEAK FLOW (min)= -8.00
MAXIMUM STORAGE USED (ha.m.)=.3759E+00

______ 010:0025-----*#-----| *# External catchment west of the site, containing a portion of exisiting *# industrial property, draining east into West Road Ditch, routing around SWM facility and entering Outlet Channel *# *#-----| | DESIGN STANDHYD | Area (ha) = 4.52 $| 07:103 \quad DT= 1.00 \quad Total Imp(%)= 80.00 \quad Dir. Conn.(%)= 50.00$ IMPERVIOUS PERVIOUS (i) Surface Area (ha)= Dep. Storage (mm)= .90 3.62 .80 1.50 (%)= (%)= 5.30 (m)= 173.59 Average Slope 5.30 Length 40.00 .013 Mannings n .250 = Max.eff.Inten.(mm/hr) = 169.55117.15 over (min) 2.00 7.00 1.75 (ii) 6.69 (ii) 2.00 7 00 Storage Coeff. (min)= Unit Hyd. Tpeak (min)= Unit Hyd. peak (cms)= .61 .17 *TOTALS* .21 PEAK FLOW (cms)= 1.01 1.112 (iii) (hrs)= TIME TO PEAK 1.00 1.12 1.000 55.48 RUNOFF VOLUME (mm) =19.71 37.598 TOTAL RAINFALL (mm) =56.28 56.28 56.282 RUNOFF COEFFICIENT = .99 .35 .668 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

THAN THE STORAGE COEFFICIENT.

010:0026

```
*#------
*#
*#
          Total Flows through West Road Ditch
*#------
          ) | ID: NHYD
ADD HYD (WRswl
                     AREA
                          QPEAK TPEAK R.V.
                                        DWF
-----
                          (cms) (hrs) (mm)
                      (ha)
                                       (cms)
                      2.19
                          .422 1.60 37.60
          ID1 06:0VF-xI
                                       .000
          +ID2 07:103
                      4.52 1.112 1.00 37.60
                                       .000
                   1.22 .017 2.07 9.72
          +ID3 02:206
                                       .000
           ______
                     7.93 1.112 1.00 33.31
           SUM 08:WRswl
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
010:0027-----
*#------
DESIGN NASHYD | Area (ha)= 1.13 Curve Number (CN)=50.00
             Ia (mm)=
                     1.500 # of Linear Res.(N)= 3.00
05:208 DT= 1.00
.
----- U.H. Tp(hrs)= .850
  Unit Hyd Qpeak (cms)= .051
  PEAK FLOW (cms) = .015 (i)
  TIME TO PEAK (hrs)= 2.117
RUNOFF VOLUME (mm)= 9.719
  TOTAL RAINFALL (mm)= 56.282
  RUNOFF COEFFICIENT = .173
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
010:0028-----
*#-----|
*#
*#
          Total Flows through Outlet Channel
*#------
```

ADD HYD (OutChan			QPEAK (cms)		(mm)	(cms)
DRY	ID1 01:SWMout	.00	.000		.00	.000
	+ID2 08:WRswl	7.93	1.112	1.00	33.31	.000
	+ID3 05:208	1.13	.015	2.12	9.72	.000
	SUM 03:OutChan				30.37	
NOTE: PEAK FLOW	NS DO NOT INCLUDE BAS	SEFLOWS IF	ANY.			
*# *#						
*#	Total Flows to the	east (event	ually to	Cedar C	reek)	
*# *#	.					
 ADD HYD (TotE		Λ D E Λ	QPEAK	TDEAV	R.V.	DWF
		(ha)	(cms)	(hrs)	(mm)	(cms)
DRY	ID1 01:SWMout	.00	.000	.00	.00	.000
	+ID2 08:WRswl	7.93	1.112	1.00	33.31	.000
	+ID3 09:UCtoE	71.82	8.624	1.22	38.58	.000
	======================================	 79.75	9.079	 1.20	38.06	.000
NOTE: PEAK ELON	NS DO NOT INCLUDE BAS	SEFIONS TE	ΔΝΥ			
NOTE: TEAR TEO	VS DO NOT INCLUDE DAS	JEI LONS II				
*# *#	-					
*#	Total Flows	s from the	Site			
*# *#	.					
	') ID: NHYD		QPEAK			
(//11/10	/ 25. 18.115	,	A	= \		D111

	ID1 04:TotE		(cms) 9.079			(cms) .000
	+ID2 10:207	.14	.007	1.08	9.72	.000
	SUM 06:AllFlo	79.89	9.085		38.01	.000
NOTE: PEAK I	FLOWS DO NOT INCLUDE BA	ASEFLOWS IF	ANY.			
010:0002 						
010:0002 						
 010:0002						
 ** END OF RUN	• 24					
*****	*********	******	****	*****	****	****
START	 Project dir.: (C:\SWMHYMO\C	EDARC~1\2	202401~4	.\	
	 Project dir.: C Rainfall dir.: C					
TZERO = .0	Rainfall dir.: 0 00 hrs on 0					
TZERO = .0	Rainfall dir.: C					
TZERO = .0 METOUT= 2 NRUN = 025 NSTORM= 1	Rainfall dir.: (00 hrs on 0 (output = METRIC)					
TZERO = .0 METOUT= 2 NRUN = 025 NSTORM= 1	Rainfall dir.: 0 00 hrs on 0					
TZERO = .0 METOUT= 2 NRUN = 025 NSTORM= 1 # 1=	Rainfall dir.: (00 hrs on 0 (output = METRIC)	C:\SWMHYMO\C	EDARC~1\Z			

```
Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
          : 01/25/2024
*#
  Date
*# Modeller
          : [Amy Kyle, Water Resources Specialist]
*#
          : Stantec Consulting Ltd. (Waterloo)
  Company
*#
  License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
 The storm events modelled are:
*#
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*#**********************
025:0002-----
                Filename: 25-yr, 3hr Chicago Storm - Kitchener IDF
READ STORM
| Ptotal= 68.26 mm|
                Comments: 25-yr, 3hr Chicago Storm - Kitchener IDF
______
         TIME
              RAIN
                     TIME
                          RAIN
                                 TIME
                                      RAIN |
                                            TIME
                                                  RAIN
          hrs
              mm/hr
                     hrs
                          mm/hr l
                                 hrs
                                     mm/hr
                                             hrs
                                                 mm/hr
          .08
              3.567
                      .83 38.324
                                1.58 16.257
                                            2.33
                                                 5.336
                      .92 87.426
                                 1.67 13.647
          .17
              4.072
                                            2.42
                                                 4.912
          .25
                     1.00 191.557
                                1.75 11.668
              4.719
                                            2.50
                                                 4.544
          .33
              5.571
                     1.08 109.318
                                 1.83 10.127
                                            2.58
                                                 4.222
          .42
              6.733
                     1.17 65.637
                                 1.92 8.900
                                            2.67
                                                 3.938
          .50
              8.387 | 1.25 44.391 |
                                2.00 7.906
                                           2.75
                                                 3.686
                                 2.08 7.088
          .58 10.876
                     1.33 32.362
                                            2.83
                                                 3.461
          .67 14.925
                     1.42 24.846
                               2.17
                                     6.405 | 2.92
                                                 3.260
                     1.50 19.811
                                 2.25 5.829
          .75 22.291
                                           3.00
                                                 3.079
025:0003-----
*#------
*# Proposed Drainage Conditions (Internal Areas)
*#-----|
*#
*#
    Small portion of West Road Ditch draining offsite to the east through
*#
                    By-Pass Storm Sewer(BPSS)
*#
*#------
DESIGN NASHYD
                 Area
                      (ha)=
                            .14 Curve Number
                                            (CN) = 50.00
| 01:200 DT= 1.00 |
                      (mm) =
                            1.500 # of Linear Res.(N)= 3.00
                Ia
                U.H. Tp(hrs)=
                           .260
```

*#

```
(cms)= .006
(hrs)= 1.367
    PEAK FLOW
                            .006 (i)
    TIME TO PEAK (hrs)=
    RUNOFF VOLUME (mm)=
                           13.890
                   (mm) =
    TOTAL RAINFALL
                          68.256
    RUNOFF COEFFICIENT =
                            .203
    (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0004-----
*#------|
*# Proposed developed catchment draining offsite to the east through BPSS
*#-----|
                     Area (ha)= .64
| DESIGN STANDHYD |
02:201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 50.00
                           IMPERVIOUS PERVIOUS (i)

      Surface Area
      (ha)=
      .58

      Dep. Storage
      (mm)=
      .80

      Average Slope
      (%)=
      2.00

      Length
      (m)=
      65.32

                            .58
                                            .06
                                           1.50
                                          2.00
                                          40.00
    Mannings n
                                           .250
                             .013
    Max.eff.Inten.(mm/hr)= 191.56
                                        521.87
                             1.00 5.00
1.24 (ii) 4.88 (ii)
              over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                              1.00
                                          5.00
    Unit Hyd. peak (cms)=
                               .94
                                           .23
                                                       *TOTALS*
    PEAK FLOW (cms)=
TIME TO PEAK (hrs)=
                            .17
1.00
                                          .07
                                         1.07
                                                         .217 (iii)
                                                       1.000
    TOTAL RAINFALL (mm)= 68.26
RUNOFF COEFFICIENT = .99
                                         38.89
                                                       53.172
                                        68.26
                                                      68.256
                                          .57
                                                        .779
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
          CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
          THAN THE STORAGE COEFFICIENT.
```

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Unit Hyd Qpeak (cms)= .021

```
025:0005-----
*#-----|
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#------|
            Area (ha)= .55 Curve Number (CN)=50.00
Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
DESIGN NASHYD
03:203 DT= 1.00
             U.H. Tp(hrs) = .080
-----
  Unit Hyd Qpeak (cms)= .263
           (cms) = .038 (i)
  PEAK FLOW
           (hrs)=
                1.100
  TIME TO PEAK
  RUNOFF VOLUME
            (mm) =
                13.893
  TOTAL RAINFALL (mm)=
                68.256
  RUNOFF COEFFICIENT =
                 . 204
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0006-----
*#-----|
      Total internal area draining onto agricultural area to the east
*#
*#------|
| ADD HYD (IntUcE ) | ID: NHYD
                       AREA
                            QPEAK TPEAK R.V.
                                          DWF
                            (cms) (hrs) (mm)
-----
                       (ha)
                                          (cms)
                        .14
                             .006 1.37 13.89
                                          .000
           ID1 01:200
                        .64 .217 1.00 53.17
           +ID2 02:201
                                         .000
           +ID3 03:203
                        .55 .038 1.10 13.89
                                          .000
            ______
            SUM 05:IntUcE 1.33 .242
                                  1.00 32.79
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
025:0007-----
```

```
*#
*#
           Proposed industrial lots draining to Rear Lot Ditch
*#
*#-----|
DESIGN STANDHYD
                  Area (ha) = 8.82
                 Total Imp(%)= 90.00 Dir. Conn.(%)=
| 06:202 DT= 1.00 |
                                                   80.00
                       IMPERVIOUS PERVIOUS (i)
   Surface Area
                       7.94
               (ha)=
                                    .88
               (mm) =
   Dep. Storage
                         .80
                                    1.50
                 (\%) = 2.00

(m) = 242.49

913
   Average Slope
               (%)=
                                    2.00
   Length
                                   40.00
   Mannings n
                        .013
                                    .250
   Max.eff.Inten.(mm/hr)=
                       191.56
                                 100.24
            over (min)
                         3.00
                                  10.00
                       2.72 (ii) 9.77 (ii)
3.00 10.00
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                         .40
   Unit Hyd. peak (cms)=
                                   .11
                                             *TOTALS*
                                   .16
   PEAK FLOW
               (cms)=
                         3.24
                                               3.305 (iii)
                        1.02
                                  1.20
   TIME TO PEAK
                (hrs)=
                                              1.017
   RUNOFF VOLUME
                       67.46
                                  23.43
                                              58.651
               (mm) =
   TOTAL RAINFALL
                (mm)=
                        68.26
                                  68.26
                                             68.256
   RUNOFF COEFFICIENT =
                         .99
                                   .34
                                               .859
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
    External agricultural area draining onsite and entering Rear Lot Ditch
*#-----|
```

.190

Unit Hyd Qpeak (cms)= .147

----- U.H. Tp(hrs)=

```
RUNOFF COEFFICIENT = .372
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0009-----
*#------|
*#
*#
     Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#------
______
| ADD HYD (RLswl ) | ID: NHYD
                           AREA
                                 QPEAK
                                      TPEAK
                                           R.V.
                                                 DWF
                           (ha) (cms) (hrs) (mm)
8.82 3.305 1.02 58.65
_____
                                                (cms)
             ID1 06:202
                                                .000
             +ID2 07:104
                           .73
                                .068 1.25 25.38
                                                 .000
             ______
             SUM 08:RLswl
                           9.55
                                3.328 1.02 56.11
                                                 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
025:0010-----
*#
*#
   Proposed industrial lots draining to East Road Ditch within catchment,
                  and new internal roadway
*#
*#
*#-----|
DESIGN STANDHYD
                Area (ha) = 4.92
| 01:204 DT= 1.00 |
               Total Imp(%)= 90.00 Dir. Conn.(%)=
                   IMPERVIOUS
                            PERVIOUS (i)
   Surface Area (ha)= 4.43

Dep. Storage (mm)= .80

Average Slope (%)= 2.00

Length (m)= 181.11
                               .49
                              1.50
                              2.00
                             40.00
                    .013
   Mannings n
                             .250
               =
```

PEAK FLOW (cms)= .068 (i) TIME TO PEAK (hrs)= 1.250

(mm) =

(mm) =

25.376

68.256

RUNOFF VOLUME

TOTAL RAINFALL

```
Max.eff.Inten.(mm/hr)= 191.56
                                  101.43
         over (min)
                       2.00
                                   9.00
                         2.28 (ii) 9.30 (ii)
Storage Coeff. (min)=
Unit Hyd. Tpeak (min)=
                        2.00
                                   9.00
Unit Hyd. peak (cms)=
                         .51
                                    .12
                                               *TOTALS*
                                    .09
PEAK FLOW
                        1.92
            (cms)=
                                                 1.951 (iii)
                    1.00
67.46
68.26
.99
             (hrs)=
TIME TO PEAK
                                   1.18
                                                 1.000
RUNOFF VOLUME
              (mm) =
                                  23.43
                                               58.651
                                  68.26
             (mm) =
TOTAL RAINFALL
                                              68.256
                                   .34
RUNOFF COEFFICIENT =
                                                .859
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0011-----*#------| *# Rooftop infiltration lumped together and sized for 25mm runoff volume from an assumed 0.15ha rooftop area per lot (7 lots) *#-----| | ADD HYD (Roof) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (cms) (hrs) (mm) (cms) -----(ha) 4.92 1.951 1.00 58.65 ID1 01:204 .000 8.82 3.305 1.02 58.65 .000 +ID2 06:202 ______ SUM 02:Roof 13.74 5.199 1.00 58.65 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 025:0012-----ROUTE RESERVOIR Requested routing time step = 1.0 min. | IN>02:(Roof) OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======

OUTFLOW STORAGE | OUTFLOW STORAGE

```
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .000 .2625E-01
  OVERFLOW<10: (inf0 ) 13.29 5.195 1.017
                                  58.651
           TOTAL NUMBER OF SIMULATED OVERFLOWS =
           CUMULATIVE TIME OF OVERFLOWS (hours)= 3.62
           PERCENTAGE OF TIME OVERFLOWING (%)=
                                   .21
           PEAK FLOW REDUCTION [Qout/Qin](%)= .000
           TIME SHIFT OF PEAK FLOW (min)= -24.00
           MAXIMUM STORAGE USED
                            (ha.m.)=.2625E-01
   *** WARNING: Outflow volume is less than inflow volume.
*#------|
         Proposed SWM facility catchment (infiltration basin)
*#
*#-----|
Unit Hyd Qpeak (cms)= .178
  PEAK FLOW (cms)= .072 (i)
TIME TO PEAK (hrs)= 1.483
            (mm) =
                17.248
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)=
                 68.256
                 .253
  RUNOFF COEFFICIENT =
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0014-----
*#-----|
*#
*#
               All flows entering SWM facility
```

```
*#
*#-----|
| ADD HYD (ToSWM ) | ID: NHYD
                             AREA
                                    QPEAK TPEAK R.V.
                                                     DWF
              (ha) (cms) (hrs) (mm)
ID1 10:inf0 13.29 5.195 1.02 58.65
                                                     (cms)
                                                   .000
                             .73 .068 1.25 25.38
              +ID2 07:104
                                                    .000
                         1.63 .072 1.48 17.25 .000
              +ID3 09:205
               ______
              SUM 06:ToSWM
                          15.65 5.227 1.02 52.79 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
*#
*#
                Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR
                 Requested routing time step = 1.0 min.
IN>06:(ToSWM)
            ======= OUTLFOW STORAGE TABLE =======
OUT<07:(SWMinf)
                 OUTFLOW STORAGE | OUTFLOW STORAGE
                        (ha.m.)
                                (cms)
                   (cms)
                                         (ha.m.)
                   .000 .0000E+00 | .044 .7033E+00
.044 .6530E-01 | .000 .0000E+00
  TOTAL NUMBER OF SIMULATED UVERFLOWS -
CUMULATIVE TIME OF OVERFLOWS (hours)= 1.28

1.32
             PEAK FLOW REDUCTION [Qout/Qin](%)=
                                           .842
             TIME SHIFT OF PEAK FLOW (min)= -8.00
             MAXIMUM STORAGE USED
                                (ha.m.)=.7033E+00
```

```
025:0016-----
*#-----|
*#
              Active Storage Portion of SWM facility
*#
*#------|
                Requested routing time step = 1.0 min.
ROUTE RESERVOIR
 IN>08:(OVF-I )
OUT<01:(SWMout) | ====== OUTLFOW STORAGE TABLE ======
                OUTFLOW STORAGE | OUTFLOW STORAGE
                  cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | 1.479 .2400E+00
.202 .7850E-01 | 4.101 .4070E+00
                  (cms) (ha.m.)
                                 .000 .0000E+00
                  .689 .1586E+00
                   AREA
                   AREA QPEAK TPEAK
(ha) (cms) (hrs)
1.58 .442 1.817
   ROUTING RESULTS
                                         R.V.
   (mm)
                          .442
   INFLOW >08: (OVF-I )
                                        52.787
  OUTFLOW<01: (SWMout) 1.58 .115 2.717 52.787 OVERFLOW<02: (OVF ) .00 .000 .000 .000
            TOTAL NUMBER OF SIMULATED OVERFLOWS =
            CUMULATIVE TIME OF OVERFLOWS (hours)=
                                          .00
            PERCENTAGE OF TIME OVERFLOWING (%)=
                                          .00
            PEAK
                 FLOW REDUCTION [Qout/Qin](%)= 25.991
            TIME SHIFT OF PEAK FLOW (min)= 54.00
            MAXIMUM STORAGE USED
                               (ha.m.)=.4460E-01
025:0017-----
*#-----|
*#
*#
    West Road Ditch, conveying external drainage from the west around the
*#
             proposed SWM facility to Outlet Channel
*#-----|
----- U.H. Tp(hrs)= .810
   Unit Hyd Qpeak (cms)= .058
```

```
TOTAL RAINFALL (mm)=
               68.256
  RUNOFF COEFFICIENT = .204
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0018-----
*#------|
*#
     Grassed area south of SWM facility draining offsite to the south
*#------
----- U.H. Tp(hrs)= .070
  Unit Hyd Qpeak (cms)= .076
  PEAK FLOW (cms) = .010 (i)
  TIME TO PEAK (hrs)=
RUNOFF VOLUME (mm)=
               1.100
               13.892
  TOTAL RAINFALL (mm)= 68.256
  RUNOFF COEFFICIENT = .204
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0019-----
*#-----|
*#
*#
         Total Flows to the east from internal catchments
*#------
| ADD HYD (IntE ) | ID: NHYD
                       (na) (cms) (hrs) (mm)
1.33 .242 1 00
                       AREA QPEAK
                                TPEAK R.V.
                                         DWF
______
                       (ha)
                                        (cms)
           ID1 05:IntUcE
                                         .000
           +ID2 01:SWMout 1.58 .115 2.72 52.79 .000
                  1.22 .024 2.07 13.89 .000
           +ID3 02:206
```

PEAK FLOW (cms)= .024 (i) TIME TO PEAK (hrs)= 2.067

RUNOFF VOLUME

(mm) =

13.893

SUM 07:IntE 4.13 .242 1.00 34.86 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Drainage	Condition Condition	ns (Includes) nent and pareek Road a (ha)=	ing Ext	ternal ====== Hwy 401 ering B	Catchi =====: , dra: PSS	ment Flo	ows t ===== outh	co Ditches)
industria	al catchm Cedar Cr 	nent and pareek Road a	irt of H and ente	Hwy 401 ering B	odra:	ining so	outh	across
industria	al catchm Cedar Cr Area Tota	ment and pa reek Road a 	ort of Found ente	Hwy 401 ering B	, dra: PSS	ining so	outh	across
DT= 1.00	Tota	n (ha)=	55.94					
DT= 1.00	Tota	1 Tmn(%)-		1				
		ir rmb(%)-	80.08) Dir	. Con	n.(%)=	50.	00
		IMPERVIOU	ıc Dı	EDI/TOLIC	(i)			
Area	(ha)=	44.75			(1)			
Slope	(%)=	1.60		2.00				
	(m) =	1500.00		30.00				
gs n	=	.020		.250				
f.Inten.(r	nm/hr)=	135.90	1	155.96				
e Coeff.	(min)=	12.90	(ii)	17.88	(ii)			
/d. peak	(cms)=	.09		.06				
0.1	, ,							
							•	.11)
) PEAK	(nrs)=	1.20						
	torage e Slope gs n f.Inten.(r over e Coeff. yd. Tpeak yd. peak LOW O PEAK VOLUME RAINFALL COEFFICI	torage (mm)= e Slope (%)= (m)= gs n = f.Inten.(mm/hr)= over (min) e Coeff. (min)= yd. Tpeak (min)= yd. peak (cms)= LOW (cms)= O PEAK (hrs)= VOLUME (mm)= RAINFALL (mm)= COEFFICIENT = CN PROCEDURE SELECTOR To State of the selector of th	torage (mm)= 2.00 e Slope (%)= 1.60 (m)= 1500.00 gs n = .020 f.Inten.(mm/hr)= 135.90 over (min) 13.00 e Coeff. (min)= 12.90 yd. Tpeak (min)= 13.00 yd. peak (cms)= .09 LOW (cms)= 7.08 O PEAK (hrs)= 1.20 VOLUME (mm)= 66.25 RAINFALL (mm)= 68.26 COEFFICIENT = .97 CN PROCEDURE SELECTED FOR PECN* = 64.0 Ia = Dep. Sto	torage (mm)= 2.00 e Slope (%)= 1.60 (m)= 1500.00 gs n = .020 f.Inten.(mm/hr)= 135.90 over (min) 13.00 e Coeff. (min)= 12.90 (ii) yd. Tpeak (min)= 13.00 yd. peak (cms)= .09 LOW (cms)= 7.08 O PEAK (hrs)= 1.20 VOLUME (mm)= 66.25 RAINFALL (mm)= 68.26 COEFFICIENT = .97 CN PROCEDURE SELECTED FOR PERVIOUS CN* = 64.0 Ia = Dep. Storage	torage (mm)= 2.00 5.00 e Slope (%)= 1.60 2.00 (m)= 1500.00 30.00 gs n = .020 .250 f.Inten.(mm/hr)= 135.90 155.96 over (min) 13.00 18.00 e Coeff. (min)= 12.90 (ii) 17.88 yd. Tpeak (min)= 13.00 18.00 yd. peak (cms)= .09 .06 LOW (cms)= 7.08 2.96 D PEAK (hrs)= 1.20 1.35 VOLUME (mm)= 66.25 35.57 RAINFALL (mm)= 68.26 68.26 COEFFICIENT = .97 .52 CN PROCEDURE SELECTED FOR PERVIOUS LOSSES CN* = 64.0 Ia = Dep. Storage (Above)	torage (mm) = 2.00 5.00 e Slope (%) = 1.60 2.00 (m) = 1500.00 30.00 gs n = .020 .250 f.Inten.(mm/hr) = 135.90 155.96 over (min) 13.00 18.00 e Coeff. (min) = 12.90 (ii) 17.88 (ii) yd. Tpeak (min) = 13.00 18.00 yd. peak (cms) = .09 .06 LOW (cms) = 7.08 2.96 D PEAK (hrs) = 1.20 1.35 VOLUME (mm) = 66.25 35.57 RAINFALL (mm) = 68.26 68.26 COEFFICIENT = .97 .52 CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:	torage (mm)= 2.00 5.00 e Slope (%)= 1.60 2.00 (m)= 1500.00 30.00 gs n = .020 .250 f.Inten.(mm/hr)= 135.90 155.96 over (min) 13.00 18.00 e Coeff. (min)= 12.90 (ii) 17.88 (ii) yd. Tpeak (min)= 13.00 18.00 yd. peak (cms)= .09 .06 **TOTAL LOW (cms)= 7.08 2.96 9.50 D PEAK (hrs)= 1.20 1.35 1.2! VOLUME (mm)= 66.25 35.57 50.93 RAINFALL (mm)= 68.26 68.26 68.26 COEFFICIENT = .97 .52 .74 CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)	torage (mm) = 2.00 5.00 e Slope (%) = 1.60 2.00 (m) = 1500.00 30.00 gs n = .020 .250 f.Inten.(mm/hr) = 135.90 155.96 over (min) 13.00 18.00 e Coeff. (min) = 12.90 (ii) 17.88 (ii) yd. Tpeak (min) = 13.00 18.00 yd. peak (cms) = .09 .06 *TOTALS* LOW (cms) = 7.08 2.96 9.560 (ii) D PEAK (hrs) = 1.20 1.35 1.250 VOLUME (mm) = 66.25 35.57 50.915 RAINFALL (mm) = 68.26 68.26 68.256 COEFFICIENT = .97 .52 .746 CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)

.....

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
025:0021-----
*#-----|
*# External catchment containing a portion of Cedar Creek Road, a portion
*# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
*#------|
DESIGN STANDHYD
                        (ha) = 14.55
                  Area
| 07:101 DT= 1.00 |
                 Total Imp(%)= 60.00 Dir. Conn.(%)=
                                                48.00
                      IMPERVIOUS
                                PERVIOUS (i)
               (ha)=
   Surface Area
                       8.73
                                  5.82
   Dep. Storage
               (mm) =
                        .80
                                  1.50
   Average Slope
                (%)=
                         2.30
                                  2.30
                       311.45
   Length
                 (m) =
                                 40.00
                                  .250
   Mannings n
                        .013
                                 42.07
   Max.eff.Inten.(mm/hr)=
                    191.56
           over (min)
                        3.00
                                 13.00
   Storage Coeff. (min)=
                        3.03 (ii) 12.60 (ii)
   Unit Hyd. Tpeak (min)=
                                 13.00
                         3.00
                                  .09
   Unit Hyd. peak (cms)=
                        .37
                                           *TOTALS*
   PEAK FLOW
               (cms)=
                        3.14
                                  .44
                                             3.259 (iii)
   TIME TO PEAK
               (hrs)=
                        1.02
                                 1.27
                                             1.017
   RUNOFF VOLUME
               (mm) =
                        67.46
                                 17.15
                                            41.299
   TOTAL RAINFALL
                (mm) =
                        68.26
                                68.26
                                            68.256
   RUNOFF COEFFICIENT =
                        .99
                                   . 25
                                             .605
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0022-----
*#-----|
*#
*#
     Total area draining offsite to east onto agricultural area to the east
```

*#-----|

AREA

(ha)

OPEAK

TPEAK

(cms) (hrs) (mm)

R.V.

DWF (cms)

| ADD HYD (UCtoE) | ID: NHYD

ID1	05:IntUcE	1.33	.242	1.00	32.79	.000
+ID2	03:100	55.94	9.560	1.25	50.91	.000
+ID3	07:101	14.55	3.259	1.02	41.30	.000
===:	=======================================	======	:======:	=====		
SUM	09:UCtoE	71.82	11.268	1.20	48.63	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:6	0023					
	-					
*#						
	Large external o					
	draining into pri					h, routing
*#	around	d SWM faci	ility and	entering Outl	et Channel	
*#						
*#	-					
•	SIGN STANDHYD	•	` '		- (0()	
04:	102 DT= 1.00	lota.	I Imp(%) =	80.00 Dir	. Conn.(%)=	50.00
			TMDEDVTOL	JS PERVIOUS	· (;)	
	Surface Area	(ha)-		2.53) (I)	
	Dep. Storage					
	Average Slope					
	Length	(%)- (m)-	200 20	40.00		
	Mannings n	(111) =	.013	.250		
	namings m	_	.013	.230		
	Max.eff.Inten.(n	nm/hr)=	191.56	150.65		
			3.00			
	Storage Coeff.	(min)=	2.66	(ii) 7.91	(ii)	
	Unit Hyd. Tpeak			8.00	(/	
	Unit Hyd. peak			.14		
		()		,	*TOTALS	*
	PEAK FLOW	(cms)=	2.92	.73	3.301	(iii)
	TIME TO PEAK	` '		1.17		• •
	RUNOFF VOLUME					
	TOTAL RAINFALL	` '				
	RUNOFF COEFFICIE		.99	.40	.692	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
025:0024-----
*#------|
*#
                Infiltration in External SWM Feature
*#-----|
                  Requested routing time step = 1.0 min.
ROUTE RESERVOIR
 IN>04:(102 )
             ======= OUTLFOW STORAGE TABLE =======
OUT<05:(xSWinf)
                  OUTFLOW STORAGE | OUTFLOW STORAGE
                   (cms)
                         (ha.m.)
                                 (cms)
                                          (ha.m.)
                    .000 .0000E+00 | .018 .3759E+00
.018 .4380E-01 | .000 .0000E+00
                     AREA
   ROUTING RESULTS
                            QPEAK TPEAK
                                             R.V.

    (ha)
    (cms)
    (hrs)
    (mm)

    12.64
    3.301
    1.017
    47.250

    8.32
    .018
    .850
    47.249

    4.32
    1.421
    1.283
    47.250

   INFLOW >04: (102 )
                     8.32
   OUTFLOW<05: (xSWinf)
  OVERFLOW<06: (OVF-xI)
                      4.32
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                              4
              CUMULATIVE TIME OF OVERFLOWS (hours)=
                                           1.87
              PERCENTAGE OF TIME OVERFLOWING (%)=
                                             1.37
                       REDUCTION [Qout/Qin](%)=
             PEAK
                  FLOW
                                            .545
              TIME SHIFT OF PEAK FLOW (min)= -10.00
             MAXIMUM STORAGE USED
                                  (ha.m.)=.3759E+00
025:0025-----
*#------|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
*#
                SWM facility and entering Outlet Channel
*#
*#-----|
| DESIGN STANDHYD |
                Area (ha) = 4.52
```

Surface Area Dep. Storage Average Slope Length Mannings n	(ha)= (mm)= (%)= (m)= =		PERVIOUS (i) .90 1.50 5.30 40.00 .250	
Max.eff.Inten.(over Storage Coeff. Unit Hyd. Tpeak Unit Hyd. peak	(min) (min)= (min)=	191.56 2.00 1.66 (ii) 2.00 .63	159.27 6.00 6.04 (ii) 6.00 .19	
PEAK FLOW TIME TO PEAK RUNOFF VOLUME TOTAL RAINFALL RUNOFF COEFFICI	(cms)= (hrs)= (mm)= (mm)=	1.15 1.00 67.46 68.26 .99	.29 1.12 27.04 68.26 .40	*TOTALS* 1.319 (iii) 1.000 47.250 68.256 .692

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

# # # # #	Total	Flows throug	h West Road	Ditch			'
ADD HYD (WRswl)	ID: NHYD	AREA	-		R.V.	DWF
	ID1	06:0VF-xI	(na) 4.32	(cms) 1.421	1.28	` '	(cms) .000
	+ID2	07:103	4.52	1.319	1.00	47.25	.000
	+ID3	02:206	1.22	.024	2.07	13.89	.000
	===: SUM	 08:WRswl	10.06	1.871	 1.28	43.20	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
025:0027-----
*#-----|
----- U.H. Tp(hrs)= .850
  Unit Hyd Qpeak (cms)= .051
              .022 (i)
  PEAK FLOW
         (cms)=
  TIME TO PEAK (hrs)=
              2.117
  RUNOFF VOLUME (mm)=
TOTAL RAINFALL (mm)=
              13.893
              68.256
  RUNOFF COEFFICIENT = .204
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
025:0028-----
*#------
*#
*#
         Total Flows through Outlet Channel
*#------
| ADD HYD (OutChan ) | ID: NHYD
                    AREA
                        OPEAK TPEAK R.V.
                                     DWF
                     (ha)
1.58
                        (cms) (hrs) (mm)
-----
                                     (cms)
          ID1 01:SWMout
                         .115 2.72 52.79
                                     .000
         +ID2 08:WRswl 10.06 1.871 1.28 43.20 .000
                    1.13 .022 2.12 13.89
          +ID3 05:208
                                     .000
          ______
          SUM 03:OutChan 12.77 1.877 1.28 41.80
                                     .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
025:0029-----
*#-----|
*#
*#
         Total Flows to the east (eventually to Cedar Creek)
```

ADD HYD (T	+ID	ID: NHYD - 1 01:SWMout 2 08:WRswl 3 09:UCtoE	1.58	QPEAK (cms) .115	(hrs) 2.72		(cms)
	+ID	2 08:WRswl	1.58	.115	2.72		
	+ID	2 08:WRswl				52.79	
			10.06	1.871			.000
	+ID	3 09:UCtoE			1.28	43.20	.000
			71.82	11.268	1.20	48.63	.000
	== SU	======== M 04:TotE	83.46	12.737		48.06	.000
NOTE: PE	AK FLOWS DO	NOT INCLUDE BA	SEFLOWS IF	ANY.			
 025:0030							
 *#							
*#	'						ı
^k #		Total Flow	s from the	Site			
*#	ı						ı
·#							
ADD HYD (A	llFlo)	ID: NHYD		QPEAK			
		- 1. 04. T-+5		(cms)			
	10	1 04:TotE	83.46	12.737	1.28	48.06	.000
	+ID	2 10:207	.14	.010	1.10	13.89	.000
		======== M 06:AllFlo		12.743		====== 48.00	

```
025:0002-----
025:0002-----
 ** END OF RUN: 49
*************************************
              Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
START
              Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
-----
  TZERO = .00 hrs on
  METOUT=
         2 (output = METRIC)
  NRUN = 050
  NSTORM=
      # 1=Kit50yr.3hr
050:0002-----
*#*********************************
  Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
*#
  Date
          : 01/25/2024
*# Modeller
          : [Amy Kyle, Water Resources Specialist]
  Company
*#
          : Stantec Consulting Ltd. (Waterloo)
*# License # : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
  The storm events modelled are:
  25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
  and the Regional Event
*±**********************************
050:0002-----
                Filename: 50-yr, 3hr Chicago Storm - Kitchener IDF
READ STORM
```

```
| Ptotal= 77.24 mm|
              Comments: 50-yr, 3hr Chicago Storm - Kitchener IDF
             RAIN |
                        RAIN |
        TIME
                   TIME
                             TIME
                                   RAIN
                                        TIME
                                             RAIN
         hrs
                              hrs
            mm/hr |
                   hrs
                       mm/hr |
                                  mm/hr |
                                        hrs
                                             mm/hr
            3.816
                   .83 44.095
         .08
                             1.58 18.483
                                        2.33
                                             5.829
         .17
            4.387
                   .92 99.987
                             1.67 15.446
                                       2.42
                                             5.344
         . 25
            5.123 |
                   1.00 214.691
                             1.75 13.144
                                       2.50
                                            4.924
         .33 6.098
                   1.08 124.641
                             1.83 11.355
                                            4.558
                                       2.58
         .42 7.433
                   1.17 75.450
                             1.92 9.934
                                       2.67
                                           4.235
            9.341 | 1.25 51.107 |
                             2.00 8.785
                                       2.75
         .50
                                            3.950
                   1.33 37.204
                            2.08 7.841 2.83
                                             3.697
         .58 12.226
         .67 16.932
                   1.42 28.478
                            2.17 7.055
                                       2.92
                                            3.470
         .75 25.505
                   1.50 22.619
                             2.25 6.393 | 3.00
                                             3.267
050:0003-----
*#------
*# Proposed Drainage Conditions (Internal Areas)
*#------|
*#
*#
   Small portion of West Road Ditch draining offsite to the east through
*#
                  By-Pass Storm Sewer(BPSS)
*#------
DESIGN NASHYD
               Area (ha)= .14 Curve Number (CN)=50.00
               Ia (mm) = 1.500
| 01:200 DT= 1.00 |
                             # of Linear Res.(N)= 3.00
               U.H. Tp(hrs) = .260
-----
   Unit Hyd Qpeak (cms)= .021
             (cms) =
   PEAK FLOW
                   .007 (i)
   TIME TO PEAK
             (hrs)=
                 1.367
   RUNOFF VOLUME
             (mm) =
                  17.392
   TOTAL RAINFALL
             (mm) =
                  77.237
   RUNOFF COEFFICIENT
                    .225
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0004-----
*#-----|
*# Proposed developed catchment draining offsite to the east through BPSS
```

```
*#
*#------|
                     Area (ha)=
                                    .64
DESIGN STANDHYD
| 02:201 DT= 1.00 |
                    Total Imp(\%) = 90.00 Dir. Conn.(\%) = 50.00
                         IMPERVIOUS PERVIOUS (i)
                           .58
    Surface Area
                 (ha)=
                                         .06
    Dep. Storage (mm)=
Average Slope (%)=
                            .80
                                        1.50
                         . 80
2.00
                                       2.00
    Length
                   (m) =
                           65.32
                                       40.00
    Mannings n
                           .013
                                        .250
                        214.69
    Max.eff.Inten.(mm/hr)=
                                     624.10
                          1.00 5.00
1.18 (ii) 4.58 (ii)
             over (min)
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
                            1.00
                                       5.00
    Unit Hyd. peak (cms)=
                            .97
                                        . 24
                                                   *TOTALS*
                                       .08
    PEAK FLOW (cms)=
                            .19
                                                     .250 (iii)
    TIME TO PEAK (hrs)=
                            1.00
                                       1.07
                                                    1.000
                       76.44
77.24
    RUNOFF VOLUME
                 (mm) =
                                       46.34
                                                   61.388
    TOTAL RAINFALL (mm)=
                                      77.24
                                                   77.237
    RUNOFF COEFFICIENT =
                                      .60
                                                    .795
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
         CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
         THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
TOTAL RAINFALL (mm)= 77.237
RUNOFF COEFFICIENT = .225
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
050:0006-----
*#-----|
*#
*#
      Total internal area draining onto agricultural area to the east
*#-----|
           ) | ID: NHYD
| ADD HYD (IntUcE
                             QPEAK TPEAK R.V.
                                          DWF
                       AREA
                            (cms) (hrs) (mm)
______
                        (ha)
                                          (cms)
           ID1 01:200
                                 1.37 17.39
                        .14
                             .007
                                          .000
           +ID2 02:201
                        .64 .250 1.00 61.39
                                         .000
                         .55 .048 1.10 17.40
           +ID3 03:203
            ______
            SUM 05:IntUcE 1.33
                             .281
                                  1.00 38.56
                                           .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
050:0007-----
*#
*#
        Proposed industrial lots draining to Rear Lot Ditch
*#-----|
DESIGN STANDHYD
                  (ha) = 8.82
              Area
| 06:202 DT= 1.00 |
              Total Imp(%)= 90.00 Dir. Conn.(%)=
                                     80.00
                 IMPERVIOUS
                         PERVIOUS (i)
  Surface Area
                7.94
          (ha)=
                           .88
  Dep. Storage
           (mm)=
                   .80
                          1.50
  Average Slope
            (%)=
                2..
242.49
013
                  2.00
                          2.00
  Length
             (m) =
                         40.00
  Mannings n
                          .250
  Max.eff.Inten.(mm/hr)= 214.69
                         125.13
         over (min)
                  3.00
                          9.00
```

```
2.60 (ii) 9.05 (ii)
Storage Coeff. (min)=
                             3.00
Unit Hyd. Tpeak (min)=
                                           9.00
                                            .13
Unit Hyd. peak (cms)=
                              .41
                                                         *TOTALS*
PEAK FLOW (cms)= 3.67
TIME TO PEAK (hrs)= 1.02
RUNOFF VOLUME (mm)= 76.44
                                         1.18
                                            .21
                                                           3.766 (iii)
                                                           1.017
                                           28.75
                                                          66.900
TOTAL RAINFALL (mm) = 77.24
RUNOFF COEFFICIENT = .99
                                           77.24
                                                          77.237
                                            .37
                                                           .866
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
050:0008-----
*#------
*#
*#
   External agricultural area draining onsite and entering Rear Lot Ditch
*#-----|
DESIGN NASHYD | Area (ha)= .73 Curve Number (CN)=70.00
| 07:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
------ U.H. Tp(hrs)= .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)= .084 (i)
TIME TO PEAK (hrs)= 1.250
           (mm) = 31.074
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)= 77.237
  RUNOFF COEFFICIENT =
                 .402
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0009-----
*#-----|
    Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#-----|
```

```
DWF
                           (cms)
                           .000
       +ID2 07:104
             .73 .084 1.25 31.07 .000
       ______
       SUM 08:RLswl
               9.55 3.795 1.02 64.16
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0010-----*# *# Proposed industrial lots draining to East Road Ditch within catchment, and new internal roadway *#------DESIGN STANDHYD | Area (ha)= 4.92 | 01:204 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= Surface Area (ha)= 4.43

Dep. Storage (mm)= .80

Average Slope (%)= 2.00

Length (m)= 181.11

013 IMPERVIOUS PERVIOUS (i) .49 1.50 2.00 40.00 Mannings n .013 .250 Max.eff.Inten.(mm/hr)= 214.69 125.13 over (min) 2.00 9.00 2.00 9.00
Unit Hyd. Tpeak (min)= 2.00 9.00
Unit Hyd. peak (cms)= 2.00 9.00
Unit Hyd. peak (cms)= .53 *TOTALS* .12 1.18

2.213 (iii)

1.000

66.900

77.237

.866

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above)

(cms)= 2.17

1.00

28.75

77.24

.37

(hrs)=

RUNOFF VOLUME (mm)= 76.44

TOTAL RAINFALL (mm)= 77.24

RUNOFF COEFFICIENT = .99

PEAK FLOW

TIME TO PEAK

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
050:0011-----
*#------|
         Rooftop infiltration lumped together and sized for 25mm
*#
*#
       runoff volume from an assumed 0.15ha rooftop area per lot (7 lots)
*#------|
ADD HYD (Roof
             ) | ID: NHYD
                                 QPEAK TPEAK R.V.
                           AREA
                                                 DWF
-----
                                 (cms) (hrs) (mm)
                           (ha)
                                                 (cms)
                           4.92 2.213 1.00 66.90 .000
             ID1 01:204
                       8.82 3.766 1.02 66.90 .000
             +ID2 06:202
             ______
             SUM 02:Roof 13.74 5.921 1.00 66.90 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
______
050:0012-----
ROUTE RESERVOIR
                Requested routing time step = 1.0 min.
IN>02:(Roof )
OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======
-----
                OUTFLOW
                       STORAGE | OUTFLOW STORAGE
                 (cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .000 .2625E-01
                   AREA QPEAK TPEAK
(ha) (cms) (hrs)
13.74 5.921 1.000
   ROUTING RESULTS
                                         R.V.
                                         (mm)
   INFLOW >02: (Roof )
                                        66.900
   OUTFLOW<04: (R-inf )
                    .39
                                 .583
                          .000
                                        14.319
  OVERFLOW<10: (infO ) 13.35
                           5.911
                                        66,900
                                 1.017
            TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                         5
            CUMULATIVE TIME OF OVERFLOWS (hours)= 3.53
            PERCENTAGE OF TIME OVERFLOWING
                                 (%)=
                                        .20
                 FLOW REDUCTION [Qout/Qin](%)=
                                        .000
            TIME SHIFT OF PEAK FLOW (min)= -25.00
            MAXIMUM STORAGE USED
                              (ha.m.)=.2625E-01
```

```
*** WARNING: Outflow volume is less than inflow volume.
050:0013-----
*#------|
*#
        Proposed SWM facility catchment (infiltration basin)
*#
*#------|
----- U.H. Tp(hrs)= .350
  Unit Hyd Qpeak (cms)= .178
  PEAK FLOW (cms)= .090 (i)
TIME TO PEAK (hrs)= 1.483
              21.455
  RUNOFF VOLUME
           (mm)=
  TOTAL RAINFALL
           (mm) = 77.237
  RUNOFF COEFFICIENT =
                .278
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0014-----
*#-----|
*#
*#
             All flows entering SWM facility
*#------|
| ADD HYD (ToSWM ) | ID: NHYD AREA QPEAK TPEAK R.V.
                                       DWF
-----
                      (ha)
                          (cms) (hrs) (mm)
                                       (cms)
                      13.35 5.911 1.02 66.90
           ID1 10:inf0
                                       .000
                      .73 .084 1.25 31.07 .000
          +ID2 07:104
                   1.63 .090 1.48 21.46
          +ID3 09:205
                                       .000
           ______
                      15.71 5.952 1.02 60.52
           SUM 06:ToSWM
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
```

```
050:0015-----
*#
*#
                 Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR
                  Requested routing time step = 1.0 min.
 IN>06:(ToSWM )
OUT<07:(SWMinf)
                  ====== OUTLFOW STORAGE TABLE ======
                  OUTFLOW STORAGE | OUTFLOW
                                             STORAGE
                          (ha.m.)
                                     (cms)
                                            (ha.m.)
                    (cms)
                                     .044 .7033E+00
                     .000 .0000E+00
                     .044 .6530E-01
                                      .000 .0000E+00
                      AREA
   ROUTING RESULTS
                              QPEAK
                                     TPEAK
                                               R.V.
                       (ha)
                              (cms)
                                     (hrs)
                                               (mm)
                   15.71
12.28
   INFLOW >06: (ToSWM )
                              5.952
                                      1.017
                                             60.519
                                      1.017
.850
                              .044
   OUTFLOW<07: (SWMinf)
                       12.28
                                             60.518
  OVERFLOW<08: (OVF-I )
                       3.43
                              1.262
                                      1.433
                                             60.519
              TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                               2
              CUMULATIVE TIME OF OVERFLOWS (hours)=
                                           1.63
              PERCENTAGE OF TIME OVERFLOWING (%)=
                                              1.68
                        REDUCTION [Qout/Qin](%)=
              PEAK FLOW
              TIME SHIFT OF PEAK FLOW
                                      (min)=
              MAXIMUM STORAGE USED
                                    (ha.m.)=.7033E+00
*#-----|
*#
*#
                Active Storage Portion of SWM facility
*#------|
ROUTE RESERVOIR
                  Requested routing time step = 1.0 min.
 IN>08:(OVF-I )
OUT<01:(SWMout)
                  ====== OUTLFOW STORAGE TABLE =======
                           STORAGE | OUTFLOW
                  OUTFLOW
                                             STORAGE
                    (cms) (ha.m.)
                                    (cms) (ha.m.)
                                  1.479 .2400E+00
4.101 .4070E+00
                     .000 .0000E+00
                     .202 .7850E-01
                                     .000 .0000E+00
                     .689 .1586E+00
```

```
R.V.
                                     (mm)
                                    60.519
                                    60.518
                                     .000
           TOTAL NUMBER OF SIMULATED OVERFLOWS =
           CUMULATIVE TIME OF OVERFLOWS (hours)=
                                      .00
           PERCENTAGE OF TIME OVERFLOWING (%)=
                                     .00
           PEAK FLOW REDUCTION [Qout/Qin](%)= 25.553
           TIME SHIFT OF PEAK FLOW (min)= 38.00
           MAXIMUM STORAGE USED (ha.m.)=.9830E-01
-----
050:0017-----
*#------
*#
*#
   West Road Ditch, conveying external drainage from the west around the
*#
            proposed SWM facility to Outlet Channel
*#------
DESIGN NASHYD | Area (ha)= 1.22 Curve Number (CN)=50.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
------ U.H. Tp(hrs)= .810
  Unit Hyd Qpeak (cms)= .058
  PEAK FLOW (cms)= .031 (i)
TIME TO PEAK (hrs)= 2.067
            (mm) = 17.396
  RUNOFF VOLUME
   TOTAL RAINFALL (mm)= 77.237
   RUNOFF COEFFICIENT =
                  .225
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0018-----
*#-----|
     Grassed area south of SWM facility draining offsite to the south
*#-----|
```

```
----- U.H. Tp(hrs)= .070
  Unit Hyd Qpeak (cms)= .076
         (cms) = .013 (i)
  PEAK FLOW
         (hrs)=
  TIME TO PEAK
             1.100
  RUNOFF VOLUME
          (mm) =
             17.395
          (mm) =
  TOTAL RAINFALL
              77.237
  RUNOFF COEFFICIENT =
             . 225
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0019-----
*#-----|
*#
        Total Flows to the east from internal catchments
*#
*#-----|
| ADD HYD (IntE ) | ID: NHYD
                    AREA
                        QPEAK
                            TPEAK R.V.
                                    DWF
_____
                    (ha)
                       (cms) (hrs) (mm)
                                   (cms)
                    1.33
          ID1 05:IntUcE
                        .281 1.00 38.56
                                   .000
         +ID2 01:SWMout 3.43 .322 2.07 60.52 .000
                    1.22 .031 2.07 17.40
         +ID3 02:206
                                    .000
          ______
          SUM 07:IntE
                    5.98 .374 2.05 46.83
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
______
050:0020-----
*#-----|
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
*#------
*# External industrial catchment and part of Hwy 401, draining south across
          Cedar Creek Road and entering BPSS
```

```
*#
*#------|
                     Area (ha)= 55.94
CALIB STANDHYD
| 03:100 DT= 1.00 |
                    Total Imp(\%) = 80.00 Dir. Conn.(\%) = 50.00
------
                          IMPERVIOUS
                                       PERVIOUS (i)
                           44.75
    Surface Area
                  (ha)=
                                        11.19
    Dep. Storage (mm)= 2.00
Average Slope (%)= 1.60
Length (m)= 1500.00
                                         5.00
                                         2.00
                                         30.00
    Mannings n
                             .020
                                          .250
    Max.eff.Inten.(mm/hr)= 158.05 194.43

over (min) 12.00 17.00

Storage Coeff. (min)= 12.15 (ii) 16.70 (ii)
    Unit Hyd. Tpeak (min)=
                            12.00
                                        17.00
    Unit Hyd. peak (cms)=
                               .09
                                          .07
                                                     *TOTALS*
                            8.29
                                        3.74
    PEAK FLOW
                (cms)=
                                                      11.442 (iii)
                 (hrs)=
    TIME TO PEAK
                             1.18
                                         1.32
                                                      1.233
                        75.23
77.24
    RUNOFF VOLUME
                  (mm) =
                                         42.76
                                                     58.997
                                        77.24
    TOTAL RAINFALL (mm)=
                                                     77.237
    RUNOFF COEFFICIENT =
                                        .55
                                                      .764
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
```

- $CN^* = 64.0$ Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
*#-----|
*# External catchment containing a portion of Cedar Creek Road, a portion
*# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
*#-----|
| DESIGN STANDHYD |
                Area (ha)= 14.55
\mid 07:101 DT= 1.00 \mid Total Imp(%)= 60.00 Dir. Conn.(%)= 48.00
                     IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)=
Dep. Storage (mm)=
                       8.73
                                 5.82
                        .80
                                 1.50
                      2.30
   Average Slope (%)=
                                 2.30
                    2.30
311.45
   Length
                (m) =
                                40.00
```

Mannings n	=	.013	.250	
Max.eff.Inten.(mm/hr)=	214.69	54.05	
over	(min)	3.00	12.00	
Storage Coeff.	(min)=	2.90 (ii)	11.55 (ii)	
Unit Hyd. Tpeak	(min)=	3.00	12.00	
Unit Hyd. peak	(cms) =	.38	.10	
				TOTALS
PEAK FLOW	(cms) =	3.56	.57	3.739 (iii)
TIME TO PEAK	(hrs)=	1.02	1.25	1.017
RUNOFF VOLUME	(mm) =	76.44	21.32	47.778
TOTAL RAINFALL	(mm) =	77.24	77.24	77.237
RUNOFF COEFFICI	ENT =	.99	.28	.619

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*# Total area *#	draining offsite to	east onto a	agricultu	ral area	to the	east
ADD HYD (UCtoE) ID: NHYD	AREA	-	TPEAK		DWF
	ID1 05:IntUcE	1.33	(cms) .281		38.56	
	+ID2 03:100	55.94	11.442	1.23	59.00	.000
	+ID3 07:101	14.55	3.739	1.02	47.78	.000
	SUM 09:UCtoE	71.82	13.561	1.20	56.35	.000
NOTE: PEAK FLO	OWS DO NOT INCLUDE BA	SEELOWS TE	ΔΝΥ			

*#-----|

```
*#
    Large external catchment west of site containing industrial property,
*#
  draining into private SWM feature and then into West Road Ditch, routing
*#
             around SWM facility and entering Outlet Channel
*#
*#-----|
| DESIGN STANDHYD |
                             (ha) = 12.64
                    Area
| 04:102 DT= 1.00 |
                    Total Imp(%)= 80.00 Dir. Conn.(%)=
                                                          50.00
                          IMPERVIOUS
                                      PERVIOUS (i)
    Surface Area (ha)=
                             10.11
                                         2.53
                  (mm) =
                             .80
    Dep. Storage
                                         1.50
    Average Slope
                  (%)=
                             3.10
                                         3.10
    Length
                    (m) =
                            290.29
                                        40.00
    Mannings n
                            .013
                                         .250
    Max.eff.Inten.(mm/hr)=
                          214.69
                                      188.85
              over (min)
                                        7.00
                            3.00
                           2.54 (ii) 7.34 (ii) 3.00 7.00
    Storage Coeff. (min)=
    Unit Hyd. Tpeak (min)=
    Unit Hyd. peak (cms)=
                             .42
                                         .16
                                                    *TOTALS*
    PEAK FLOW
                  (cms) =
                             3.30
                                         .93
                                                     3.858 (iii)
    TIME TO PEAK
                  (hrs)=
                                        1.13
                            1.02
                                                     1.017
    RUNOFF VOLUME
                  (mm) =
                           76.44
                                       32.95
                                                    54,694
                           77.24
                                       77.24
    TOTAL RAINFALL
                   (mm) =
                                                    77.237
    RUNOFF COEFFICIENT =
                             .99
                                         .43
                                                      .708
      (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
         CN^* = 50.0 Ia = Dep. Storage (Above)
     (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
         THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

050:0024	
*# .	
*#	ı
 *#	Infiltration in External SWM Feature
*#	
*#	
ROUTE RESERVOIR IN>04:(102)	- Requested routing time step = 1.0 min.
OUT<05:(xSWinf)	======= OUTLFOW STORAGE TABLE ======
	- OUTFLOW STORAGE OUTFLOW STORAGE
	(cms) (ha.m.) cms) (ha.m.)
	.000 .0000E+00 .018 .3759E+00

```
.018 .4380E-01 | .000 .0000E+00
   ROUTING RESULTS
                                        TPEAK
                                                  R.V.
                         AREA
                                QPEAK
    -----
                         (ha)
                                 (cms)
                                        (hrs)
                                                  (mm)
   INFLOW >04: (102 )
                                        1.017
                        12.64
                                 3.858
                                                 54.694
   OUTFLOW<05: (xSWinf)
                        7.19
                                 .018
                                         .817
                                                 54.693
   OVERFLOW<06: (OVF-xI)
                         5.45
                                 2.263
                                         1.200
                                                 54.694
               TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                                   2
               CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                1.97
               PERCENTAGE OF TIME OVERFLOWING (%)=
                                                 1.44
               PEAK
                          REDUCTION [Qout/Qin](%)=
                                   (min) = -12.00
               TIME SHIFT OF PEAK FLOW
               MAXIMUM STORAGE USED
                                      (ha.m.)=.3759E+00
050:0025-----
*#-----|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
*#
                  SWM facility and entering Outlet Channel
*#
*#-----|
______
| DESIGN STANDHYD |
                          (ha) = 4.52
                  Area
                  Total Imp(%)= 80.00 Dir. Conn.(%)=
07:103 DT= 1.00
                                                     50.00
                        IMPERVIOUS
                                   PERVIOUS (i)
                                      .90
   Surface Area
                 (ha)=
                           3.62
   Dep. Storage
                 (mm) =
                           .80
                                     1.50
   Average Slope
                  (%)=
                          5.30
                                     5.30
                  (m) =
                         173.59
   Length
                                     40.00
   Mannings n
                                      .250
                          .013
                                    195.13
   Max.eff.Inten.(mm/hr)=
                         214.69
            over (min)
                           2.00
                                     6.00
   Storage Coeff. (min)=
                           1.59 (ii)
                                     5.62 (ii)
   Unit Hyd. Tpeak (min)=
                           2.00
                                     6.00
   Unit Hyd. peak (cms)=
                           .64
                                     . 20
                                               *TOTALS*
   PEAK FLOW
                 (cms) =
                           1.30
                                     .36
                                                 1.513 (iii)
    TIME TO PEAK
                 (hrs)=
                          1.00
                                     1.10
                                                 1.000
    RUNOFF VOLUME
                 (mm) =
                          76.44
                                     32.95
                                                54.694
                 (mm) =
                         77.24
                                    77.24
                                                77.237
    TOTAL RAINFALL
    RUNOFF COEFFICIENT =
                          .99
                                     .43
                                                 .708
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
______
050:0026-----
*#------|
*#
       Total Flows through West Road Ditch
*#------|
DWF
                 (ha) (cms) (hrs) (mm)
5.45 2.263 1.20 54.69
                              (cms)
        ID1 06:0VF-xI
                             .000
                 4.52 1.513 1.00 54.69
        +ID2 07:103
                              .000
              1.22 .031 2.07 17.40 .000
        +ID3 02:206
        ______
        SUM 08:WRswl
              11.19 2.977 1.20 50.63
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
050:0027-----
*#------
Unit Hyd Qpeak (cms)= .051
        (cms) = .027 (i)
  PEAK FLOW
  TIME TO PEAK
        (hrs)=
           2.117
  RUNOFF VOLUME
        (mm) =
           17.396
  TOTAL RAINFALL (mm)=
            77.237
  RUNOFF COEFFICIENT =
           .225
```

-								
‡								
#		Total	Flows through	Outlet Cha	annel			
# #		1						
ADD HYD	(OutChan)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)		
		ID1	01:SWMout		.322			
		+ID2	08:WRswl	11.19	2.977	1.20	50.63	.000
		+ID3	05:208	1.13	.027	2.12	17.40	.000
		===:		=======	 2.982	====== 1 20	50.39	 .000
· -		IS DO I	03:OutChan		ANY.			
 - 50:0029 - #		IS DO I	NOT INCLUDE BAS	SEFLOWS IF	ANY.			
 - 50:0029 - # # #		IS DO I	NOT INCLUDE BAS	SEFLOWS IF	ANY.	 Cedar C	 (reek)	
		Total	NOT INCLUDE BAS	SEFLOWS IF	ANY.	 Cedar C	reek)	
		Total	NOT INCLUDE BAS	SEFLOWS IFeast (event AREA (ha)	ANY. cually to QPEAK (cms)	Cedar C	reek)	 DWF (cms)
	(TotE	Total	NOT INCLUDE BAS	SEFLOWS IFeast (event AREA (ha)	ANY.	Cedar C	reek)	 DWF (cms)
	(TotE	Total JD1	NOT INCLUDE BAS	SEFLOWS IF east (event AREA (ha) 3.43	ANY. cually to QPEAK (cms)	Cedar C TPEAK (hrs) 2.07	reek)	DWF (cms)
	(TotE	Total John Jo	NOT INCLUDE BASE	SEFLOWS IF east (event AREA (ha) 3.43 11.19	ANY. Cually to QPEAK (cms) .322	TPEAK (hrs) 2.07	R.V. (mm) 60.52	DWF (cms)

##	
Total Flows from the Site Total Flows from the Site Flows from the Site Total Flows from the Site Flows from the Si	
# Total Flows from the Site # #	
# Total Flows from the Site ## ## ADD HYD (AllFlo) ID: NHYD AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) (ID1 04:TotE 86.44 16.538 1.20 55.77 +ID2 10:207 .14 .013 1.10 17.40 ===================================	
######################################	
ADD HYD (AllFlo) ID: NHYD AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) (ID1 04:TotE 86.44 16.538 1.20 55.77 +ID2 10:207 .14 .013 1.10 17.40 ===================================	
ADD HYD (AllFlo) ID: NHYD	
ID1 04:TotE 86.44 16.538 1.20 55.77	
(ha) (cms) (hrs) (mm) (ID1 04:TotE 86.44 16.538 1.20 55.77 +ID2 10:207 .14 .013 1.10 17.40	DWF
ID1 04:TotE 86.44 16.538 1.20 55.77 +ID2 10:207 .14 .013 1.10 17.40 ===================================	
+ID2 10:207 .14 .013 1.10 17.40 ===================================	.000
SUM 06:AllFlo 86.58 16.548 1.20 55.71 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.	
SUM 06:AllFlo 86.58 16.548 1.20 55.71 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.	.000
SUM 06:AllFlo 86.58 16.548 1.20 55.71 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 50:0031	
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY	
	.000
: :0:0002	
- 	
- 50:0002 -	
- 50:0002	
-	
-	
- 	
-	
50:0002	
-	
-	
50:0002	
-	
-	
50:0002	
-	
-	
50:0002	
- ** FND OF BUN	
** END OF RUN : 99	

```
Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\
START
                 Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\
   TZERO =
           .00 hrs on
           2 (output = METRIC)
   METOUT=
   NRUN = 100
   NSTORM=
        # 1=Kit100yr.3hr
100:0002-----
*#*********************************
   Project Name: [2509 Cedar Creek Road SWM - Ayr, ON] Project #: [161414214]
*#
   Date
            : 01/25/2024
            : [Amy Kyle, Water Resources Specialist]
*# Modeller
*#
  Company
            : Stantec Consulting Ltd. (Waterloo)
*# License #
           : 4730904
*#
*# This hydrologic analysis prepared to provide pond sizing
*# for the 2509 Cedar Creek Road SWM Facility
*#
  The storm events modelled are:
   25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)
   and the Regional Event
*#**********************************
  ______
100:0002-----
                   Filename: 100-yr, 3hr Chicago Storm - Kitchener ID
READ STORM
                   Comments: 100-yr, 3hr Chicago Storm - Kitchener ID
| Ptotal= 87.07 mm|
           TIME
                 RAIN |
                         TIME
                               RAIN
                                      TIME
                                                    TIME
                                                           RAIN
                                             RAIN |
                mm/hr
                         hrs
                              mm/hr |
                                       hrs
                                            mm/hr
                                                     hrs
                                                          mm/hr
            hrs
            .08
                4.087
                          .83 50.502
                                      1.58 20.973
                                                    2.33
                                                          6.373
            .17
                 4.733
                          .92 113.675
                                      1.67 17.458
                                                    2.42
                                                          5.820
            .25
                 5.569 l
                         1.00 239.354
                                      1.75 14.796
                                                    2.50
                                                          5.342
            .33
                 6.681 |
                         1.08 141.249
                                      1.83 12.729
                                                    2.58
                                                          4.926
            .42
                 8.210
                         1.17 86.233
                                      1.92 11.089
                                                    2.67
                                                          4.561
            .50 10.405
                         1.25 58.548
                                      2.00 9.765
                                                    2.75
                                                          4.239
            .58 13.734
                         1.33 42.595
                                      2.08 8.679
                                                    2.83
                                                          3.953
            .67 19.179
                         1.42 32.533
                                      2.17
                                            7.777
                                                    2.92
                                                          3.698
            .75 29.096
                         1.50 25.760
                                      2.25 7.018
                                                    3.00
                                                          3.469
```

```
100:0003-----
*#-----|
*# Proposed Drainage Conditions (Internal Areas)
*#------
*#
*#
   Small portion of West Road Ditch draining offsite to the east through
*#
                By-Pass Storm Sewer(BPSS)
*#------|
DESIGN NASHYD | Area (ha)= .14 Curve Number (CN)=50.00
            Ia
| 01:200 DT= 1.00 |
                  (mm) = 1.500 \# of Linear Res.(N) = 3.00
----- U.H. Tp(hrs)=
                     .260
  Unit Hyd Qpeak (cms)=
               .021
  PEAK FLOW
          (cms)=
                .009 (i)
               1.367
           (hrs)=
  TIME TO PEAK
           (mm) =
  RUNOFF VOLUME
                21.559
  TOTAL RAINFALL
           (mm) =
                87.067
  RUNOFF COEFFICIENT =
                . 248
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0004-----
*#------|
 Proposed developed catchment draining offsite to the east through BPSS
*#
*#-----|
------
DESIGN STANDHYD
            Area (ha)=
                       .64
| 02:201 DT= 1.00 |
            Total Imp(%)= 90.00 Dir. Conn.(%)=
                                    50.00
                IMPERVIOUS
                        PERVIOUS (i)
  Surface Area
            (ha)=
                  .58
                          .06
                   .80
  Dep. Storage
            (mm) =
                          1.50
                2.00
  Average Slope
            (%)=
                         2.00
  Length
            (m) =
                  65.32
                         40.00
  Mannings n
                 .013
                          .250
  Max.eff.Inten.(mm/hr)=
               239.35
                        761.63
```

```
1.00 4.00
1.13 (ii) 4.27 (ii)
           over (min)
Storage Coeff. (min)=
Unit Hyd. Tpeak (min)=
                            1.00
                                        4.00
                                        .27
Unit Hyd. peak (cms)=
                            1.00
                                                     *TOTALS*
                                        .10
PEAK FLOW
              (cms)=
                          .21
1.00
                                                       .295 (iii)
                                      1.05
              (hrs)=
TIME TO PEAK
                                                      1.000
TOTAL RAINFALL (mm)= 86.27
RUNOFF COEFFICIENT = .99
                                      54.73
                                                      70.497
                                        87.07
                                                      87.067
                                         .63
                                                       .810
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
100:0005-----
*#-----|
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#-----|
.
----- U.H. Tp(hrs)= .080
  Unit Hyd Qpeak (cms)= .263
  PEAK FLOW
       (cms) = .060 (i)
        (hrs)= 1.100
  TIME TO PEAK
  RUNOFF VOLUME
             21.562
         ( mm ) =
  TOTAL RAINFALL (mm)= 87.067
  RUNOFF COEFFICIENT =
             . 248
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0006-----
*#-----|
*#
     Total internal area draining onto agricultural area to the east
*#------
```

```
ADD HYD (Intuce ) | ID: NHYD AREA QPEAK TPEAK R.V.
                                                              DWF
_____
                                         (cms) (hrs) (mm)
                                   (ha)
                                                              (cms)
                                   .14
                 ID1 01:200
                                          .009 1.37 21.56
                                                              .000
                +ID2 02:201
                              .64 .295 1.00 70.50 .000
                +ID3 03:203
                                    .55
                                          .060 1.10 21.56
                                                              .000
                 SUM 05:IntUcE 1.33 .334 1.00 45.11
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0007-----
*#
*#
            Proposed industrial lots draining to Rear Lot Ditch
*#
*#------|
DESIGN STANDHYD | Area (ha)= 8.82
| 06:202 \quad DT= 1.00 \quad Total Imp(%)= 90.00 \quad Dir. Conn.(%)= 80.00
                         IMPERVIOUS PERVIOUS (i)
   Surface Area (ha)= 7.94

Dep. Storage (mm)= .80

Average Slope (%)= 2.00

Length (m)= 242.49

Mannings n = .013
                                       .88
                                      1.50
                                      2.00
                                     40.00
                          .013
                                       .250
    Max.eff.Inten.(mm/hr)= 239.35
                                    154.12
    over (min) 2.00 8.00

Storage Coeff. (min)= 2.49 (ii) 8.43 (ii)

Unit Hyd. Tpeak (min)= 2.00 8.00
```

.14

.26

1.17

87.07

.40

34.93

TOTALS

1.000

.873

75.999

87.067

4.348 (iii)

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above)

.99

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

Unit Hya. PC

PEAK FLOW (cms)= 4.24

TIME TO PEAK (hrs)= 1.00

"MOEF VOLUME (mm)= 86.27

(mm)= 87.07

99

RUNOFF COEFFICIENT =

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
100:0008-----
*#------|
*#
   External agricultural area draining onsite and entering Rear Lot Ditch
*#-----|
DESIGN NASHYD | Area (ha)= .73 Curve Number (CN)=70.00
| 07:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)=
                       .190
  Unit Hyd Qpeak (cms)= .147
  PEAK FLOW (cms)= .103 (i)
TIME TO PEAK (hrs)= 1.250
            (mm) =
  RUNOFF VOLUME
                37.658
  TOTAL RAINFALL (mm)= 87.067
  RUNOFF COEFFICIENT = .433
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0009-----
*#------
*#
    Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#------
ADD HYD (RLswl ) | ID: NHYD
                        AREA
                             OPEAK TPEAK R.V.
                                            DWF
                        (ha) (cms) (hrs) (mm) (cms)
8.82 4.348 1.00 76.00 .000
______
            ID1 06:202
           +ID2 07:104
                         .73
                             .103 1.25 37.66
                                            .000
            ______
            SUM 08:RLswl
                        9.55 4.377 1.00 73.07
                                            .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
```

- -

```
- -
*#
   Proposed industrial lots draining to East Road Ditch within catchment,
*#
*#
                      and new internal roadway
*#
*#-----|
-----
| DESIGN STANDHYD |
                  Area (ha) = 4.92
| 01:204 DT= 1.00 |
                 Total Imp(%)= 90.00 Dir. Conn.(%)= 80.00
                       IMPERVIOUS PERVIOUS (i)
   Surface Area
               (ha)=
                       4.43
                                     .49
                 (mm)= .80
(%)= 2.00
(m)= 181.11
   Dep. Storage
Average Slope
                                    1.50
                (%)=
   Average Slope
                                    2.00
   Length
                                   40.00
   Mannings n
                         .013
                                     .250
   Max.eff.Inten.(mm/hr)= 239.35 154.12

over (min) 2.00 8.00

Storage Coeff. (min)= 2.09 (ii) 8.03 (ii)
   Unit Hyd. Tpeak (min)=
                         2.00
                                    8.00
   Unit Hyd. peak (cms)=
                                    .14
                          .54
                                              *TOTALS*
   PEAK FLOW (cms)=
                                   .15
                        2.44
                                                2.502 (iii)
   TOTAL RAINFALL (mm)= 86.27
RUNOFF COEFFICIENT = .99
   TIME TO PEAK (hrs)=
                         1.00
                                    1.17
                                               1.000
                                   34.93
                                              75.999
                                  87.07
                                              87.067
                                    .40
                                               .873
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
    (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0011-----
*#------
*#
           Rooftop infiltration lumped together and sized for 25mm
       runoff volume from an assumed 0.15ha rooftop area per lot (7 lots)
*#
*#-----|
```

AREA

(ha) 4.92

QPEAK TPEAK

2.502 1.00 76.00

R.V.

(cms) (hrs) (mm) (cms)

DWF

.000

| ADD HYD (Roof

) | ID: NHYD

ID1 01:204

```
______
           SUM 02:Roof
                    13.74 6.850 1.00 76.00 .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0012-----
ROUTE RESERVOIR
              Requested routing time step = 1.0 min.
IN>02:(Roof )
OUT<04:(R-inf) ======= OUTLFOW STORAGE TABLE =======
             OUTFLOW STORAGE | OUTFLOW STORAGE
               (cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | .000 .2625E-01
  TOTAL NUMBER OF SIMULATED OVERFLOWS =
          CUMULATIVE TIME OF OVERFLOWS (hours)= 3.52
          PERCENTAGE OF TIME OVERFLOWING (%)=
                                  .20
          PEAK FLOW REDUCTION [Qout/Qin](%)= .000
          TIME SHIFT OF PEAK FLOW (min)= -27.00
          MAXIMUM STORAGE USED
                          (ha.m.)=.2625E-01
   *** WARNING: Outflow volume is less than inflow volume.
100:0013-----
*#------
*#
        Proposed SWM facility catchment (infiltration basin)
*#-----|
----- U.H. Tp(hrs)= .350
```

+ID2 06:202 8.82 4.348 1.00 76.00 .000

```
(cms)=
                 .112 (i)
1.483
   PEAK FLOW
  TIME TO PEAK (hrs)=
   RUNOFF VOLUME
            (mm) =
                  26.415
             (mm) =
   TOTAL RAINFALL
                 87.067
   RUNOFF COEFFICIENT =
                  .303
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0014-----
*#-----|
*#
               All flows entering SWM facility
*#------|
            ) | ID: NHYD
| ADD HYD (ToSWM
                         AREA
                              QPEAK TPEAK R.V.
                                              DWF
_____
            (ha) (cms) (hrs) (mm)
ID1 10:inf0 13.39 6.755 1.02 76.00
                                             (cms)
                                             .000
                         .73 .103 1.25 37.66 .000
            +ID2 07:104
            +ID3 09:205
                      1.63 .112 1.48 26.41
                                             .000
             ______
                      15.75 6.807 1.02 69.09
            SUM 06:ToSWM
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0015-----
*#
*#
              Infiltration Portion of SWM facility
*#-----|
ROUTE RESERVOIR
               Requested routing time step = 1.0 min.
 IN>06:(ToSWM )
OUT<07:(SWMinf) ======= OUTLFOW STORAGE TABLE ======
               OUTFLOW STORAGE | OUTFLOW STORAGE
                           (cms) (ha.m.)
.044 .7033E+00
                (cms) (ha.m.)
                 .000 .0000E+00
```

Unit Hyd Qpeak (cms)= .178

```
.044 .6530E-01 | .000 .0000E+00
   OVERFLOW<08: (OVF-I )
               TOTAL NUMBER OF SIMULATED OVERFLOWS =
               CUMULATIVE TIME OF OVERFLOWS (hours)= 1.80
PERCENTAGE OF TIME OVERFLOWING (%)= 1.85
               PEAK FLOW REDUCTION [Qout/Qin](%)= .646
               TIME SHIFT OF PEAK FLOW (min)= -11.00
               MAXIMUM STORAGE USED
                                       (ha.m.)=.7033E+00
100:0016-----
*#-----|
*#
                 Active Storage Portion of SWM facility
*#------|
ROUTE RESERVOIR
                    Requested routing time step = 1.0 min.
 IN>08:(OVF-I )
OUT<01:(SWMout) ======= OUTLFOW STORAGE TABLE =======
                    OUTFLOW STORAGE | OUTFLOW STORAGE (cms) (ha.m.) | (cms) (ha.m.)
                       (cms) (ha.m.) (cms) (ha.m.)

.000 .0000E+00 | 1.479 .2400E+00

.202 .7850E-01 | 4.101 .4070E+00
                                         .000 .0000E+00
                       .689 .1586E+00
                       AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) 4.99 2.319 1.283 69.093
    ROUTING RESULTS
    -----
    INFLOW >08: (OVF-I )
   OUTFLOW<01: (SWMout) 4.99 .631 1.783
OVERFLOW<02: (OVF ) .00 .000 .000
                                         1.783
                                                 69.093
                                                   .000
                                                  0
.00
               TOTAL NUMBER OF SIMULATED OVERFLOWS =
               CUMULATIVE TIME OF OVERFLOWS (hours)=
               PERCENTAGE OF TIME OVERFLOWING (%)=
                                                    .00
               PEAK FLOW REDUCTION [Qout/Qin](%)= 27.206
               TIME SHIFT OF PEAK FLOW (min)= 30.00
               MAXIMUM STORAGE USED (ha.m.)=.1491E+00
```

```
100:0017-----
*#------|
*#
   West Road Ditch, conveying external drainage from the west around the
*#
            proposed SWM facility to Outlet Channel
*#------|
DESIGN NASHYD
              Area (ha)= 1.22 Curve Number (CN)=50.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
.
----- U.H. Tp(hrs)=
                       .810
   Unit Hyd Qpeak (cms)=
                  .058
  PEAK FLOW (cms)= .038 (i)
TIME TO PEAK (hrs)= 2.067
   TIME TO PEAK (hrs)=
            (mm) =
   RUNOFF VOLUME
                 21.562
   TOTAL RAINFALL (mm)=
                 87.067
   RUNOFF COEFFICIENT = .248
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
      Grassed area south of SWM facility draining offsite to the south
*#------
----- U.H. Tp(hrs)= .070
   Unit Hyd Qpeak (cms)= .076
   PEAK FLOW (cms)=
                 .016 (i)
           (hrs)=
   TIME TO PEAK
                  1.100
   RUNOFF VOLUME
            (mm) =
                  21.561
   TOTAL RAINFALL (mm)=
                  87.067
   RUNOFF COEFFICIENT = .248
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
100:0019-----
*#------|
*#
        Total Flows to the east from internal catchments
*#
*#------|
         ) | ID: NHYD
ADD HYD (IntE
                         QPEAK TPEAK R.V.
                                     DWF
                    AREA
-----
                    (ha)
                        (cms) (hrs) (mm)
                                    (cms)
          ID1 05:IntUcE
                     1.33
                         .334 1.00 45.11
                                     .000
         +ID2 01:SWMout 4.99 .631 1.78 69.09
                                    .000
         +ID3 02:206
                    1.22 .038 2.07 21.56
                                     .000
          ______
                    7.54
                         .705
                             1.75 57.17
          SUM 07:IntE
                                     .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0020-----
*#-----|
*# Proposed Drainage Conditions (Including External Catchment Flows to Ditches)
*#-----|
*# External industrial catchment and part of Hwy 401, draining south across
*#
          Cedar Creek Road and entering BPSS
*#
*#-----|
______
| CALIB STANDHYD |
               (ha)=
                    55.94
           Area
50.00
              IMPERVIOUS
                     PERVIOUS (i)
  Surface Area
          (ha)=
               44.75
                      11.19
                       5.00
  Dep. Storage
          (mm) =
                2.00
              1.60
  Average Slope
           (%)=
                       2.00
  Length
           (m)=
               1500.00
                      30.00
  Mannings n
                .020
                       .250
  Max.eff.Inten.(mm/hr)=
              177.53
                      239.93
```

```
16.00
          over (min)
                           12.00
Storage Coeff. (min)=
                           11.60 (ii)
                                       15.78 (ii)
Unit Hyd. Tpeak (min)=
                           12.00
                                        16.00
Unit Hyd. peak (cms)=
                           .10
                                        .07
                                                    *TOTALS*
PEAK FLOW
               (cms) =
                           9.52
                                        4.63
                                                     13.580 (iii)
                                        1.30
TIME TO PEAK
               (hrs)=
                           1.18
                                                     1.217
RUNOFF VOLUME
                                                     67.975
                (mm) =
                           85.06
                                        50.88
                (mm) =
                                        87.07
                                                     87.067
TOTAL RAINFALL
                           87.07
RUNOFF COEFFICIENT =
                            .98
                                        .58
                                                       .781
```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 64.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0021					
*#					
*#					ı
*# External catchme	nt contai	ning a por	tion of Cedar	Creek Road, a	portion
*# of industrial ar		•			-
*#	,	Ü	,	1,	J
*#					
·					·
DESIGN STANDHYD	Area	(ha)=	14.55		
07:101 DT= 1.00	Tota	al Imp(%)=	60.00 Dir	. Conn.(%)= 4	18.00
			JS PERVIOUS	(i)	
Surface Area	, ,				
Dep. Storage					
Average Slope	(%)=	2.30	2.30		
Length			40.00		
Mannings n	=	.013	.250		
Max.eff.Inten.(
			11.00		
Storage Coeff.				(11)	
Unit Hyd. Tpeak					
Unit Hyd. peak	(cms)=	.39	.11	*TOTAL C	v
DEAK FLOW	(a.m.a.)	4 01	72	*TOTALS*	
PEAK FLOW			.73		(111)
TIME TO PEAK RUNOFF VOLUME					
	` '		87.07		

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-							
00:0022 -							
# #	-						
•	draining offs	site to ea	st onto	agricultu	ral area	to the	east
‡ ‡	-						
· 							•
ADD HYD (UCtoE) ID: NH	HYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)		DWF (cms)
	ID1 05:Int	UcE	• •	.334	• •	• •	.000
	+ID2 03:100)	55.94	13.580	1.22	67.98	.000
	+ID3 07:101	L	14.55	4.274	1.02	55.05	.000
	========						
NOTE: PEAK FLO	SUM 09:UC1		71.82 EFLOWS IF		1.18	64.93	.000
NOTE: PEAK FLO	WS DO NOT INC	CLUDE BASE	EFLOWS IF	ANY.			
	WS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.			
	OWS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.			
	OWS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.			
	WS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.	 ustrial	 property	
	WS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.	ustrial	 property	
	OWS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.	ustrial	 property	
	OWS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.	ustrial	 property	
	OWS DO NOT INC	CLUDE BASE	FLOWS IF	ANY.	ustrial Road Dit	 property	
	OWS DO NOT INC	CLUDE BASE	te containentering (ANY.	ustrial Road Dit	property	
# Large externa # draining into # aro # DESIGN STANDHYD 04:102 DT= 1.	ows DO NOT INC	CLUDE BASE vest of sifeature ar lity and e (ha)= Imp(%)= IMPERVIOUS 10.11	EFLOWS IF te contained then in entering (12.64) 80.00 PERVI	ANY. ANY. ANY. ining indunto West IOutlet Charles Dir. Condition	ustrial Road Dit	property	
	NOT INC 	vest of sifeature arlity and e	EFLOWS IF Lite contained then in entering (12.64 80.00 PERV 2 1	ANY. ining indunto West IOutlet Cha	ustrial Road Dit	property	

Mannings n	=	.013	.250		
Max.eff.Inten.(n	nm/hr)=	239.35	228.73		
over	(min)	2.00	7.00		
Storage Coeff.	(min)=	2.43	(ii) 6.88	(ii)	
Unit Hyd. Tpeak	(min)=	2.00	7.00		
Unit Hyd. peak	(cms)=	.49	.16		
				TOTALS	:
PEAK FLOW	(cms)=	3.81	1.15	4.403	(iii)
TIME TO PEAK	(hrs)=	1.00	1.13	1.017	
RUNOFF VOLUME	(mm)=	86.27	39.75	63.011	
TOTAL RAINFALL	(mm) =	87.07	87.07	87.067	
RUNOFF COEFFICIE	ENT =	.99	.46	.724	

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

PEAK

## Infiltration in External SWM Feature ###################################	•
Infiltration in External SWM Feature ROUTE RESERVOIR Requested routing time step = 1.0 min. IN>04:(102) OUT<05:(xSWinf) ======== OUTLFOW STORAGE TABLE ======== OUTFLOW STORAGE OUTFLOW STORAGE (cms) (ha.m.) (cms) (ha.m.) .000 .0000E+00 .018 .3759E+00 .018 .4380E-01 .000 .0000E+00	•
IN>04:(102)	ı
OUTFLOW STORAGE OUTFLOW STORAGE (cms) (ha.m.) (cms) (ha.m.) .000 .0000E+00 .018 .3759E+00 .018 .4380E-01 .000 .0000E+00	
(cms) (ha.m.) (cms) (ha.m.) .000 .0000E+00 .018 .3759E+00 .018 .4380E-01 .000 .0000E+00	
.000 .0000E+00 .018 .3759E+00 .018 .4380E-01 .000 .0000E+00	
.018 .4380E-01 .000 .0000E+00	
ROUTING RESULTS AREA QPEAK TPEAK R.V.	
(ha) (cms) (hrs) (mm)	
INFLOW >04: (102) 12.64 4.403 1.017 63.011	
OUTFLOW<05: (xSWinf) 6.24 .018 .783 63.010	
OVERFLOW<06: (OVF-xI) 6.40 3.189 1.133 63.011	
TOTAL NUMBER OF SIMULATED OVERFLOWS = 2	
CUMULATIVE TIME OF OVERFLOWS (hours)= 2.02	
PERCENTAGE OF TIME OVERFLOWING (%)= 1.48	

FLOW REDUCTION [Qout/Qin](%)= .409

TIME SHIFT OF PEAK FLOW (min)= -14.00 MAXIMUM STORAGE USED (ha.m.)=.3759E+00

*#-----| *# External catchment west of the site, containing a portion of exisiting *# industrial property, draining east into West Road Ditch, routing around *# SWM facility and entering Outlet Channel *#-----| ------| DESIGN STANDHYD | Area (ha) = 4.52| 07:103 DT= 1.00 | Total Imp(%) = 80.00 Dir. Conn.(%) = 50.00 IMPERVIOUS PERVIOUS (i) Surface Area (ha)= 3.62 .90 Dep. Storage (mm) =.80 1.50 (%)= Average Slope 5.30 5.30 Length (m) =173.59 40.00 .013 Mannings n .250 247.90 Max.eff.Inten.(mm/hr)= 239.35 over (min) 2.00 5.00 1.52 (ii) 5.19 (ii) Storage Coeff. (min)= Unit Hyd. Tpeak (min)= 2.00 5.00 Unit Hyd. peak (cms)= .22 .66 *TOTALS* PEAK FLOW (cms)= 1.46 .46 1.767 (iii) 1.00 TIME TO PEAK (hrs)=1.08 1.000 39.75 RUNOFF VOLUME (mm)= 86.27 63.011 TOTAL RAINFALL (mm) =87.07 87.07 87.067 RUNOFF COEFFICIENT = .99 .46 .724 (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: $CN^* = 50.0$ Ia = Dep. Storage (Above) (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT. (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY. 100:0026-----

*# *#

*#------

```
*#
*#-----|
ADD HYD (WRswl ) | ID: NHYD
                      AREA
                           QPEAK TPEAK R.V.
                                        DWF
                      (ha) (cms) (hrs) (mm)
6.40 3.189 1.13 63.01
                                        (cms)
           ID1 06:0VF-xI
                                       .000
                      4.52 1.767 1.00 63.01
          +ID2 07:103
                                        .000
          +ID3 02:206
                 1.22 .038 2.07 21.56 .000
           ______
           SUM 08:WRswl
                   12.14 4.256 1.13 58.84
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0027-----
*#-----|
_____
----- U.H. Tp(hrs)= .850
  Unit Hyd Qpeak (cms)= .051
  PEAK FLOW (cms)= .034 (i)
  TIME TO PEAK (hrs)=
RUNOFF VOLUME (mm)=
               2.117
               21.562
  TOTAL RAINFALL (mm)=
                87.067
  RUNOFF COEFFICIENT = .248
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0028-----
*#------
*#
          Total Flows through Outlet Channel
*#-----|
| ADD HYD (OutChan ) | ID: NHYD
                      AREA QPEAK TPEAK R.V.
                                        DWF
                       (ha) (cms) (hrs) (mm) (cms)
4.99 .631 1.78 69.09 .000
                      (ha)
           ID1 01:SWMout
```

		SUM 03:OutChan	18.25	4.260	1.13	59.34	.000
NOTE:	PEAK FLOW	S DO NOT INCLUDE BA	SEFLOWS IF	ANY.			
		.					
*# *# *#		Total Flows to the	east (event	cually to	Cedar C	reek)	·
ADD HYD	(TotE) ID: NHYD		QPEAK			
		ID1 01:SWMout	(ha) 4.99	(cms) .631	(hrs) 1.78		(cms) .000
		+ID2 08:WRswl	12.14	4.256	1.13	58.84	.000
		+ID3 09:UCtoE	71.82	16.132	1.18	64.93	.000
		SUM 04:TotE		19.839			.000
 		NS DO NOT INCLUDE BA					
 *#		.					
*# *# *#			s from the				ı
		· ·					
ADD HYD	(AllFlo) ID: NHYD		QPEAK (cms)		R.V. (mm)	
		ID1 04:TotE		19.839			
		+ID2 10:207	.14	.016	1.10	21.56	.000

+ID2 08:WRswl 12.14 4.256 1.13 58.84

+ID3 05:208

1.13 .034 2.12 21.56

.000

.000

SUM 06:AllFlo 89.08 19.853 1.17 64.27 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 100:0031-----100:0002-----100:0002-----100:0002-----______ 100:0002-----** END OF RUN: 499 Project dir.: C:\SWMHYMO\CEDARC~1\202401~4\ START -----Rainfall dir.: C:\SWMHYMO\CEDARC~1\202401~4\

TZERO = .00 hrs on

METOUT= 2 (output = METRIC)

```
NRUN = 500

NSTORM = 1
```

1=hurhaz48.stm

--

500:0002-----

--

*# Date : 01/25/2024

*# Modeller : [Amy Kyle, Water Resources Specialist]
*# Company : Stantec Consulting Ltd. (Waterloo)

*# License # : 4730904

*#

*# This hydrologic analysis prepared to provide pond sizing

*# for the 2509 Cedar Creek Road SWM Facility

*# The storm events modelled are:

*# 25mm, 2, 5, 25, 50, and 100-year Chicago storms (City of Kitchener IDF)

*# and the Regional Event

--

500:0002-----

- -

| READ STORM | Filer | Ptotal= 285.00 mm | Comme

Filename: REGIONAL STORM Comments: REGIONAL STORM

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr .25 12.25 2.000 l 2.000 24.25 2.000 36.25 6.000 12.50 .50 2.000 2.000 24.50 2.000 36.50 6.000 .75 2.000 12.75 2.000 24.75 2.000 36.75 6.000 1.00 2.000 13.00 2.000 l 25.00 2.000 37.00 6.000 1.25 2.000 2.000 2,000 4.000 13.25 25.25 37.25 1.50 2.000 13.50 2.000 25.50 2.000 37.50 4.000 1.75 2.000 13.75 2.000 25.75 2.000 37.75 4.000 2.00 14.00 2.000 2.000 26.00 2.000 38.00 4.000 2.25 14.25 2.000 2.000 38.25 2.000 26.25 6.000 2.50 2.000 14.50 2.000 26.50 2.000 38.50 6.000 2.75 2.000 14.75 2.000 26.75 2.000 38.75 6.000 2.000 l 3.00 15.00 2.000 27.00 39.00 2.000 6.000 3.25 2.000 15.25 2.000 l 27.25 2.000 39.25 13.000 3.50 2.000 15.50 2.000 27.50 2.000 39.50 13.000 3.75 15.75 2.000 27.75 39.75 2.000 2.000 13.000 4.00 2.000 16.00 2.000 40.00 13.000 28.00 2.000 4.25 16.25 2.000 28.25 2.000 40.25 2.000 17.000 4.50 2.000 16.50 2.000 28.50 2.000 40.50 17.000 4.75 2.000 16.75 2.000 28.75 2.000 40.75 17.000 5.00 2.000 l 17.00 2.000 29.00 2.000 41.00 17.000

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               17.25
                                               41.25 13.000
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                       2.000
                               29.25
                                      2.000
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5.50
       2.000 l
               17.50
                       2.000
                               29.50
                                               41.50 13.000
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                       2.000
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                                               47.75 13.000
                                       3.000 |
12.00
       2.000
               24.00
                      2.000
                               36.00
                                               48.00 13.000
```

500:0003-----*#-----| *# Proposed Drainage Conditions (Internal Areas) *#------*# *# Small portion of West Road Ditch draining offsite to the east through *# By-Pass Storm Sewer(BPSS) *#------Curve Number (CN)=50.00 DESIGN NASHYD Area (ha)=.14 DT= 1.00 (mm) =1.500 # of Linear Res.(N)= 3.0001:200 Ia U.H. Tp(hrs)= .260

.021

Unit Hyd Qpeak (cms)=

```
PEAK FLOW (cms)= .014 (i)
TIME TO PEAK (hrs)= 46.050
RUNOFF VOLUME
                 (mm) = 149.528
TOTAL RAINFALL
                  (mm) = 285.000
RUNOFF COEFFICIENT =
                        .525
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

	ed catchme	ent draining	offsite to t	he east thro	 ugh BPSS
DESIGN STANDHYD 02:201 DT= 1.00	Area Tota]	(ha)= . Imp(%)= 9	.64 0.00 Dir.	Conn.(%)=	50.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area				/	
Dep. Storage	(mm)=	.80	1.50		
Average Slope					
		65.32			
Mannings n	=	.013	.250		
Max.eff.Inten.(r	nm/hr)=	53.00	256.36		
over Storage Coeff.	(min)	2.00	7.00		
Storage Coeff.	(min)=	2.07 (ii) 6.91 (i	.i)	
Unit Hyd. Tpeak	(min)=	2.00	7.00		
Unit Hyd. peak	(cms)=	.55	.16		
				*TOTALS	*
PEAK FLOW	(cms)=	.05	.05		(iii)
TIME TO PEAK	(hrs)=	45.50	46.00		
RUNOFF VOLUME					
TOTAL RAINFALL					
RUNOFF COEFFICI	ENT =	1.00	.85	.922	
(ii) TIME STEP	.0 Ia = (DT) SHOU	Dep. Storag	e (Above)		

- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

500:0005-----

```
*#-----|
*# Proposed internal grassed area and plunge pool draining offsite to the east
*#------|
DESIGN NASHYD | Area (ha)= .55 Curve Number (CN)=50.00
             Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 03:203 DT= 1.00 |
----- U.H. Tp(hrs)= .080
  Unit Hyd Qpeak (cms)= .263
  PEAK FLOW
          (cms) = .058 (i)
  TIME TO PEAK (hrs)= 46.000
  RUNOFF VOLUME (mm)= 149.530
  TOTAL RAINFALL (mm)= 285.000
  RUNOFF COEFFICIENT =
                  .525
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0006-----
*#-----|
*#
      Total internal area draining onto agricultural area to the east
*#-----|
-----
| ADD HYD (IntUcE ) | ID: NHYD
                       AREA
                             QPEAK TPEAK R.V.
                                            DWF
-----
                             (cms)
                        (ha)
                                  (hrs) (mm)
                                           (cms)
                         .14
                             .014 46.05 149.53
            ID1 01:200
                         .64 .093 46.00 262.90
           +ID2 02:201
                                           .000
                         .55 .058 46.00 149.53
           +ID3 03:203
                                           .000
            ______
            SUM 05:IntUcE 1.33 .165 46.00 204.08
                                           .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
500:0007-----
*#
        Proposed industrial lots draining to Rear Lot Ditch
*#
```

```
*#
*#------|
                  Area (ha) = 8.82
DESIGN STANDHYD
                 Total Imp(\%) = 90.00 Dir. Conn.(\%) = 80.00
| 06:202 DT= 1.00 |
                      IMPERVIOUS
                                 PERVIOUS (i)
   Surface Area
               (ha)=
                       7.94
                                    .88
                     .80
2.00
242.49
   Dep. Storage (mm)=
Average Slope (%)=
                                   1.50
                                  2.00
   Length
                 (m) =
                                  40.00
   Mannings n
                         .013
                                   .250
   Max.eff.Inten.(mm/hr)=
                     53.00
                                 92.43
                        5.00
            over (min)
                                  12.00
                        4.55 (ii) 11.83 (ii)
   Storage Coeff. (min)=
   Unit Hyd. Tpeak (min)=
                         5.00
                                  12.00
   Unit Hyd. peak (cms)=
                                   .10
                          .24
                                             *TOTALS*
                                 .22
                     1.04
   PEAK FLOW (cms)=
                                              1.261 (iii)
              (hrs)=
                       46.00
   TIME TO PEAK
                                 46.02
                                             46.000
   RUNOFF VOLUME
               (mm) =
                        284.17
                                  196.45
                                            266.654
   TOTAL RAINFALL (mm)=
                        285.00
                                  285.00
                                            285.000
   RUNOFF COEFFICIENT =
                        1.00
                                  .69
                                              .936
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
        CN^* = 50.0 Ia = Dep. Storage (Above)
    (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
        THAN THE STORAGE COEFFICIENT.
   (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*#-----|
*#
    External agricultural area draining onsite and entering Rear Lot Ditch
*#------
DESIGN NASHYD | Area (ha)= .73 Curve Number (CN)=70.00
| 07:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .190
```

PEAK FLOW (cms)= .095 (i) TIME TO PEAK (hrs)= 46.017 RUNOFF VOLUME (mm)= 204.845

.147

Unit Hyd Qpeak (cms)=

```
TOTAL RAINFALL (mm)= 285.000
RUNOFF COEFFICIENT = .719
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
500:0009----
*#-----|
*#
*#
    Total area entering Rear Lot Ditch and entering SWMF at East inlet
*#-----|
______
           ) | ID: NHYD AREA
ADD HYD (RLswl
                             QPEAK TPEAK R.V.
                                           DWF
                       (ha)
                             (cms) (hrs) (mm)
_____
                                           (cms)
                        8.82 1.261 46.00 266.65
            ID1 06:202
                                           .000
           +ID2 07:104
                    .73 .095 46.02 204.85 .000
            ______
                        9.55 1.357 46.00 261.93 .000
            SUM 08:RLswl
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
500:0010-----
*#
  Proposed industrial lots draining to East Road Ditch within catchment,
*#
*#
                and new internal roadway
*#
*#-----|
| DESIGN STANDHYD |
              Area (ha) = 4.92
| 01:204 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)=
                                      80.00
                 IMPERVIOUS PERVIOUS (i)
  Surface Area (ha)=
Dep. Storage (mm)=
                  4.43
                           .49
                   .80
                           1.50
                  2.00
                2.00
181.11
  Average Slope
            (%)=
                          2.00
            (m)=
  Length
                         40.00
  Mannings n
                          .250
             =
  Max.eff.Inten.(mm/hr)= 53.00 92.46
over (min) 4.00 11.00
                         11.00
                3.82 (ii) 11.10 (ii)
  Storage Coeff. (min)=
```

Unit Hyd. Tpeak	(min)=	4.00	11.00	
Unit Hyd. peak	(cms)=	.29	.10	
•				*TOTALS*
PEAK FLOW	(cms)=	.58	.12	.704 (iii)
TIME TO PEAK	(hrs)=	45.98	46.00	46.000
RUNOFF VOLUME	(mm)=	284.17	196.44	266.654
TOTAL RAINFALL	(mm) =	285.00	285.00	285.000
RUNOFF COEFFICI	ENT =	1.00	.69	.936

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

500:0011-----*#------| *# *# Rooftop infiltration lumped together and sized for 25mm runoff volume from an assumed 0.15ha rooftop area per lot (7 lots) *# *#-----| | ADD HYD (Roof) | ID: NHYD AREA QPEAK TPEAK R.V. **DWF** (ha) (cms) 4.92 .704 (hrs) (mm) (cms) .704 46.00 266.65 ID1 01:204 4.92 +ID2 06:202 8.82 1.261 46.00 266.65 .000 ______ SUM 02:Roof 13.74 1.965 46.00 266.65 .000 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY. 500:0012-----ROUTE RESERVOIR Requested routing time step = 1.0 min. IN>02:(Roof) OUT<04:(R-inf) ====== OUTLFOW STORAGE TABLE ====== OUTFLOW STORAGE (cms) (ha.m.) STORAGE | OUTFLOW **STORAGE** cms) (ha.m.) | (cms) (ha.m.) .000 .0000E+00 | .000 .2625E-01

```
AREA QPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) 13.74 1.965 46.000 266.654 .10 .000 1.700 57.057
   ROUTING RESULTS
   ______
   INFLOW >02: (Roof )
OUTFLOW<04: (R-inf )</pre>
  OVERFLOW<10: (infO ) 13.64 1.965 46.000 266.654
            TOTAL NUMBER OF SIMULATED OVERFLOWS =
            CUMULATIVE TIME OF OVERFLOWS (hours)= 48.10
            PERCENTAGE OF TIME OVERFLOWING (%)=
                                     2.74
            PEAK FLOW REDUCTION [Qout/Qin](%)= .001
            TIME SHIFT OF PEAK FLOW (min)= -2658.00
            MAXIMUM STORAGE USED (ha.m.)=.2625E-01
   *** WARNING: Outflow volume is less than inflow volume.
 ______
*#------
          Proposed SWM facility catchment (infiltration basin)
*#
*#-----|
DESIGN NASHYD | Area (ha)= 1.63 Curve Number (CN)=57.00
Unit Hyd Qpeak (cms)= .178
  PEAK FLOW (cms)= .178 (i)
TIME TO PEAK (hrs)= 46.117
             (mm) = 169.164
   RUNOFF VOLUME
   TOTAL RAINFALL (mm)= 285.000
   RUNOFF COEFFICIENT = .594
   (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0014-----
*#-----|
*#
                All flows entering SWM facility
*#-----|
```

```
ADD HYD (ToSWM
             ) | ID: NHYD
                               AREA
                                      OPEAK
                                            TPEAK R.V.
                                                        DWF
                                      (cms)
                                            (hrs) (mm)
                               (ha)
                                                        (cms)
                               13.64
               ID1 10:inf0
                                     1.965
                                            46.00 266.65
                                                        .000
              +ID2 07:104
                                .73 .095 46.02 204.85
                                                        .000
               +ID3 09:205
                               1.63 .178 46.12 169.16
                                                        .000
               ______
               SUM 06:ToSWM
                               16.00 2.235 46.00 253.90
  NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
*#
*#
                 Infiltration Portion of SWM facility
*#------|
-----
ROUTE RESERVOIR
                  Requested routing time step = 1.0 min.
IN>06:(ToSWM )
                  ====== OUTLFOW STORAGE TABLE ======
OUT<07:(SWMinf)
                  OUTFLOW
                           STORAGE | OUTFLOW STORAGE
                                  (cms) (ha.m.)
                    (cms) (ha.m.)
                                     .044 .7033E+00
                     .000 .0000E+00
                     .044 .6530E-01
                                      .000 .0000E+00
                    AREA QPEAK
(ha) (cms)
16.00 2.235
                                     TPEAK
   ROUTING RESULTS
                                               R.V.
                                     (hrs)
                                               (mm)
                                     46.000 253.903
   INFLOW >06: (ToSWM )
   OUTFLOW<07: (SWMinf)
                       5.58
                              .044
                                     6.517 253.894
  OVERFLOW<08: (OVF-I ) 10.42
                                     46.000 253.903
                               2.190
              TOTAL NUMBER OF SIMULATED OVERFLOWS =
              CUMULATIVE TIME OF OVERFLOWS (hours)=
                                              8.37
              PERCENTAGE OF TIME OVERFLOWING (%)=
                                             5.87
                   FLOW REDUCTION [Qout/Qin](%)=
              PEAK
              TIME SHIFT OF PEAK FLOW
                                      (min) = -2369.00
                                     (ha.m.)=.7033E+00
              MAXIMUM STORAGE USED
500:0016-----
```

- -

```
*#
*#
                                             Active Storage Portion of SWM facility
*#
*#-----|
  ROUTE RESERVOIR
                                                    Requested routing time step = 1.0 min.
    IN>08:(OVF-I )
OUT<01:(SWMout) ======= OUTLFOW STORAGE TABLE =======
                                                                          STORAGE | OUTFLOW
                                                   OUTFLOW
                                                                                                                         STORAGE
                                                                                                 (cms)
                                                        (cms)
                                                                        (ha.m.)
                                                                                                                          (ha.m.)
                                                                                                1.479 .2400E+00
4.101 .4070E+00
                                                          .000 .0000E+00
                                                          .202 .7850E-01
                                                          .689 .1586E+00 | .000 .0000E+00
      | ADEA | QPEAK | TPEAK | R.V. | (ha) | (cms) | (hrs) | (mm) | | (10.42 | 2.190 | 46.000 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 253.903 | (10.42 | 2.145 | 46.050 | 2.145 | (10.42 | 2.145 | 46.050 | 2.145 | (10.42 | 2.145 | 46.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 40.050 | 2.145 | (10.42 | 2.145 | 2.145 | 40.050 | (10.42 | 2.145 | 2.145 | 2.145 | (10.42 | 2.145 | 2.145 | (10.42 | 2.145 | 2.145 | (10.42 | 2.145 | 2.145 | 2.145 | (10.42 | 2
                                       TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                       CUMULATIVE TIME OF OVERFLOWS (hours)=
                                                                                                                                    .00
                                       PERCENTAGE OF TIME OVERFLOWING (%)=
                                                                                                                                    .00
                                       PEAK FLOW REDUCTION [Qout/Qin](%)= 97.929
                                       TIME SHIFT OF PEAK FLOW (min)= 3.00
                                       MAXIMUM STORAGE USED
                                                                                                      (ha.m.)=.2824E+00
500:0017-----
*#------
*#
*#
            West Road Ditch, conveying external drainage from the west around the
*#
                                          proposed SWM facility to Outlet Channel
*#------|
DESIGN NASHYD | Area (ha)= 1.22 Curve Number (CN)=50.00
\mid 02:206 DT= 1.00 \mid Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .810
         Unit Hyd Qpeak (cms)=
                                                               .058
         PEAK FLOW
                                           (cms) = .100 (i)
          TIME TO PEAK
                                           (hrs) = 47.067
          RUNOFF VOLUME
                                          (mm) = 149.530
```

```
RUNOFF COEFFICIENT = .525
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0018-----
*#-----|
*#
*#
     Grassed area south of SWM facility draining offsite to the south
*#-----|
DESIGN NASHYD
             Area (ha)= .14 Curve Number (CN)=50.00
             Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| 10:207 DT= 1.00 |
----- U.H. Tp(hrs)=
                      .070
  Unit Hyd Qpeak (cms)= .076
           (cms) = .015 (i)
  PEAK FLOW
  TIME TO PEAK (hrs)=
                46.000
           (mm)= 149.530
  RUNOFF VOLUME
  TOTAL RAINFALL (mm)= 285.000
  RUNOFF COEFFICIENT =
                  .525
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0019-----
*#------|
*#
          Total Flows to the east from internal catchments
*#------
_____
           ) | ID: NHYD
                                 TPEAK R.V.
ADD HYD (IntE
                             QPEAK
                                           DWF
                        AREA
_____
                            (cms)
                        (ha)
                                 (hrs) (mm)
                                           (cms)
                        1.33
                             .165 46.00 204.08
            ID1 05:IntUcE
                                           .000
           +ID2 01:SWMout 10.42 2.145 46.05 253.90 .000
                    1.22 .100 47.07 149.53
           +ID3 02:206
                                           .000
```

SUM 07:IntE

12.97 2.375 46.02 238.98 .000

TOTAL RAINFALL (mm)= 285.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

500:0020			
*#			·
*#====================================			
*#=============			
*#			
*#			
*# External industrial ca *# Ceda	•	_	ining south across
*# Ceua	r Creek Road and	entering phoo	
*#			
			•
CALIB STANDHYD			
03:100 DT= 1.00	Total $Imp(\%) = 8$	0.00 Dir. Con	n.(%)= 50.00
	TMPERVIOUS	PERVIOUS (i)	
Surface Area (ha			
Dep. Storage (mm			
Average Slope (%	1.60	2.00	
)= 1500.00		
Mannings n	= .020	.250	
Max.eff.Inten.(mm/hr)= 53.00	126.91	
over (min	19.00	24.00	
Storage Coeff. (min)= 18.81 (ii) 24.21 (ii)	
Unit Hyd. Tpeak (min)= 19.00	24.00	
Unit Hyd. peak (cms)= .06	.05	*TOTALS*
PEAK FLOW (cms)= 3 91	3 57	7.465 (iii)
TIME TO PEAK (hrs			
RUNOFF VOLUME (mm)= 282.91	235.37	259.226
TOTAL RAINFALL (mm)= 285.00	285.00	285.000
RUNOFF COEFFICIENT	= .99	.83	.910
(i) CN PROCEDURE S	ELECTED EOD DEDVT	OUS LOSSES.	
• •	Ia = Dep. Storag		
(ii) TIME STEP (DT)		•	
THAN THE STORA	GE COEFFICIENT.		
(iii) PEAK FLOW DOES	NOT INCLUDE BASE	FLOW IF ANY.	

500:0021-----

- -

```
*#-----|
*#
*# External catchment containing a portion of Cedar Creek Road, a portion
*# of industrial area, and a grassed area near Hwy 401 off-ramp, entering BPSS
*#-----|
                   Area (ha) = 14.55
DESIGN STANDHYD
| 07:101 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)=
                       IMPERVIOUS
                                   PERVIOUS (i)
   Surface Area (ha)=
                        8.73
                                     5.82
   Dep. Storage (mm)=
Average Slope (%)=
                      .80
2.30
311.45
                                     1.50
                                    2.30
   Length
                 (m)=
                                   40.00
   Mannings n
                         .013
                                    .250
                        53.00
                                   54.13
   Max.eff.Inten.(mm/hr)=
            over (min)
                          5.00
                                   14.00
   Storage Coeff. (min)=
                         5.07 (ii) 13.72 (ii)
   Unit Hyd. Tpeak (min)=
                          5.00
                                   14.00
                                     .08
   Unit Hyd. peak (cms)=
                          .22
                                               *TOTALS*
                      1.03
46.00
   PEAK FLOW
                (cms)=
                                    .85
                                                1.875 (iii)
                                  46.03
   TIME TO PEAK
               (hrs)=
                                               46.000
   RUNOFF VOLUME
                (mm) =
                         284.19
                                   168.10
                                               223.839
   TOTAL RAINFALL (mm)=
                         285.00
                                    285.00
                                               285.000
   RUNOFF COEFFICIENT =
                          1.00
                                     .59
                                                 .785
     (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
```

- $CN^* = 50.0$ Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
500:0022-----
*#-----|
*#
   Total area draining offsite to east onto agricultural area to the east
*#-----|
-----
| ADD HYD (UCtoE ) | ID: NHYD
                     AREA
                          OPEAK
                              TPEAK
                                  R.V.
                                      DWF
                     (ha)
                          (cms)
                              (hrs) (mm)
                                      (cms)
          ID1 05:IntUcE
                     1.33
                          .165 46.00 204.08
                                      .000
                     55.94 7.465 46.10 259.23
          +ID2 03:100
                                      .000
```

+ID3 07:101 14.55 1.875 46.00 223.84 .000

SUM 09:UCtoE 71.82 9.434 46.03 251.04 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

500:0023					
*#					
*#	'				'
*# Large exte	rnal catchment	west of si	te containing	industrial pr	operty.
•	to private SWM		_	-	
•	around SWM faci				, 8
*#		•	· ·		
*#					
					·
DESIGN STANDH	YD Area	(ha)=	12.64		
04:102 DT=	1.00 Total	Imp(%)=	80.00 Dir.	Conn.(%)= 50	0.00
			PERVIOUS ((i)	
Surface Ar	ea (ha)=	10.11	2.53		
Dep. Stora	ge (mm)=	.80	1.50		
	ope (%)=				
Length	(m)=	290.29	40.00		
Mannings n	=	.013	.250		
Max.eff.In	ten.(mm/hr)=	53.00	119.98		
	over (min) eff. (min)=	4.00	10.00		
Storage Co	eff. (min)=	4.45 (ii) 10.20 (i	ii)	
_	Tpeak (min)=				
Unit Hyd.	peak (cms)=	.26	.11		
				TOTALS	
	(cms)=				(iii)
TIME TO PE	AK (hrs)=	46.00	46.00	46.000	
RUNOFF VOL	UME (mm)=	284.17	209.52	246.871	
TOTAL RAIN	FALL (mm)=	285.00	285.00	285.000	
RUNOFF COE	FFICIENT =	1.00	.74	.866	
(i) CN P	ROCEDURE SELECT	ED FOR PER	VIOUS LOSSES:		

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
500:0024-----
*#-----|
*#
                Infiltration in External SWM Feature
*#
*#-----|
                 Requested routing time step = 1.0 min.
 ROUTE RESERVOIR
 IN>04:(102 )
OUT<05:(xSWinf) ======= OUTLFOW STORAGE TABLE =======
                 OUTFLOW
                        STORAGE | OUTFLOW
                                         STORAGE
                  (cms)
                        (ha.m.)
                                  (cms)
                                         (ha.m.)
                                  .018 .3759E+00
                   .000 .0000E+00
                   .018 .4380E-01
                                   .000 .0000E+00
                     AREA
                            QPEAK
                                  TPEAK
                                           R.V.
   ROUTING RESULTS
                     (ha)
                            (cms)
                                   (hrs)
                                           (mm)
   INFLOW >04: (102 )
                     12.64
                            1.765
                                  46.000
                                         246.871
   OUTFLOW<05: (xSWinf)
                     2.73
                            .018
                                  4.833
                                         246.884
  OVERFLOW<06: (OVF-xI)
                     9.91
                            1.746
                                  46.000
                                         246.871
             TOTAL NUMBER OF SIMULATED OVERFLOWS =
                                             2
             CUMULATIVE TIME OF OVERFLOWS (hours)=
                                         15.28
             PERCENTAGE OF TIME OVERFLOWING
                                    (%)=
                                          8.41
             PEAK
                  FLOW
                      REDUCTION [Qout/Qin](%)=
             TIME SHIFT OF PEAK FLOW
                               (min) = -2470.00
             MAXIMUM STORAGE USED
                                 (ha.m.)=.3759E+00
500:0025-----
*#-----|
*# External catchment west of the site, containing a portion of exisiting
*# industrial property, draining east into West Road Ditch, routing around
*#
               SWM facility and entering Outlet Channel
*#
*#-----|
DESIGN STANDHYD
                 Area (ha) = 4.52
07:103 DT= 1.00
                Total Imp(%)=
                            80.00 Dir. Conn.(%)=
                                              50.00
                    IMPERVIOUS
                              PERVIOUS (i)
   Surface Area
               (ha)=
                     3.62
                                .90
   Dep. Storage
               (mm) =
                       .80
                                1.50
```

Average Slope	(%)=	5.30	5.30	
Length	(m) =	173.59	40.00	
Mannings n	=	.013	.250	
	41.		400.05	
Max.eff.Inten.(mm/hr)=	53.00	120.05	
over	(min)	3.00	8.00	
Storage Coeff.	(min)=	2.78	(ii) 7.68	(ii)
Unit Hyd. Tpeak	(min)=	3.00	8.00	
Unit Hyd. peak	(cms) =	.39	.15	
				TOTALS
PEAK FLOW	(cms) =	.33	.30	.633 (iii)
TIME TO PEAK	(hrs)=	45.73	46.00	46.000
RUNOFF VOLUME	(mm) =	284.18	209.52	246.871
TOTAL RAINFALL	(mm)=	285.00	285.00	285.000
RUNOFF COEFFICI	ENT =	1.00	.74	.866

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 50.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

- # # # # #	Total	Flows through	West Road	Ditch			
ADD HYD (WRswl) 	ID: NHYD	AREA (ha)	QPEAK (cms)		R.V.	DWF
	ID1	06:0VF-xI	9.91	, ,		246.87	.000
	+ID2	07:103	4.52	.633	46.00	246.87	.000
	+ID3	02:206	1.22	.100	47.07	149.53	.000
	===: SUM	========= 08:WRswl	15.65	2.451	46.00	239.28	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

500:0027-----

- -

```
_____
| 05:208 DT= 1.00 |
 ----- U.H. Tp(hrs)=
                   .850
  Unit Hyd Qpeak (cms)= .051
  PEAK FLOW (cms) = .092 (i)
  TIME TO PEAK (hrs)=
              47.100
          (mm) = 149.530
  RUNOFF VOLUME
          (mm) = 285.000
  TOTAL RAINFALL
  RUNOFF COEFFICIENT =
              .525
  (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
500:0028-----
*#------
*#
         Total Flows through Outlet Channel
*#------|
______
| ADD HYD (OutChan ) | ID: NHYD
                     AREA
                         QPEAK
                             TPEAK R.V.
                                     DWF
                     (ha) (cms) (hrs) (mm)
10.42 2.145 46.05 253.90
                             (hrs) (mm)
                                     (cms)
          ID1 01:SWMout
                 15.65 2.451 46.00 239.28
         +ID2 08:WRswl
                                     .000
          +ID3 05:208
                 1.13 .092 47.10 149.53
                                     .000
          ______
          SUM 03:OutChan
                     27.20 4.650 46.00 241.15
                                     .000
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
______
500:0029-----
*#-----|
*#
*#
         Total Flows to the east (eventually to Cedar Creek)
*#------
```

*#------

ADD HYD (TotE) ID: NHYD ID1 01:SWMout	AREA (ha) 10.42	(cms)	(hrs)	R.V. (mm) 253.90	
	+ID2 08:WRswl	15.65	2.451	46.00	239.28	.000
	+ID3 09:UCtoE	71.82	9.434	46.03	251.04	.000
	SUM 04:TotE		14.011			
	S DO NOT INCLUDE BASE					
 *# *#						
 *# *#	Total Flows -					
ADD HYD (AllFlo) ID: NHYD		QPEAK			
	ID1 04:TotE		(cms) 14.011			
	+ID2 10:207	.14	.015	46.00	149.53	.000
	SUM 06:AllFlo	98.03	14.026	46.02	249.32	.000
NOTE: PEAK FLOW	S DO NOT INCLUDE BASE	FLOWS IF	ANY.			
500:0031						
500:0002						
500:0002						

```
500:0002-----
______
500:0002-----
500:0002-----
500:0002-----
500:0002-----
   FINISH
**************************************
   WARNINGS / ERRORS / NOTES
   -----
001:0012 ROUTE RESERVOIR
   *** WARNING: Outflow volume is less than inflow volume.
001:0016 ROUTE RESERVOIR
   *** WARNING: Inflow hydrograph is dry.
002:0012 ROUTE RESERVOIR
   *** WARNING: Outflow volume is less than inflow volume.
002:0016 ROUTE RESERVOIR
   *** WARNING: Inflow hydrograph is dry.
005:0012 ROUTE RESERVOIR
   *** WARNING: Outflow volume is less than inflow volume.
005:0016 ROUTE RESERVOIR
   *** WARNING: Inflow hydrograph is dry.
010:0012 ROUTE RESERVOIR
   *** WARNING: Outflow volume is less than inflow volume.
010:0016 ROUTE RESERVOIR
   *** WARNING: Inflow hydrograph is dry.
025:0012 ROUTE RESERVOIR
   *** WARNING: Outflow volume is less than inflow volume.
   *** WARNING: Outflow volume is less than inflow volume.
   *** WARNING: Outflow volume is less than inflow volume.
   *** WARNING: Outflow volume is less than inflow volume.
 Simulation ended on 2024-01-25
                       at 15:15:07
______
```

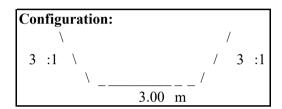
Manning's Equation Calculations for Flow in a Channel

2509 Cedar Creek Road

Section: West Road Ditch

Input Data: Flow = 4.256 m³/s Manning's 'n' = 0.025 Channel Slope = 1.0% Side Slope = 3 m/m [3 means 3:1] Side Slope = 3 m/m [3 means 3:1] Bottom Width = 3 m [0 = triangular, +ve = trapezoidal]

Calculated Values:Velocity =2.00 m/sArea= 2.130 m^2 Wetted Perimeter =6.035 mHydraulic Radius (R) =0.353 m

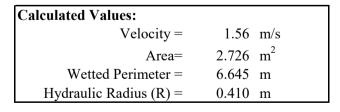


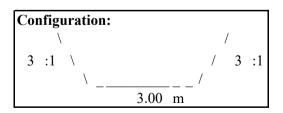
Depth Estimate:

Estimated Flow Depth = 0.480 m lhs-rhs = -0.00038

Note: Calculations are correct when lhs-rhs = 0

Section: West Road Ditch (South of SWMF)





Depth Estimate:

Estimated Flow Depth = 0.576 m lhs-rhs = 3.8E-06

Note: Calculations are correct when lhs-rhs = 0

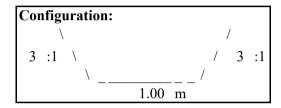
Manning's Equation Calculations for Flow in a Channel

2509 Cedar Creek Road

Section: Rear Lot Ditch

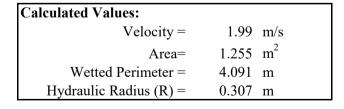
Input Data: Flow = 4.377 m³/s Manning's 'n' = 0.025 Channel Slope = 1.0% Side Slope = 3 m/m [3 means 3:1] Side Slope = 3 m/m [3 means 3:1] Bottom Width = 1 m [0 = triangular, +ve = trapezoidal]

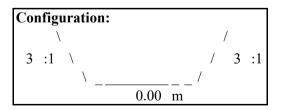
Calculated Values:Velocity =2.13 m/sArea= 2.054 m^2 Wetted Perimeter =5.285 mHydraulic Radius (R) =0.389 m



Depth Estimate:
Estimated Flow Depth = 0.677 m lhs-rhs = 0.00018
Note: Calculations are correct when lhs-rhs = 0

Section: East Road Ditch





Depth Estimate:
Estimated Flow Depth = 0.647 m lhs-rhs = 0.00031
Note: Calculations are correct when lhs-rhs = 0

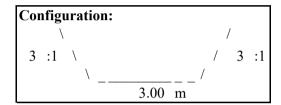
Manning's Equation Calculations for Flow in a Channel

2509 Cedar Creek Road

Section: Outlet Channel

Input Data:	
Flow =	$4.65 ext{ m}^3/\text{s}$
Manning's 'n' =	0.025
Channel Slope =	0.5%
Side Slope =	3 m/m [3 means 3:1]
Side Slope =	3 m/m [3 means 3:1]
Bottom Width =	3 m $[0 = triangular, +ve = trapezoidal]$

Calculated Values:Velocity =1.60 m/sArea = 2.904 m^2 Wetted Perimeter =6.818 mHydraulic Radius (R) =0.426 m



Depth Estimate:

Estimated Flow Depth = 0.604 m lhs-rhs = 0.00014

Note: Calculations are correct when lhs-rhs = 0

APPENDIX E

Utility Correspondence

Nicholas, Pacifique

From: Nicholas, Pacifique

Sent: Thursday, August 3, 2023 3:14 PM

To: Steffler, Daniel

Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Hi Dan,

Thank you very much for providing this information.

Our understating is that Bell sees no concern with supporting the proposed development given the surrounding existing infrastructure. Could you please confirm this?

Thank you,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

Stantec

100-300 Hagey Boulevard Waterloo ON N2L 0A4



From: Steffler, Daniel <daniel.steffler@bell.ca>
Sent: Wednesday, August 2, 2023 6:00 PM

To: Nicholas, Pacifique <Pacifique.Nicholas@stantec.com> **Subject:** RE: 161414214- 2509 Cedar Creek Road - Utility

See attached. The black line is existing duct to our fibre pedestal. The red is our proposed new to get fibre to your development.

thanks



Dan Steffler

Specialist – Network Provisioning F2-20 Water Street North Kitchener, Ontario N2H 5A5

Phone: 519-568-5785 Cell: 519-577-2531 daniel.steffler@bell.ca

From: Nicholas, Pacifique < Pacifique. Nicholas@stantec.com >

Sent: July-27-23 1:49 PM

To: Steffler, Daniel < daniel.steffler@bell.ca>

Subject: [EXT]RE: 161414214- 2509 Cedar Creek Road - Utility

Hi Dan,

Could you please reattach the drawing? I could not find the attachment as addressed in your email.

Thanks

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

Stantec 100-300	Hagey Bo	ulevaro
	ON N2L	
		1

From: Nicholas, Pacifique

Sent: Wednesday, July 26, 2023 8:45 AM **To:** Steffler, Daniel < daniel.steffler@bell.ca>

Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Hi Dan,

I do not see the attachment in this email. Could you please verify if it was attached properly? We have not stated the construction yet. We are still in the process of Draft Plan approval.

Thanks,

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Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development Direct: 519 585-7484

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

100-300 Hagey Boulevard

Waterloo ON N2L 0A4

From: Steffler, Daniel < daniel.steffler@bell.ca>

Sent: Tuesday, July 25, 2023 6:18 PM

To: Nicholas, Pacifique < <u>Pacifique.Nicholas@stantec.com</u>> **Subject:** RE: 161414214- 2509 Cedar Creek Road - Utility

Hello,

See attached, we have a fibre ped on opposite side of Earl Thompson with conduit crossing and goes down Earl Thompson. We will use that duct and trench down Cedar Creek to your development. Have any lots started construction? thanks



Dan Steffler

Specialist – Network Provisioning F2-20 Water Street North Kitchener, Ontario N2H 5A5

Phone: 519-568-5785 Cell: 519-577-2531 daniel.steffler@bell.ca

From: Nicholas, Pacifique < Pacifique.Nicholas@stantec.com>

Sent: July-17-23 11:15 AM

To: Steffler, Daniel < daniel.steffler@bell.ca>

Subject: [EXT]161414214- 2509 Cedar Creek Road - Utility

Hi Dan,

We are currently working towards completing the preliminary engineering for the above noted development in support of draft plan approval which will follow with detail design.

Please find attached Conceptual Draft Plan for your review.

Please provide utility information for the surrounding area that Bell may have and confirm if you are able to service this development or if any external works would need to be upgraded or extended to the property.

If you have any questions, please let me know.

Thank you,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

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Nicholas, Pacifique

From: Nicholas, Pacifique

Sent: Tuesday, August 15, 2023 4:57 PM

To: Sahil Singh Sidhu

RE: 161414214- 2509 Cedar Creek Road - Utility Subject:

We can have this information late this Fall.

Thanks,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

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From: Sahil Singh Sidhu <sahilsingh.sidhu@enbridge.com>

Sent: Tuesday, August 15, 2023 4:30 PM

To: Nicholas, Pacifique < Pacifique. Nicholas@stantec.com > Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Hi Nicholas,

I will need that info for me to see if the load Gas main can support it. When do you think you can provide me with this info.

Thanks

Sahil Singh Sidhu

Sr Analyst New Business Projects

Construction Brantford



CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

101 Carter St, Brantford, ON N3S 0K6

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Customer Attachment - Residential enbridgegas.com/connect-to-gas
Customer Attachment - Developers enbridgegas.com/connect-to-gas/developers

Customer Attachment - Builders & HVAC's enbridgegas.com/connect-to-gas/builders-hvacs

From: Nicholas, Pacifique < Pacifique.Nicholas@stantec.com

Sent: Tuesday, August 15, 2023 4:25 PM

To: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com>

Subject: [External] RE: 161414214- 2509 Cedar Creek Road - Utility

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Hi Sahil,

We do not have this information yet.

Once we advance to detailed design, we can then provide you with more information.

Thanks,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

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100-300 Hagey Boulevard Waterloo ON N2L 0A4



From: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com >

Sent: Tuesday, August 15, 2023 3:39 PM

To: Nicholas, Pacifique < Pacifique.Nicholas@stantec.com> Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Can you please let me know the load for each lot if you have that info available.

Thanks,

Sahil Singh Sidhu

Sr Analyst New Business Projects

Construction Brantford



CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

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Customer Attachment - Developers enbridgegas.com/connect-to-gas/developers

Customer Attachment - Builders & HVAC's enbridgegas.com/connect-to-gas/builders-hvacs

From: Nicholas, Pacifique < Pacifique.Nicholas@stantec.com

Sent: Tuesday, August 15, 2023 3:32 PM

To: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com> **Cc:** Brousseau, Kevin < <u>kevin.brousseau@stantec.com</u>>

Subject: [External] RE: 161414214- 2509 Cedar Creek Road - Utility

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Hi Sahil,

Thank you very much for getting back to me. As said earlier, we are still in the prelim design stage for Draft Plan approval. All we need currently is an understanding of your existing infrastructure in the area of the subject lands and if you have capacity to support the development.

Thanks,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

Direct: 519 585-7484 Mobile: 226 581-2805 Fax: 519 579-6733

Pacifique.nicholas@stantec.com

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From: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com >

Sent: Monday, August 14, 2023 10:42 AM

To: Nicholas, Pacifique < Pacifique. Nicholas@stantec.com >

Cc: Brousseau, Kevin < kevin.brousseau@stantec.com > Subject: FW: 161414214-2509 Cedar Creek Road - Utility

Hi,

I received this from our department.

Can you please provide me with answers

Thanks,

Sahil Singh Sidhu

Sr Analyst New Business Projects Construction Brantford

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CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

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Natural Gas Inquiries - <u>Inquiry Form</u>
Customer Attachment - Residential <u>enbridgegas.com/connect-to-gas</u>

Customer Attachment - Developers enbridgegas.com/connect-to-gas/developers
Customer Attachment - Builders & HVAC's enbridgegas.com/connect-to-gas/builders-hvacs

From: Ontario Lands < ONTLands@enbridge.com >

Sent: Monday, August 14, 2023 10:39 AM

To: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com> Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Good morning,

Being from North Dumfries, this is Kelly's area and she is off this week.

I can look into it, but require a bit of info first.

Do you have the Notice of Decision which contains the conditions of Draft Approval? We require the conditions that require the release being the document as issued by the Municipality that sites our conditions.

Thanks,

Barb

Barbara M.J. Baranow **Analyst Land Support** Lands

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From: Sahil Singh Sidhu <sahilsingh.sidhu@enbridge.com>

Sent: Monday, August 14, 2023 10:24 AM

To: Ontario Lands <ONTLands@enbridge.com>; Kelly Buchanan <Kelly.Buchanan@enbridge.com>

Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Hi,

Can you please advice the customer what to do here.

Thanks,

Sahil Singh Sidhu

Sr Analyst New Business Projects Construction Brantford



CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

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Natural Gas Inquiries - <u>Inquiry Form</u> Customer Attachment - Residential <u>enbridgegas.com/connect-to-gas</u>

Customer Attachment - Developers enb

Customer Attachment - Builders & HVAC's enbridgegas.com/connect-to-gas/builders-hvacs

From: Sahil Singh Sidhu

Sent: Friday, August 4, 2023 8:16 AM

To: Ontario Lands < ONTLands@enbridge.com >

Subject: RE: 161414214- 2509 Cedar Creek Road - Utility

Hi,

I am just following up on this request.

Thanks,

Sahil Singh Sidhu

Sr Analyst New Business Projects

Construction Brantford



CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

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Customer Attachment - Residential enbridgegas.com/connect-to-gas

Customer Attachment - Developers <u>enbridgegas.com/connect-to-gas/developers</u>
Customer Attachment - Builders & HVAC's <u>enbridgegas.com/connect-to-gas/builders-hvacs</u>

From: Sahil Singh Sidhu

Sent: Tuesday, July 25, 2023 10:03 AM

To: Ontario Lands < ONTLands@enbridge.com>

Subject: FW: 161414214- 2509 Cedar Creek Road - Utility

Good Morning,

This customer is looking for clearance letter I don't see any issues with this. Please let me know if you need anything.

Thanks,

Sahil Singh Sidhu

Sr Analyst New Business Projects

Construction Brantford



CELL: (519) 209-8538 | sahilsingh.sidhu@enbridge.com

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Customer Attachment - Residential enbridgegas.com/connect-to-gas

Customer Attachment - Developers enbridgegas.com/connect-to-gas/developers

Customer Attachment - Builders & HVAC's enbridgegas.com/connect-to-gas/builders-hvacs

From: Nicholas, Pacifique < Pacifique.Nicholas@stantec.com>

Sent: Monday, July 17, 2023 11:13 AM

To: Sahil Singh Sidhu < sahilsingh.sidhu@enbridge.com> **Cc:** Brousseau, Kevin < <u>kevin.brousseau@stantec.com</u>>

Subject: [External] FW: 161414214- 2509 Cedar Creek Road - Utility

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Hi Sahil,

We are currently working towards completing the preliminary engineering for the above noted development in support of draft plan approval which will follow with detail design.

Please find attached Conceptual Draft Plan for your review.

Please provide utility information for the surrounding area that Enbridge may have and confirm if you are able to service this development or if any external works would need to be upgraded or extended to the property.

If you have any questions, please let me know.

Thank you,

Pacifique Nicholas, P.Eng., M.Eng., PMP®.

Project Coordinator - Community Development

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